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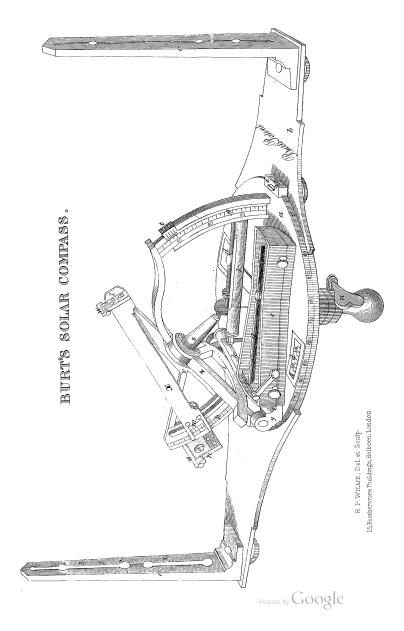
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## AKEY

TO THE

# SOLAR COMPASS,

AND

## SURVEYOR'S COMPANION;

COMPRISING

All the Kules necessary for Use in the Field.

ALSO,

DESCRIPTION OF THE LINEAR SURVEYS, AND PUBLIC LAND SYSTEM
OF THE UNITED STATES; NOTES ON THE BAROMETER,
SUGGESTIONS FOR AN OUTFIT FOR A SURVEY
OF FOUR MONTHS, ETC., ETC.

### BY WILLIAM A. BURT,

U. S. DEPUTY SURVEYOR.

PHILADELPHIA:
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### PREFACE.

Much perplexity and difficulty has been felt by surveyors in the use of the Magnetic Compass, in consequence of its variations from the true meridian, at various localities or stations, and also its almost constant diurnal changes as well as aberrations, caused by local attraction. A more perfect guide for the surveyor than the Magnetic Needle was, therefore, very desirable. The long continued efforts made by the author to accomplish this object, resulted in the invention of the Solar or Astronomical Compass. A model of this instrument was made in the year 1835, by the inventor, in order to test its principles, and in the latter part of the same year, the first Solar Compass was made, under his direction and supervision, by William J. Young, of Philadelphia. Pa. The instrument was then submitted to a committee of the Franklin Institute, of the State of Pennsylvania, who after a full examination of its principles and merits, awarded the inventor a premium of twenty dollars and a "Scott's Legacy" medal. The Solar Compass as then made, like most newly invented instruments, was soon found susceptible of improvement and of greater usefulness than at first anticipated. Accordingly the inventor made several alterations and improvements suggested by experience, and in December, 1840, again submitted the instrument, as improved, to a committee of the same Institute, who reported a decided improvement, in point of accuracy, and the simplicity of its adjustments and use. The inventor has since continued to improve this instrument as more experience in the use of it seemed to suggest. And in 1851 exhibited it, as improved, at the World's Fair, in the city of London, where a premium medal was awarded the exhibitor by the jurors on Astronomical Instruments.

Since its invention in 1835, and during its progressive improvements, the inventor has been called upon, personally or by letter, from a large portion of the surveyors of the public lands, for information how to adjust and use it. Such inquiries could be but imperfectly answered by letter, or a few hours' conversation, and the author could not, without being discourteous, avoid replying in some manner to such necessary inquiries, though a serious tax sometimes on his business. To prevent this the inventor published a few pages of instructions, showing how to adjust and use this instrument, and distributed them among the surveyors; but soon after this, new discoveries were made in the construction and adjustments of the Solar Compass, consequently what had been done only supplied their wants in part, and the inventor was solicited by many of the surveyors of the public lands for full instructions on this subject, and a treatise on surveying adapted to their wants in the field of survey. The foregoing remarks constitute the apology of the author for assuming a task so foreign to his habits of life, and to which duty seemed to impel him in the absence of any prospects of this much needed work being soon accomplished by any other person. This treatise contains much original matter, mostly derived from experience in practical surveying. The elements of surveying as published and taught in the schools, are purposely omitted to lessen the size of this work, the object of which is to furnish the practical surveyor with a convenient pocket companion suited to his business while engaged in his field work. The inexperienced surveyor in this branch of the public service has

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need of all necessary information to enable him to accomplish his arduous duties in a proper manner. The frequent failures in part, or in whole, by many Deputy Surveyors, have done much injury to the public surveys, and ruined their hopes and reputation.

This is a sufficient reason for introducing into this work the necessary outfit and preparations for a large survey in the wilderness, the want of which has been one of the principal causes of these failures.

The author does not presume that this treatise is without defects; he indulges the hope, however, that it will answer the purpose for which it is designed, until further experience shall furnish a better. The author has availed himself of the experience of several practical surveyors, in preparing this work, and has also consulted the best authorities that appeared to throw light upon the subjects treated of.

The tables of Natural Sines and Tangents, at the end of the work, have been carefully compared with different standard works, and are offered to the surveyor with a confidence that he will find them accurate. The table of chords has been added to supply a want, frequently experienced, in draughting, where a reliable protractor is not at hand. The majority of protractors accompanying draughting instruments are either so small or so inaccurate as to be productive of sensible errors in large draughts.

## CONTENTS.

Solar Compass described,	Page
Principles of the Solar Compass explained,	
Adjustments of the Solar Compass, "	
How the Solar Compass should be made,	
Astronomy, for the use of the Solar Compass,	
Nautical Almanac, how to use it, &c.,	
Fixed stars, and table of,	
Latitude, how to determine with the Solar Compass,	
" by the Pole star, " "	
Table of elongations of the Pole star,	
To find the true meridian, &c., by the Solar Compass,	
To find the Zenith distance and altitude, "	
Time of day by the Sun,	
Diurnal variation of the magnetic needle,	
To find the time of the meridian passage of fixed stars,	
The effects of refraction and parallax on the Solar Compass,	
Table of the proportional parts of refraction and	
parallax to be allowed on the Solar Compass,	31
Table of refraction,	
Table of corrections for the Moon's parallax and refraction,	
Measuring lines with the chain,	
Telescopic measurement in meandering rivers, &c.,	
Table—chains into feet. Feet into chains,	
Measuring distances over rivers, lakes, &c.,	
Use of the parallel rule, in ascertaining the contents of	
multangular fields, &c.,	43
Rafts for crossing rivers, lakes, &c.,	
Running lines with the Solar Compass,	45
Table for correcting the Sun's declination by the hourly differ-	
ences,	47

Influence of metallic veins on the magnetic needle	49
Rules for correcting the course of random lines	
Table for correcting the course of random lines,	
Latitude and longitude of places in North America,	
Table of lengths of degrees of latitude and longitude,	
How to run parallels of latitude	
Convergency of meridians,	
Rule for computing the amplitude,	
" to find the time of the Sun's rising or setting,	
" for the angles of the equatorial lines,	
Rule for computing the elongation of the Pole star,	
" the Moon's parallax in altitude, &c.,	
To find the meridional refraction,	60
Barometer,	61
Barometrical table for computing heights, &c.,	31–64
Aneroid Barometer, and measurement of heights,	63
System of Survey of the United States lands,	
Of Subdividing Townships,	
Restoring extinct corners, &c.,	69
Act concerning mode of Surveying Public Lands,	
Linear, Geological and Topographical Surveys,	
Table of corrections of levels for curvature and refraction,	
Suggestions for an outfit for a Surveying Company,	
Depots in advance of a survey,	
PART II.	
Traverse Table,	
Table of Natural Sines,	92
" Tangents,	
Table for comparison of French and English Barometers,	116
Table of Chards to a Radius of Unity	

## AKEY

TO THE

## SOLAR COMPASS, AND SURVEYOR'S COMPANION.

#### THE SOLAR COMPASS DESCRIBED.

SEE PLATE I.

The Solar Compass works astronomically in determining latitude. and in measuring horizontal angles from the true meridian, and in determining the declination, and hour arcs, of celestial objects within the Zodiac; and is further used as a magnetic compass. strument is used on a tripod, with a ball and socket, in order to adjust it readily to an approximate level by the hand, after which it is adjusted to a true level by means of four thumb-screws at the lower end of the socket, by which it is attached to the tripod. part of these are seen in the plate, except the ball, clamp and screw, This clamp fastens the instrument on the tripod in any required position. The Solar Compass has two main plates, seen at a. and b.—a. is the upper and b. the under plate, the latter is that on which the compass sights cc. are attached by screws and steady pins. This plate revolves underneath the upper plate on a conical centre piece, and may be clamped to it at any required angle by two clamps, one of which is seen at p. There is, also, an inlaid silver ring on the under plate, divided into half degrees, which is covered by the upper plate, except at two openings at opposite points, with a vernier attached to each, d. d. Upon the upper plate is attached a needle-box, e, by a conical centre piece below the cap of the needle q. This needle has an arc of about 36°, divided into halves, for its north end only. A lever, r, is to raise the needle from its pivot when not in use.



The needle-box has a limb extending at right angles from its centre, which is not seen in the plate. At the end of this limb is a vernier and arc to set off the needle's variation; the tangent screw to this limb and vernier is seen between k and d. In consequence of the imperfection of magnetic needles, the arc is attached to the upper plate by two screws, and made adjustable, so that all instruments of this kind can be made to read the same magnetic variation. On the upper plate two adjustable spirit levels are placed at right angles to each other, for the purpose of adjusting the instrument to a true level, when an observation is made on any celestial object. The edge of the upper plate is divided to every five degrees of a circle; and in its centre is placed a brass pin, rising a little above the needle-box; by this arrangement, the surveyor can readily see the approximate course of any object in view, without turning the sights in its direction.

Together with the foregoing described parts, on the upper plate is placed the solar apparatus, which is attached to it by two small blocks, fastened by screws and steady pins, one of which is seen at y. Into each of these blocks one axis of the latitude arc g enters. These axes are connected by the hour arc i and two radial arms z zfrom its centre at s. From this centre of the hour arc, a curvilinear arm extends to the latitude arc g. The latitude arc moves in a grooved arc to which its vernier t is attached. The grooved arc is fastened to the compass plate by a flange at its base, and two screws. The latitude arc g has a radius of about five inches, and is divided into quarter degrees, and its vernier t reads these divisions to minutes. The latitude arc is clamped at any required latitude, by a clamp screw on the back side, not seen on the plate. The hour arc i, as above stated, lies between, and connects the axes of the latitude arc: it is only a portion of the hour circle, and is divided to half de-This arc gives the hour angle of celestial objects within the Zodiac of about 55° or 60° east and west of the meridian.

The revolving limb v, with its declination arc h, is mounted on the centre of the hour arc, and has a free motion on its conical spindle or axis, within the conical socket s, at the lower end of which is a collar and screw, for the purpose of giving a suitable tenseness to its movement. This is called the polar axis.

In connexion with the revolving limb is another moveable limb x, attached to it by a short conical centre at l; the other end with its vernier m, moves over the declination arc h, and is clamped to it at

any required declination, by a clamp screw on the back side of the arc. This arc has about the same radius, and the same divisions and vernier as the latitude arc.

A small brass plate is attached by screws to each end of the limb x, standing out at right angles from the limb; and into the upper half of one plate, and the lower half of the other, is set a small convex lens, as seen at o o, called the solar lenses; and on the opposite brass plate to each lens, is attached a small adjustable silver plate by means of three screws. On each of these silver plates two sets of parallel lines are drawn, crossing each other at right angles, at a suitable distance apart to embrace the sun's image, which falls between them from the lens.

The set of lines which are parallel to the hour are are called the equatorial lines, and the set which are vertical to the hour are are called the hour lines. On the upper edge of each brass plate above named, is placed an equatorial sight w w, which can be attached or detached at pleasure, by means of small thumb screws.

There is also another limb (not seen in the plate) called an adjuster, which can be substituted in the place occupied by the limb x, for the purpose of adjusting to a parallelism with the lenses, the equatorial lines on the silver plates. It is a brass bar about six inches long, and one-fourth of an inch thick, with a plane surface, and three small pins at each end. The pins are for the purpose of keeping the limb x, when on the adjuster, in its place.

The adjuster when used must be attached to the same place occupied by the  $\lim x$ , with the same centre and screws that held the latter. (See second adjustment.)

# PRINCIPLES OF THE SOLAR COMPASS BRIEFLY EXPLAINED.

Where a solar compass is correctly adjusted in all its parts, and also to the latitude and meridian of the place of observation, with its vernier m, of the declination are clamped at 0, or zero, then the polar axis s, of the instrument, will be parallel to the axis of the earth, and the moveable limb x, with its lenses and equatorial sights, will consequently be at right angles to the polar axis, and will revolve on this axis parallel to the plane of the equator; therefore, it

is clear that this motion coincides with the diurnal motion of any heavenly body that has no declination, and it is equally clear, that this coincidence holds good when a celestial object has north or south declination, if its declination be set off on the declination are of the instrument; for, the diurnal motion of the heavenly object will be like the motion of the moveable limb x, parallel to the equator and equidistant from it. Now if the instrument be turned horizontally out of the meridian, the polar axis will not be parallel to the axis of the earth, nor will the moveable limb x revolve parallel to the equator; consequently it will not follow the diurnal motion of any heavenly body; therefore, if the sun's declination be set off on the declination are, the sun's image from the lens will not fall between the equatorial lines on the silver plate, but will fall above or below them, and will not fall between them until the compass is turned again into the true meridian.

It is from these principles of the solar compass that the true meridian is obtained, and the variation of the needle determined, etc.

#### ADJUSTMENTS OF THE SOLAR COMPASS.

Before using the solar compass it must be correctly adjusted. This consists in bringing its different parts to their proper place, and in determining the index errors of the instrument in its graduated arcs, which is chiefly done by reversals and adjusting screws.

#### FIRST ADJUSTMENT.

To adjust the two spirit levels k k, to a horizontal movement of the instrument on its lower axis.

Place the compass on the tripod, and level it, or nearly so, with the hand, then by means of the levelling screws at the lower end of the ball and socket, bring the bubble in each level to the middle of its opening. If the bubbles do not move while the compass is turned horizontally around on its lower axis, this adjustment is right; but if they move, the levels must be adjusted by the screws at the end of each for that purpose, until the bubbles will remain stationary while the instrument is turned horizontally around.

#### SECOND ADJUSTMENT.

To make the solar lenses and the equatorial lines on their opposite plates parallel to each other.

Detach the limb x, by taking out its fastening screws, and attach the adjuster in its place, with the same screws that held the limb; then clamp it at the moveable end, to the sun's declination as near as practicable. Now let the compass be placed on the tripod where the sun shines, and level it, with the sights north and south, or nearly so; then place the limb x on the adjuster, between the pins, the same side up that was upon the compass, and then bring it to bear on the sun as in other observations, and turn the compass horizontally, if necessary to bring the sun's image precisely between the equatorial lines on the silver plate; now, without moving the compass in the least out of level, or otherwise, take the limb x from the adjuster and turn the upper side down, without changing ends, and place it on the adjuster again; then see if the sun's image falls between the equatorial lines as before. If it does, this plate is in adjustment; but if it does not, loosen the three small screws which hold the silver plate, (having oblong holes under their heads,) and move this plate one-half of the observed difference, up or down as the case requires, and lightly tighten the screws again. these observations and adjustments, as above described, until the sun's image falls precisely between the equatorial lines, either side This plate then will be in correct adjustment.

Now reverse the ends of the limb x, and adjust the other silver plate in the same manner as the first. When this is done, the parallelism of the lenses and equatorial lines are as perfect as reversals will make them, and the equatorial sights are also parallel to these. The adjuster may now be taken off and the limb x returned to its place. It will not be necessary to repeat this adjustment unless the silver plates get moved by accident or otherwise. The best time to make these adjustments, is between the hours of 10 A. M. and 2 P. M.

In making this adjustment the  $\limsup x$  should fit accurately on the adjuster, and the brass plates in which the lenses are set must be precisely of the same breadth; if they are not, this adjustment cannot be correctly made. Therefore, these plates should be carefully tried with a gauge, and any difference in size corrected.

#### THIRD ADJUSTMENT.

To find the index error of the declination arc.

#### FIRST METHOD.

Set the vernier m of the declination arc h at 0, or zero, place the compass on the tripod, and incline it north or south, as the sun may have north or south declination, until the sun's image falls precisely between the equatorial lines on the silver plate; then reverse the lenses by turning the revolving limb half way around, and see if the sun's image falls precisely between the equatorial lines on the other silver plate; if it does, there is no index error in this arc; but if it does not, move the limb x up or down, as the case requires, on the declination are one-half of the observed difference, and try the reversals again, and so repeat them, if necessary, until the sun's image falls precisely between the equatorial lines on both silver plates. The amount of index error in this arc can now be read by its vernier If the index error is below the graduated zero point on the declination are, its amount must be subtracted from the declination of the celestial object, before it is set off on the declination arc; but if above, it must be added.

#### SECOND METHOD.

Set the vernier m of the declination are h at zero, as before, and bring the equatorial sights to bear on some distant object; then, without moving the compass in the least, reverse the revolving limb v, and see if the line of sight is the same as before; if it is, there is no index error; but if not, proceed as described, by reversals on the sun, until the equatorial sights will bear on the same objects when reversed.

#### FOURTH ADJUSTMENT.

To bring the polar axis to a right angle with the axis of the latitude arc.

This adjustment generally is, and always should be made by the instrument maker, but the surveyor should test his instrument in all of its parts. First detach the solar apparatus from the upper plate, by taking out the clamp screw of the latitude arc, and the screws that fasten its axis and blocks to the upper plate; then take a piece of board about four inches wide and a foot long, with smooth edges, and nail one edge to another board about one foot square, so that

it will be at right angles to its surface. Place this on a stand or table, in a convenient place to view some distant object, then take the blocks that hold the axes of the latitude arc, and place them on their axes, and fasten them by their screws to the upper edge of the narrow board; by this arrangement the polar axis s can be brought to a perpendicular, and then reversed, by giving motion to the axes of the latitude arc of 180°.

The moveable limb x must now be clamped to its true zero point, as found by the third adjustment, and the polar axis s brought to a perpendicular; the revolving limb v must now be turned parallel to the axis of the latitude arc; then observe some distant object through the equatorial sights; now reverse the polar axis as above directed, and see if the equatorial sights bear on the same object as before reversing the polar axis; if they do, the polar axis is at right angles to the axis of the latitude arc; but if not, the face of the flange, or the seat of the conical socket s, must be ground on one side enough to correct this error, so that the equatorial sights will bear on the same object when reversed as above stated. If the error be small, it may be corrected by placing a thin piece of tin foil, or some other firm substance, under one side of the flange of the conical socket s.

#### FIFTH ADJUSTMENT.

To make the compass sights coincide with the true meridian, when an observation is made with the solar compass.

Place the compass on the tripod, and clamp the sights to an east, west course; then take out the clamp screw to the latitude arc, and raise this arc until the polar axis s is horizontal, or nearly so, and fasten it in this position, which can be easily done by placing a small wedging piece of wood between the edge of the hour arc and the upper plate of the compass, and a small brace of wood between the brass centre pin and the conical centre s of the hour arc. Then clamp the vernier m of the declination arc at its true zero point, as found by the third adjustment. Now bring the equatorial sights to bear on some distant object in or near the horizon; then unclamp the main plates a and b, and bring the compass sights to bear on the same distant object; (it is well to reverse the equatorial sights and make the same observation again;) if both sights still coincide, read at the verniers d d, the amount of the index error, if any, between these plates.

This adjustment should always be made by the instrument maker, and cleared of index error, by a proper adjustment of the compass sights on the lower plate. But if any index error is found in the instrument, while in the hands of the surveyor, it should be allowed for in all courses run by him, or he may correct it by removing one of the compass sights the required amount so as to make the line of sight to coincide with the meridian. This can be done by enlarging, with a small round file, the holes on one side of the steady pins and screw that hold the compass sight to the lower plate, enough to correct the index error. The vacancy on the side of the steady pins may be filled with tin foil, or some other substance that is not magnetic.

#### SIXTH ADJUSTMENT.

To find the index error of the latitude arc.

This is most correctly done by determining the latitude of any station by north and south stars, or, determine the latitude by the sun, and again by the pole star; (see article, "Latitude by the Solar Compass;") one-half of the difference of latitude thus found, if any, is the index error of this arc. If the latitude determined by an observation on the sun, or star within the zodiac, be less than the latitude by the north star, the half difference must be added to the zodiacal observation, to obtain the true latitude of the station; but if greater, it must be subtracted. But this index error is not used for any other purpose than to find the true latitude, for the latitude given by an observation on a celestial object within the zodiac, is the latitude to be used for all other purposes.

#### SEVENTH ADJUSTMENT.

To find the index error of the hour arc.

Adjust and clamp the compass sights to the true meridian, as directed in the remarks to find the meridian, variation of the needle, &c.; also, set a stake in the meridian, four or five chains south of the instrument, and keep the compass sights directed to it. Then at the distance of ten or twelve feet south of the instrument, suspend a plumb line from the top of a suitably inclined pole set in the ground, and firmly supported with crotches, and of a sufficient height to observe, near the top of the line, the meridian passage of the sun. Then with the aid of a suitable dark glass, observe through the north sight vane, the meridian contact of the sun's west limb with

the line, while an assistant has kept the sun's image accurately between the hour lines on the silver plate. At this point, read on the graduated side of the declination are, at either end of the revolving limb, its distance from the graduated zero point, and the same again with the last contact of the sun's east limb: half the difference on the hour are, between these two observations, will be its true zero point; from which read the index error.

It should be remarked here, that the principles of the solar compass have been applied in various ways to surveying instruments. to suit the views of mathematical instrument makers, or surveyors for whom they were made; but the solar compass described in the foregoing pages, and for which the adjustments are given, has been found, after much experience in its use, to be the best adapted to surveying the public lands, and for this purpose it is generally used; for the reason that it is more safely and conveniently carried and used through all the exposures which are unavoidable in the wilder-Some change, however, may be made in its mechanical construction, for the purpose of city surveying, and for running the lines and curves of railroads, etc. But in whatever form they may be made, it is important to a good solar apparatus, that the latitude and declination arcs have a radius not less than five inches, so that their divisions may be sufficiently large to be easily read, and the arcs readily and accurately adjusted for use. The importance of this will be understood by considering the frequency of these adjustments, and the circumstances under which they are made while running lines in the field. So far as known to the author, but few surveyors have qualified themselves to use the solar compass on any other celestial object than the sun; and, perhaps, as few have fully understood its principles and adjustments. The reason of this is found in the fact, that no work has been published before this, sufficiently elucidating its principles, adjustments and use. The sun is the principal celestial object used in surveying lines with this instrument, which only requires a knowledge of the true declination of the sun for each hour of the day, in the longitude where the survey is to be Therefore, with the instructions here given, no accomplished surveyor with the magnetic compass, need hesitate to use the solar compass on the sun; and he will soon acquire the further knowledge of using it on other heavenly bodies at night, to determine the variation of the needle, and for other purposes treated of in this work. If the solar compass has been truly adjusted in all of its parts, previous to its being used in the field, the surveyor may feel the fullest confidence in the true course of his lines run with it.

### ASTRONOMY.

Though merely a knowledge of the apparent diurnal motion of the sun in the heavens, will serve for the single purpose of using the solar compass on that luminary; yet, for all the purposes for which this instrument can be employed by night on the planets and fixed stars, a more extended knowledge of astronomy is required.

Therefore, the following brief notice of astronomical facts and phenomena is deemed necessary to be understood by all surveyors, to enable them to use the solar compass to the best advantage.

#### SOLAR SYSTEM.

The sun is the centre of the solar system, around which all the planets revolve in elliptical orbits, from west to east,\* with diminished velocities as their distances increase from the sun: the planes of their orbits are nearly coincident with the plane of the ecliptic; therefore, their greatest declinations will be sometimes more or less than the sun's greatest declination, by the amount of the angle of inclination of each of their orbits to the plane of the ecliptic. See the following table.

Planet's names.	Mean diame- ter in Eng- lish miles.	Mean distance in English miles from the Sun.		of orbit to	
The Sun, Mercury, Venus, The Earth, The Moon, Mars, Jupiter, Saturn, Uranus, Neptune,	883,246 3,224 7,687 7,912 2,160 4,189 89,170 79,042 35,112 35,000	37.000.000 68.000.000 95.000.000 95.000.000 142.000.000 495.000.000 906.000.000 1.820.000.000 3.600.000.000	87.969.225 224.700.787 365.256.361 27.321.661 686.979.646 4.332.584.821 10.759.219.817 30.686.820.830 60.128.000.000	7° 0\ 9".1 3°23\28".5 5° 8\47".9 1°51\ 6".2 1°18\51\"3 2°29\35".7 0°46\28".4	109.400 80.060 68.080 2.290 55.000 28.000 20.000 15.000

<sup>\*</sup>East and west are relative, or local terms. It is meant here, that they move in their orbits around the sun, in the same direction as the opposite side of the earth from the sun moves around its axis.



#### THE EARTH.

The earth is an oblate spheroid, whose equatorial diameter exceeds its polar diameter about 26 miles; the cause of this difference is supposed to be the centrifugal force of the earth's rotary motion around its axis.

The north and south poles of the earth are two points on its surface, opposite to each other; and a straight line between these two points is called the axis of the earth, around which the earth revolves, from west to east, once in a sidereal day.

The axis of the earth is always inclined from a perpendicular to the plane of its orbit; in other words, the axis of the earth has an angle to the axis of the ecliptic, of about 23° 28′. Therefore, the axis of the earth is always in the same direction in regard to the heavens, in every part of its orbit.

This angle of inclination causes the declination of the sun north and south of the celestial equator, during each revolution of the earth around the sun. It is, also, the principal cause of the declinations of the planets; the different seasons of the year; and the different length of days and nights.

#### EQUATOR.

The Equator encircles the earth at right angles to the axis, and is equidistant, or 90° from its poles; its plane divides the earth into two equal parts, called northern and southern hemispheres.

The plane of the equator, if extended to the heavens, is called the celestial equator, which has an angle to the plane of the ecliptic, (like the angle between their axes) of about 23° 28′.

The motion of the earth around its axis is uniform; but the velocity of the earth in its orbit around the sun is unequal, the mean of which is 59'8" each day. The sun will therefore return to any given meridian each day in unequal times; hence the difference between apparent and mean time, called the equation of time.

A tropical year is 365 d., 5 h., 48 m., 49 s. A sidereal year, reckoned in mean solar time, is 365 d., 6 h., 9 m., 9. 6s., and reckoned in sidereal time, is 366 d., 6 h., 9 m., 9. 6s.

The reason of this difference is; the earth has moved once around the sun in its orbit the same way the equator moves around its own axis. The earth must therefore complete one revolution and 59' 8' on its axis each day, to bring the sun to the same meridian This is called solar time.

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The earth has precisely one revolution on its axis from the transit of a fixed star to the next transit of the same star, which is a sidereal day of 24 hours; but, if reckoned in mean solar time, it is 23 h., 56 m., 4 s., 9".

An astronomical day commences at noon, and is reckoned from one to 24 hours successively; the civil day commences at the preceding midnight, and is reckoned from 1 to 12 hours, twice in a civi day: therefore the last 12 hours of the civil day correspond to the first 12 hours of the astronomical day. All astronomical calculations are computed in astronomical time.

#### LATITUDE.

Latitude on the earth is reckoned north and south of the equator in degrees, etc., of the meridian, to the poles (or 90°.) Difference of latitude is an arc of the meridian, between any two parallels of latitude.

#### LONGITUDE.

Longitude on the earth is reckoned east and west from any prime meridian, in arc or time to 180° or 12 hours. Difference of longitude is the difference in arc or time, between any two meridians, reckoned on any parallel of latitude.

#### ECLIPTIC.

The Ecliptic is a great circle of the heavens, and its plane is the extension of the plane of the earth's orbit, indefinitely, into space, or the starry heavens.

The sun is always in the ecliptic, and the orbits of all the planets cut or intersect the ecliptic at opposite points, called their nodes, in which only eclipses occur.

#### ZODIAC.

The Zodiac is an imaginary belt or circle of the heavens, and occupies a space of 8° on each side of the ecliptic; within which all the planets appear to perform their revolutions around the sun.

#### DECLINATION.

Declination of a heavenly body is reckoned north and south of the equatorial plane. The complement of the declination of a celestial object is its nearest polar distance.



#### RIGHT ASCENSION.

The right ascension of heavenly bodies is reckoned in time from the first point of Aries, or the vernal equinox, around in the order of the signs, on the equator, to the same point again. The longitude of heavenly bodies is reckoned from the same point, and in the same order on the ecliptic, in degrees, etc., as right ascension is reckoned in time on the equator.

#### ALTITUDE AND ZENITH DISTANCE.

The altitude of a celestial object is the angle in which it is observed above the horizon. The zenith distance of a heavenly body is its angular distance from the zenith, or point directly over head of the observer.

#### HORIZON.

An observer has two horizons, the sensible and rational. The sensible horizon is a circle at the extent of view in all directions, on a horizontal plain, or on the ocean. The plane of the rational horizon divides the earth into two equal parts through its centre, parallel to the sensible horizon; it is, therefore, the semi-diameter of the earth below the sensible horizon.

#### REFRACTION AND PARALLAX.

The atmospheric refraction causes a heavenly body to appear above its true place in the heavens, except it be in the zenith. The parallax of a celestial object is the difference in altitude that would appear between an observation made from any point on the earth's surface and from its centre. Therefore, parallax causes heavenly bodies to appear below their true place in the heavens, except they are in the zenith; hence the corrections for parallax and refraction of instrumental observations on celestial objects.

#### AZIMUTH.

The azimuth of a heavenly body is reckoned on the horizon of the observer, between a vertical plane of the meridian, and another vertical plane passing through the centre of the celestial object, to the zenith of the observer. In other words, it is the true bearing of a heavenly body referred to the horizon from the meridian.



Azimuths are generally reckoned from the north in north latitude, and from the south in south latitude.

The amplitude of a heavenly body is its true course or bearing at rising or setting, from the east or west points of the horizon.

#### NAUTICAL ALMANAC.

Blunt's Nautical Almanac and Astronomical Ephemeris, (on account of its size) is the most convenient that has yet been published for the surveyor to take data from, for the use of the solar compass. The heading of each page and column is a sufficient explanation of its contents and use.

This almanae is adapted to mean noon at Greenwich, England, except the sun's declination, which is more properly given for apparent noon.

It will be seen that the quantities in the columns are continually varying from day to day; therefore some reduction is necessary to adapt them to any other time or longitude, than that for which they were registered. This is accomplished by applying the hourly differences, where they are given, according to their sign or precept; and where the hourly differences are not given, take the required proportional part of the difference between the preceding and succeeding noon at Greenwich, and add to or subtract from the registered quantities, according as they are increasing or decreasing, as the case requires.

#### FIXED STARS.

The following table of the mean places of 35 fixed stars has been selected from the Nautical Almanac, for January 1st, 1854, for the purpose of night observation with the solar compass. The sign + prefixed to an annual variation is to be added to, and the sign — is to be subtracted from the right ascension: also, for stars having north declination, + signifies add, and — subtract; but for stars of south declination + denotes that the variation is to be subtracted from, and — that it is to be added to the declination.

FIXED STARS.

MEAN PLACES OF THIRTY-FIVE PRINCIPAL FIXED STARS
FOR JANUARY 1st, 1854.

#### LATITUDE BY THE SOLAR COMPASS.

After the solar compass has been correctly adjusted in all of its parts, its future usefulness depends upon finding the latitude as given by the instrument, at the place where it is used.

That it may not be repeated again, hereafter, it should be remarked, that in all observations with the solar compass, it must be placed on the tripod, and accurately levelled, with the latitude are turned toward the equator; except, that when making an observation on

the pole-star, it must be turned in that direction. This can be done approximately by the magnetic needle.

Thus prepared, set off the sun's declination for noon on the declination are, allowing for its index error, if any, and the sun's meridional refraction, also, adjust the latitude are approximately to the latitude of the place, and the revolving limb v. at its true zero point on the hour are i.: in other words, for noon.

Commence the observation for latitude about fifteen minutes before the sun culminates, by turning the instrument horizontally on its lower axis, so that the sun's image will fall between the hour lines on the silver plate, and raise or lower the latitude arc, if necessary, to bring the sun's image between the equatorial lines. Then follow the motion of the sun, by turning the compass horizontally, at short intervals of time, and adjust the latitude arc, to keep the sun's image between the equatorial lines, until he culminates. The latitude of the station can then be read at the vernier of the latitude arc.

The same method may be pursued by night to determine the latitude by an observation on any celestial object within the zodiac, viewed through the equatorial sights. In making these observations, it will sometimes be necessary for an assistant to hold a lighted candle a little behind and above the head of the observer, in such a manner that the equatorial sights can be seen; but not so bright as to obscure the star.

#### LATITUDE BY THE POLE-STAR.

It should be remarked, that the latitude given by an observation on any heavenly body within the zodiac, is read direct on the latitude arc; but when the latitude arc is turned to the north for an observation on the pole-star, or some other star near the pole, the latitude arc will read the co-latitude of the station; it must, therefore, be subtracted from 90° to obtain the true latitude. In these latter observations, the polar distance of the star must be set off on the declination arc instead of its declination, and if the upper meridian passage of the star be observed, the declination arc must be turned toward it; but, if the lower meridian passage of the star be observed, the declination arc must be turned from the star.

See sixth adjustment to find the index error of the latitude arc.



EASTERN ELONGATIONS OF POLARIS.

DAYS.	APRIL.	MAY.	JUNE.	July.	August.	SEPT.
1 7 13 19 25	н. м. 18·18 17·56 17·34 17·12 16·49	H. M. 16·26 16·03 15·40 15·17 14·53	н. м. 14·24 14·00 13·35 13·10 12·45	H. M. 12·20 11·55 11·31 11·07 10·43	H. M. 10·16 9·53 9·30 9·08 8·45	H. M. 8·20 7·58 7·36 7·15 6·53

WESTERN ELONGATIONS OF POLARIS.

DAYS.	Oct.	Nov.	DEC.	JAN.	FEB.	March.
1 7, 13 19 25	H. M. 18·18 17·56 17·34 17·12 16·49	H. M. 16·22 15·59 15·35 15·10 14·45	H. M. 14·19 13·53 13·27 13·00 12·34	H. M. 12·02 11·36 11·10 10·44 10·18	H. M. 9·50 9·26 9·02 8·39 8·16	н. м. 8·01 7·38 7·16 6·54 6·33

To find the time of the meridian passages of the pole star, add 5 hr. 59 min. to the time of its elongation.

# TO FIND THE TRUE MERIDIAN, AND HORIZONTAL ANGLES FROM IT; ALSO, THE VARIATION OF THE NEEDLE.

Clamp the sight of the compass at 0 or zero, and adjust the latitude arc to the latitude of the place; also, set off the sun's declination for the time of day, allowing for index error, if any, and the sun's meridional refraction; then bring the sights of the compass approximately into the meridian by the needle, and the solar lenses into the direction of the sun; if the sun's image does not fall between the equatorial lines, turn the instrument horizontally, and the revolving limb v. on its axis, in a manner to bring the sun's image between the equatorial lines, allowing for refraction, if required; then the compass sights will be in the true meridian. Now if the needle q, be lowered on to its pivot by the lever r, its variation from the true meridian can be read, and set off on the arc for that purpose; the tangent serew of the vernier limb is seen at k. and d. (See Plate 1.)

To set the sights of the compass to any other course or angle from the meridian it is only necessary to unclamp the under plate from the upper, and turn the sights to the course required, the angle of which can be read at the verniers d. d.

Observations for the same purpose can be made in the night, on any celestial object within the zodiac, by the use of the equatorial sights, instead of the lenses; and by observing two stars, one east, and the other west of the meridian, the variation of the needle, or the course of a line, may be more accurately defined.

#### ZENITH DISTANCE AND ALTITUDE.

Clamp the compass sights to  $90^{\circ}$ , or for an E. and W. course, also, set off on the declination are 23 degrees, and bring the revolving limb v to zero or noon on the hour are. Then by turning the instrument horizontally on its lower axis, bring the solar lenses and equatorial sights into the direction of the sun or star to be observed, and raise or lower the latitude are as the case requires, until the sun's image falls between the equatorial lines, or the star is seen through the equatorial sights. If the observation be made with the declination are turned from the object, 23 degrees must be added to the reading of the latitude are, to obtain the zenith distance of the object observed; but if the declination are is turned toward the object, 23 degrees must be subtracted from the reading of the latitude are, to obtain the zenith distance.

If the zenith distance be subtracted from 90 degrees, the altitude of the object will be had.

#### TIME OF DAY BY THE SUN.

After an observation is made to determine the variation of the needle, or the course of a line by the sun, bring the revolving limb to one division on the hour are in advance of the sun, then observe the movement of the sun's image to the instant it arrives between the hour lines, and correct for index error of the hour arc, and the effects of refraction, and the hour angle from the meridian at that time, expressed in degrees will be had, which may be converted into time by allowing 15 degrees for an hour, and for each degree four minutes of time. If mean time is required, add or subtract the equation of time according to its precept, and mean time will be had.

#### DIURNAL VARIATION OF THE NEEDLE.

It has been found by numerous observations, that the diurnal variation of the needle is more in summer than in winter months, and the amount of these aberrations is more or less on different days of the same season of the year, and is probably caused by heat and cold.

But the order in which these diurnal changes take place, can be a little more clearly defined. The north end of the needle will arrive at its most easterly declination between one and two hours after sunrise. It will soon after gradually decline westerly until one or two o'clock, P. M., soon after which it will decline eastward, and at sunset it will have returned half way back to where it was in the morning. Its daily movement may be better understood by an examination of the following table:—

July. 5½ A. M. 6664669THERMOMETER. 1 P. M. 6½ P.M. 77866677777788666762 WEATHER. clear, clear, clear, clear, clear, clear, clear, clear, rain, clear, cloudy cloudy A.M light showers, flying clouds, some. cloudy, clear, some cloudy flying clouds, ight showers WEATHER. clear,
clear,
clear,
cloudy,
shower,
clear,
clear,
showers; cloudy, cloudy, ĸ West. WIND. A.M. MAGNETIC VARIATION. 1 P.M. 61/2 P. M. 

The following observations were made by the author in latitude 42 degrees 42 minutes North, near Detroit, in July, 1839.

It will be seen that the average variation for eighteen days at 5 h., 30 m., A. M., is 1° 39′ 50′′, E. at 1 h., 00 m., P. M., is 1° 25′ 37′′, E. at 6 h., 30 m., P. M., is 1° 33′ 23′′, E.

The difference of these numbers gives the diurnal variation as follows:—

Between morning and evening—6' 27", Between morning and noon—14' 13", Between noon and evening—7' 46".

From these facts it may be seen, that the variation of the needle, as found at one time, cannot be safely relied upon in running lines at any length of time subsequently. Hence the importance of finding its variation at the time the line is being run.

To guard against errors occurring on account of the variation, the surveyor should at the end of each line, or at the point where the variation of the needle is found, for the purpose of running a line from it at some future time, take the bearing of some distant object, and make a note of the same. On resuming the work, if the sun should be obscured by clouds so as to prevent finding the variation of the needle, he can observe the course of the same object again, and the difference in its course, if any, is the change of variation, and must be allowed for to correct the variation previously determined.

Local attraction, also, so frequently changes the direction of the needle, that the surveyor cannot safely extend his line far without an observation to find its variation; and it will be frequently found that a little delay for this purpose, will more than compensate for all the supposed advantages of running the line without it.

## TO FIND THE MERIDIAN PASSAGE OF A FIXED STAR, AND ITS HOUR ANGLE AT ANY HOUR OF THE DAY.

Subtract the sun's Right Ascension for the day and hour of observation, from the star's Right Ascension, borrowing 24 hours for the latter when necessary, and the difference will give the star's meridian passage in solar time; if mean time be required, add to or subtract from the solar time, the equation of time, according to its precept, and the meridian passage of the star will be given sufficiently near for that purpose. Then, if the hour of observation, (astronomical time) can be subtracted from the time of the star's meridian passage, the star's hour angle, east of the meridian will be

given; but if the meridian passage of the star be subtracted from the hour of observation, it will give its hour angle, west of the meridian. And thus it may be determined what stars are most favourably situated, for the purpose of finding the variation of the needle, at any time of night.

If any one of the fixed stars named in the preceding table are not truly known to the observer by the geography of the heavens, it is necessary to find the time of meridian passage in order to know the star's hour angle at the time of the proposed observation.

This being known, set the instrument to the star's declination and the equatorial sights to the hour angle of the star, on the hour are, then bring the sights of the compass into the meridian as near as may be by the needle; the equatorial sights will then direct the eye, nearly, to the star sought for, and by a little movement of the instrument horizontally on its lower axis, bring the line of sight to bear directly on the star, and the observation is complete.

# THE EFFECT OF REFRACTION AND PARALLAX IN THE USE OF THE SOLAR COMPASS EXPLAINED.

The equatorial and hour lines of the solar compass will vary their angles from the horizon, as the object observed by the instrument recedes from, or approaches to the meridian of the observer; and when at 90°, or six hours from the meridian, the equatorial lines will have an angle to the horizon, equal to the co-latitude, and the hour lines equal to the latitude of the place of observation. Now if the equatorial lines were at all times in a vertical plane, passing through the centre of the celestial object, refraction would not produce any effect in the course of lines run with the solar compass; but as they will have an angle, as above stated, at different hours of the day, a proportion of the whole amount of refraction, according to the angle, must be allowed for, when large enough to produce a sensible effect in the course of the lines. The equatorial lines are parallel to the horizon when observing a celestial object on the meridian; therefore, the whole amount of the meridional refraction must be allowed for, in setting off its declination. The hour lines are only affected by the whole amount of the refraction, or parallax, when on the equator, or latitude 0°.

The effect of parallax of the sun and large planets, is too small to be regarded, except in the most refined observations. But the parallax of the moon is too large to be neglected in any; for this reason, a table of refraction in altitude is given in this work.

Refraction does not decrease in regular proportion to the altitude of the object. When a celestial object is in the zenith, it has no refraction or parallax; but when it is in the horizon, its refraction is 33′51″, and at an altitude of 45° about one minute, (more exactly 58″;) the natural co-tangent of the altitude of a heavenly body, express nearly its refraction.

For the purpose of determining with facility the whole amount of refraction in altitude of a celestial object, the compass sights have lines drawn across them at various distances from the top; at each of these lines are figures, which indicate, in minutes of a degree, the amount of refraction in altitude of a celestial object, as seen from each line in range with the top of the other sight.

From the amount of refraction thus found, subtract the meridional refraction, then the following table will give the proportion of the remainder, expressed in hundredths, to be added to its declination, when the latitude is of the same name; or subtracted from it, when of a contrary name, from one to six hours in time, east and west of the meridian; also, the proportion of the whole amount of the sun's refraction, to be subtracted in time from his hour arc, in the forencon, and added to it in the afternoon, to obtain the true apparent time. This table will also be useful in observations on the Moon; for the same proportion of the moon's parallax in altitude, must be allowed for on the declination arc, in a reversed order from that of refraction; in other words, the same proportion of the moon's parallax in altitude, corrected for refraction, (see table for that purpose) must be subtracted from her declination, when the latitude is of the same name, and added to it, when of a contrary name.

For the purpose of making corrections for refraction expeditiously, while running lines by the sun, there are three lines drawn below the equatorial lines, 5' apart, by which to estimate the proportion of refraction to be allowed, by bringing the lower limb of the sun's image the number of minutes below the lower equatorial line on the silver plate, instead of setting it off with the sun's declination. When the surveyor becomes familiarly acquainted with making these allowances for refraction, in using the solar compass, he will seldom need to refer to the tables, or to mathematical calculations, to enable him to make a proper allowance for refraction at all hours of



the day, except when the sun is within 5° of the horizon. But for an observation by night on a star, its refraction should be set off with its declination, in the manner before stated.

PROPORTION OF REFRACTION TO BE ALLOWED IN HUNDREDTHS
OF THE WHOLE.

ON THE EQUATORIAL LINES.						ON THE HOUR ARC.						
HOURS FROM THE MERIDIAN.						HOURS FROM THE MERIDIAN.						
Ļat.	1 н.	2 н.	3 н.	4 н.	5 н.	6 н.	1 н.	2 н.	3 н.	4 н.	5 н.	6 н.
10°	97	87	72	52	31	17	26	49	70	85	95	98
120	97	87	72	53	33	21	25	49	69	85	95	98
140	97	87	73	53	35	24	25	48	69	85	94	97
160	97	88	73	55	36	28	25	48	68	83	93	96
18°	97	88	74	57	39	31	25	48	67	82	92	95
20°	97	88	75	58	42	34	24	47	67	81	91	94
220	97	89	75	59	45	37	24	46	66	80	89	93
240	97	89	76	61	47	41	23	46	65	79	88	91
260	97	89	77	63	50	44	23	45	64	78	87	90
28°	97	90	78	65	52	47	23	44	63	76	85	88
30°	97	90	79	66	55	50	22	43	61	75	84	87
32°	98	91	80	68	57	53	22	42	60	73	82	85
340	.98	91	81	71	60	56	22	42	59	71	80	83
360	98	92	82	71	62	59	21	40	57	70	78	81
380	98	92	83	73	65	62	20	39	56	68	76	79
400	98	92	84	75	67	64	20	38	54	66	74	77
420	98	93	85	77	69	67	19	37	53	64	72	74
440	98	93	86	78	72	69	19	36	51	62	69	72
460	98	93	87	80	74	72	18	36	49	60	67	69
480	98	94	89	81	76	74	18	33	46	58	65	67
500	99	95	89	83	78	77	17	32	45	56	62	64
520	99	95	90	85	80	79	16	31	43	53	59	62
540	99	96	91	86	82	81	15	29	42	51	57	59
560	99	96	92	87	84	83	14	28	39	48	54	56
580	. 99	96	93	89	86	85	14	26	37	47	51	53
60°	99	97	94	90	87	87	13	25	35	43	48	50

# DR. YOUNG'S REFRACTIONS.

The Barometer being at 30 inches, and the *internal* Thermometer at 50, or the *external* at 47 degrees, with the correction for +1 inch in the Barometer, and for -1 degree in the Thermometer of Farenheit.

App. Alt.	Refr. B. 30. Th. 50°.	Diff. for + 1 B.	Diff. for — 1° Fa.	App. Alt.	Refr. B. 30. Th. 50°.	Diff. for + 1 B.	Diff. for — 1º Fa.	App. Alt.	Refr. B. 30. Th. 50°.	Diff. for + 1 B.	Diff. for — 1° Fa.
0 0 5 10 15 20 25	/ " 33·51 32·53 31·58 31·5 30·13 29·24	74 71 69 67 65 63	8·1 7·6 7·3 7·0 6·7 6·4	3· 0 5 10 15 20 25	/ // 14:35 14:19 14: 4 13:50 13:35 13:21	30 29 29 28 28 27	" 2:3 2:2 2:2 2:1 2:1 2:0	8 0 10 20 30 40 50	6.35 6.28 6.21 6.14 6.7 6.0	" 13·3 13·1 12·8 12·6 12·3 12·1	85 83 82 80 79
30 35 40 45 50 55	28·37 27·51 27·6 26·24 25·43 25·3	61 59 58 56 56 55 53	6·1 5·9 5·6 5·4 5·1 4·9	30 35 40 45 50 55	13· 7 12·53 12·41 12·28 12·16 12· 3	27 26 26 26 25 25 25	2·0 2·0 1·9 1·9 1·9 1·8	9· 0 10 20 30 40 50	5·54 5·47 5·41 5·36 5·30 5·25	11·9 11·7 11·5 11·3 11·1 11·0	76 74 73 72 71 70
1. 0	24·25	52	4·7	$ \begin{array}{ c c } \hline 4 \cdot 0 \\ 10 \\ 20 \\ 30 \\ 40 \\ 50 \end{array} $	11·52	24·1	1·70	10· 0	5·20	10·8	·69
5	23·48	50	4·6		11·30	23·4	1·64	10	5·15	10·6	·67
10	23·13	49	4·6		11·10	22·7	1·58	20	5·10	10·4	·65
15	22·40	48	4·4		10·50	22·0	1·53	30	5·5	10·2	·64
20	22·8	46	4·2		10·32	21·3	1·48	40	5·0	10·1	·63
25	21·37	45	4·0		10·15	20·7	1·48	50	4·56	9·9	·62
30	21· 7	44	3·9	5· 0	9·58	20·1	1·38	11. 0	4·51	9·8	·60
35	20·38	43	3·8	10	9·42	19·6	1·34	10	4·47	9·6	·59
40	20·10	42	3·6	20	9·27	19·1	1·30	20	4·43	9·5	·58
45	19·43	40	3·5	30 ·	9·11	18·6	1·26	30	4·39	9·4	·57
50	19·17	39	3·4	40	8·58	18·1	1·22	40	4·35	9·2	·56
55	18·52	39	3·3	50	8·45	17·6	1·19	50	4·31	9·1	·55
2· 0	18·29	38	3·2	6· 0	8·32	17·2	1·15	12· 0	4·28·1	9·00	·556
5	18· 5	37	3·1	10	8·20	16·8	1·11	10	4·24·4	8·86	·548
10	17·43	36	3·0	20	8· 9	16·4	1·09	20	4·20·8	8·74	·541
15	17·21	36	2·9	30	7·58	16·0	1·06	30	4·17·3	8·63	·533
20	17· 0	35	2·8	40	7·47	15·7	1·03	40	4·13·9	8·51	·524
25	16·40	34	2·8	50	7·37	15·3	1·00	50	4·10·7	8·41	·517
30	16·21	33	2·7	7· 0	7·27	15·0	•98	13· 0	4· 7·5	8:30	·509
35	16· 2	33	2·7	10	7·17	14·6	•95	10	4· 4·4	8:20	·503
40	15·43	32	2·6	20	7· 8	14·3	•93	20	4· 1·4	8:10	·496
45	15·25	32	2·5	30	6·59	14·1	•91	30	3·58·4	8:00	·490
50	15· 8	31	2·4	40	6·51	13·8	•89	40	3·55·5	7:89	·482
55	14·51	30	3·3	50	6·43	13·5	•87	50	3·52·6	7:79	·476

TABLE OF REFRACTIONS-continuea.

App. Alt.	Refr. B. 30. Th. 50°.	Diff. for +1B.	Diff. for — 1º Fa.	App. Alt.	Refr. B. 30. Th. 50°.	Diff. for +1 B.	Diff. for —1° Fa.	App. Alt.	Refr. B. 30. Th. 50°.	Diff. for +1B.	Diff. for —1° Fa.
0 /	1 "	"	"	0	/ //	"	"	0	1 11	"	"
14.0	3.49.9	7.70	•469	36	1.20.0	2.68	.161	66	25.9	-87	.052
10	3.47.1	7.61	464	37	1.17.1	2.58	.155	67	24.7	.83	.050
20	3.44.4	7.52	·458	38	1.14.4	2.49	.149	68	23.5	.79	047
30	3.41.8	7.43	453	39	1.11.8	2.40	.144	69	22.4	.75	.045
40	3.39.2	7.34	•448	40	1. 9.3	2.32	.139	70	21.2	.71	.043
50	3.36.7	7.26	.444	41	1. 6.9	2.24	.134	71	19.9	•67	.040
15.0	3.34.3	7.18	•439	42	1. 4.6	2.16	·130	72	18.8	•63	.038
30	3.27.3	6.95	.424	43	1. 2.4	2.09	125	73	17.7	•59	.036
16.0	3.20.6	6.73	411	44	1. 0.3	2.02	.120	74	16.6	-56	.033
30	3.14.4	6.51	399	45	58.1	1.95	·116	75	15.5	.52	.031
17.0	3 8 5	6.31	386	46	56.1	1.88	.112	76	14.4	•48	.029
30	3. 2.9	6.12	·374	47	54.2	1.81	108	77	13.4	•45	.027
18.0	2.57.6	5.94	362	48	52.3	1.75	·104	78	12.3	•41	.025
19	2.47.7	5.61	•340	49	50.5	1.69	101	79	11.2	•38	023
20	2.38.7	5.31	•322	50	48.8	1.63	.097	80	10.2	-34	.021
21	2.30.5	5.04	•305	51	47.1	1.58	.094	81	9.2	•31	.018
22	2.23.2	4.79	•290	52	45.4	1.52	.090	82	8.2	.27	.016
23	2.16.5	4.57	•276	53	43.8	1.47	•0.88	83	7.1	•24	.014
24	2.10.1	4.35	·264	54	42.2	1.41	•085	84	6.1	•20	.012
25	2. 4.2	4.16	252	55	40.8	1.36	.082	85	5.1	.17	.010
26	1.58.8	3.97	241	56	39.3	1.31	.079	80	4.1	•14	.008
27	1.53.8	3.81	230	57	37.8	1.26	.076	87	3.1	·10	1006
28	1.49.1	3.65	219	58	36.4	1.22	073	88	2.0	•07	.004
29	1.44.7	3.50	209	59	35.0	1.17	.070	89	1.0	.03	.002
30	1.40.5	3:36	·201	60	33.6	1.12	•067	90	0.0	•00	.000
31	1.36.6	3.23	193	61	32.3	1.08	065	00		00	, 000
32	1.33.0	3.11	.186	62	31.0	1.04	.062	1			
33	1.29.5	2.99	179	63	29.7	-99	.060				
34	1.26.1	2.88	.173	64	28.4	95	.057				
35	1.23.0	2.78	167	65	27.2	.91	.055	1			
								<del></del>			

The correction for an increase of altitude of one inch in the Barometer, or for depression of one degree in the Thermometer, is to be added to the tabular refraction; but when the Barometer is lower than thirty inches, or the Thermometer higher than 47 degrees, the correction becomes subtractive.

When great accuracy is required, 0.003 inch should be deducted from the observed height of the Barometer, for each degree that the Thermometer near it is above *fifty* degrees, and the same quantity added for an equal depression.

CORRECTION OF MOON'S APPARENT ALTITUDE FOR PARALLAX AND MEAN REFRACTION.

r's ent	Moon'	s Horiz	ONTAL I	PARAIL	X. BAR	ом, 30 і	n. Thei	км. 50°.	r's rent rde.
Moon's apparent altitude.	54'	55'	56′	57′	58′	59'	60′	61′	Moon's apparent altitude.
0	1 11	1 11	1 11	1 11	1 11	1 11	/ //	1 11	0
8	46 59	47 58	48 58	49 57	50 57	51.56	52 56	53 55	8
10	47 56	48 55	49 54	50 53	51 52	52 51	53 50	54 49	10
12	48 26	49 25	50 23	51 22	52 21	53 19	54 18	55 17	12
15	48 39	49 37	50 35	51 33	$52\ 31$	53 29	54 27	55 25	15
20	48 7	49 3	50 0	50 56	51 53	52 49	53 45	5442	20
24	47 9	48 4	48 59	49 54	50 49	51 44	52.38	53 33	24
27	4612	47 6	47 59	48 53	49 46	50 40	51 33	52 27	27
30	45 3	45 55	46 47	47 35	48 31	49 23	50 15	51 7	30
32	44 12	45 3	45 54	46 45	47 35	48 26	49 17	50 8	32
34	43 17	44 7	44 56	45 46	46 36	47 25	48 15	49 5	34
36	42  18	43 6	43 55	44 44	45 32	46 21	47 9	47 58	36
38	41 14	42 2	42 49	43 36	44 23	45 11	45 58	$46 \ 45$	38
40	40 8	40 54	41 40	$42 \ 26$	43 12	43 58	44 44	45 30	40
42	38 59	39 43	40 28	41 12	41 57	42 41	43 26	44 11	42
44	37 44	38 28	39 11	39 54	40 37	41 21	42. 4	4246	44
45	37 7	37 50	38 32	39  14	39 57	40 39	41 22	42 4	45
46	36 29	37 10	37 52	$38 \ 34$	39.15	39 57	$40 \ 39$	41 20	46
47	35 50	36 31	37 11	37 52	38 33	38 14	39 55	40 36	47
48	35 10	35 50	36 30	36 10	37 50	37 30	38 11	39 51	48
49	34 29	35 8	35 48	36 27	36 7	37 46	38 25	39 5	49
50	33 48	34 26	35 5	35 44	36 22	37 1	37 39	38 18	50
51	33 6	33 44	34 21	34 59	35 37	36 15	36 52	37 30	51
52	32 22	32 59	33 36	34 13	34 50	35 27	36 4	36 41	52
53	31 39	32 15	32 51	33 27	34 3	34 40	35 16	35 52	58
54	30 55	31 30	32 5	32.41	33 16	33 51	34 27	35 2	54
55 56	$\begin{array}{c} 30\ 11 \\ 29\ 25 \end{array}$	30 45	31 19	31 54	32 28	33 3	33 37	34 11 33 20	55
57	$\frac{29}{28} \frac{25}{40}$	29 59	$\begin{vmatrix} 30 & 32 \\ 29 & 45 \end{vmatrix}$	$\frac{31}{30} \frac{6}{18}$	31 40	32 13 31 23	32 47	32 28	56
		29 12			30 50		31 56 31 4	31 36	57 58
58	27 53	28 25	28 57	29 29	30 10	30 32			
59	27 7	27 37	28 8	28 39	29 10	29 41	30 12	30 43	59
60	$26\ 19$	26 49	27 19	27 49	28 19	28 49	29 19	29 49	60

# MEASURING LINES.

In the surveys of the United States lands it is required, that the measuring chain should be two poles, or thirty-three feet in length, and containing fifty links, which must be compared with, and adjusted to the length of the standard chain in the Surveyor General's Office, and afterwards to be frequently compared with a standard chain kept by the surveyor for that purpose. But all the measurements, and calculations, are kept, and entered in the field book, in four pole chains, of one hundred links.

The surveyor is required to use eleven tally pins; they should be made of steel, and not more than about one foot in length, and large enough near the points, to cause them to drop perpendicularly; at

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the top end of each pin, a loop or eye should be made, in which a piece of red cloth may be fixed, that they may be more readily found, when stuck among weeds, grass, &c.

In all measurements the level or horizontal length is to be taken; for this purpose, in ascending hills, banks, &c., the chain-men must let down one end of the chain to the ground, and raise the other end to a level therewith, at the *elevated end* of which a tally pin should be plumbed and let fall, to ascertain the spot for setting it; and, when the surface of the ground is very steep, it may be necessary to take so much of the length of the chain as can be raised to a level, so as to obtain the true horizontal measurement.

In measuring lines, one of the eleven tally pins must be set at the starting-point, and when the remaining ten are set, it is called a tally or out, (five chains) and the forward chain-man cries "Tally," and each chain-man registers the distance by slipping a thimble or loop on a tally belt worn for that purpose. The back chain-man then comes up, and having counted, in the presence of his fellow, the tally pins which he had taken up, so that both may be assured that none have been lost, takes the forward end of the chain and proceeds to set them. Thus the chain-men alternately change places, each setting the pins that he had taken up, so that one is forward in all the odd, and the other in all the even tallies; which contributes to the accuracy of the measurement, facilitates the recollection of the distances to notable objects on the line, and renders a mistally almost impossible.

Measurements with the chain and tally-pins are often very imperfectly performed by the chain-men, and much more error is made than is generally supposed. It has been found by many trials, with as good men as can generally be obtained, that with two sets of chainmen, instructed alike in the proper manner of keeping their chain level and straight on the line, and of setting the tally-pins plumb, as well as holding the ends of the chain to them, a difference has sometimes been made of 36 links, and an average difference of 15 or 16 links to a mile, in common timbered land. But repeated measurements over the same mile, by the same chain-men, and near the same time, will generally agree within five links; yet after several months' employment in the field, a measurement of this line may not agree so nearly. Again, the same chain-men will make a different measurement to some extent, over swamps, marshes, wind-



falls and thickets, when there is snow on the ground and when there is none, in cold and in warm weather, effecting a change in the length of the chain, and by measuring fast or slow the amount of error to each would be difficult to estimate. Therefore the surveyor should keep a vigilant watch over his chain-men, and see that their duties are performed in the best manner, to counteract all these sources of error as far as practicable.

# TELESCOPIC MEASUREMENT.

This method of measuring, when properly conducted, is more uniformly the same, and therefore correct, than measurements made by the chain by various chainmen. It is well adapted to measure along the shores of lakes and rivers where obstacles are frequently found of a character to prevent a good measurement with a chain, also for measuring short distances over streams, ponds, &c.

The following arrangement and method of measuring with a telescope and rod will be found very convenient for meandering rivers, lakes, &c. A good telescope must be provided, of about 16 or 18 inches in length when adjusted for use, with two parallel lines correctly set in its principal focus, forming between them, in the field view, not less than 45' of a degree. This telescope is attached to the sight of the compass with a suitable fixture for that purpose, when wanted for use. Provide a sliding-rod, such as are commonly used for taking levels for canals, railroads, &c., with two targets, one stationary at the top of the rod, the other moveable, with a vernier for the usual readings, on the lower part.

When measurements with the telescope and rod are to be made, the telescope must be attached to the compass sights and adjusted for an observation; then measure four chains from it very accurately, and place the rod at that point, with the targets facing the compass, then bring the upper line in the telescope to bear correctly on the upper target by means of the levelling screws, and adjust the moveable target to range with the lower line, then by observing accurately the distance the targets are apart on the rod, when they measure the angle formed by the parallel lines in the telescope at the given distance from the compass, the observer will have data from which a table may be readily constructed for all other distances, of which the telescope will enable the observer to view the distance between the targets accurately. It may conduce to the

# METHODS FOR MEASURING DISTANCES, ETC. 37

correctness of this method of measuring to make observations at various distances, to test the accuracy of the table thus formed; after this, the surveyor may feel a confidence in the correctness of his measurements with the telescope and rod.

Lines run and measured by this arrangement along the shores of lakes and navigable streams are most conveniently and expeditiously done with two skiffs or canoes, or even with two light rafts, with the compass in one and the rod in the other, which can be landed at suitable points and distances apart on their shores; then, after the bearing and distance between them has been taken, the compass can be moved, with the skiff or canoe, to the position occupied by the rod, and the latter again stationed at the next suitable point, and its course and distance taken as before, and so on to the close of the survey.

In all observations, care should be taken to hold the rod at right angles to the line between it and the compass; but it is often necessary to lean the rod at right angles to this line, sometimes even to a level with the horizon; in all such cases, the telescope must be rolled in the y's to bring the parallel line at right angles to the rod.

By this method, the shores of lakes and rivers, however difficult to be measured with the chain, may be correctly meandered by course and distance, without encountering the obstacles on shore with the compass and chain.

To prevent confusion or mistake in the locality of the different stations and notable objects on the land or off the shore, a temporary map should be fully kept up with the survey, on which each object must be represented in order to furnish data for the construction of a good and correct map.

No surveyor, however, should presume to meander important surveys by this method, except he has previously made the necessary preparations, and has qualified himself by some practical experience beforehand.

TABLE
CHAINS TO FEET,—FEET TO CHAINS.

Links, 7.92 inches.—Chain, 66 feet, = 792 inches.

	CHAINS INT	ro feet.		FEET INTO CHAINS.				
Chains. Links.	Feet.	Chains. Links.	Feet.	Feet.	Links.	Feet.	Links.	
0.1	0.66	3.0	198	0.10	0.15	10.0	15.1	
0.2	1.32	4.0	264	0.20	0.30	15.0	22.7	
0.3	1.98	5.0	330	0.25	0.38	20.	30.3	
0.4	2.64	6.0	396	0.30	0.45	24.	36.3	
0.5	3.30	7.0	462	0.40	0.60	27.	40.9	
0.6	3.96	8.0	528	0.50	0.76	30.	45.4	
0.7	4.62	9.0	594	0.60	0.91	33.	50.0	
0.8	5.28	10.0	660	0.70	1.06	36.	54.5	
0.9	5.94	20.	1320	0.75	1.13	39.	59.1	
0.10	6.60	30.	1980	0.80	1.21	40.	60.6	
0.20	13.20	35.	2310	0.90	1.36	42.	63.3	
0.30	19.80	40.	2640	1.00	1.51	45.	68.2	
0.40	26:40	45.	2970	2.0	3.0	48.	72.7	
0.50	33.00	50.	3300	3.0	4.5	50.	75.7	
0.60	89.60	55	3630	4.0	6.0	51.	77.3	
0.70	46.20	60.	3960	5.0	7.5	54.	81.8	
0.80	52.80	65.	4290	6.0	9.1	57.	86.3	
0.90	59.40	70.	4620	7.0	10.6	60•	90.9	
1.00	66.00	75.	4950	8.0	12.1	63.	95.4	
2.00	132.	80.	5280	9.0	13.6	66.	100.	

CONVENIENT METHODS FOR MEASURING DISTANCES OVER RIVERS, LAKES, MIRY-MARSHES, ETC.; WHICH CANNOT BE MEASURED DIRECTLY WITH THE CHAIN.

It may be remarked here, that in surveying large districts of new country, many obstacles of this kind are to be expected, and are met with sometimes under many difficulties, such as the direction and swampy or thickety character of their shores, also, the annoyance felt by the presence of increasing swarms of blood-thirsty flies and moschetoes, which largely infest such shores in summer; hence the importance of the best management, and correct and expeditious methods of passing such obstacles.

The following illustrations will assist the inexperienced surveyor in the accomplishment of this object. They are given on the principle of reducing the base, whatever may be its course or courses, to

# METHODS FOR MEASURING DISTANCES. 39

a right-angled base to the course of the line to be measured. This can be readily done if care be taken to run and measure the base, at such angles that their latitude and departure can be taken from the traverse table.

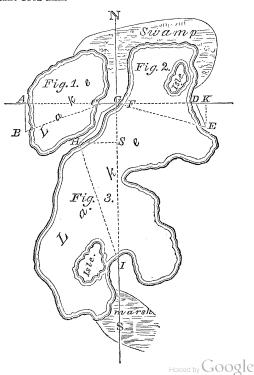
#### FIGURE 1.

Distance required over lake from A to C, course East,—right-angled base,—from A to B 690 links. Angle at C 20° 20′

Natural co-tangent of the angle at C, .....=2.698525 Multiplied by base A. B. 690

 $\begin{array}{r}
242867250 \\
16191150 \\
\hline
1861.982250
\end{array}$ 

Over lake 1862 links



## FIGURE 2.

Distance required over lake from D to F, course West.—From D to E, S. 20° E 752 links—gives 707 links southing, which is the right-angled base K G, and 257 links easting from D to K. Angle at F 15 $\frac{3}{4}$ °.

Natural co-tangent of the angle at $F$ Multiplied by the base $K$ . $E$ ,	=3.545732 707
(Nat. co-tan. $F \times K E$ .)— $K D = D F$ . (3.545.702×707)=2507—257=2250.	$\frac{24820124}{24820124}$
Subtract distance from $D$ to $K$ ,	2506.832524 257
Distance from $D$ to $F$ ,	2250 links nearly.

## FIGURE 3

Distance required over lake from G to I, course South. To obtain a base in this example, we run

	Southing.	Westing.
S. 553 degrees, W. 400	225	331
S. 19 <sup>1</sup> / <sub>4</sub> do W. 440		
S. 50 do W. 548	352	420
Distance from G to S Co-tangent of the angle 16° 33		H to S 896 links. 3.347319
Multiply by the base HS,	,	896
		20083914
		30125871
		26778552
Distance from $S$ to $I$		2999.197824
Add distance from $G$ to $A$	S	992
Distance over lake from	G to I	3991 links.

# DISTANCE OVER A RIVER BY "OFF-SET." EXAMPLE.

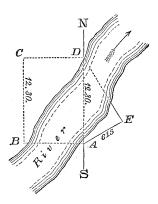


FIGURE 4.

In running a line north, intersect the right bank of a river at A, (course N. N. E.,) and erect an object, turn the compass sights to west, to an object at B, and pass over the river to it, then run and measure a line north to C, and "off-set" east into line at D, the distance between A and D will be equal to the distance between B and C. Or, if a line be run and measured from A, N. 60°, E. until an object in line at D bears N. 30° W., the distance A. D. will be twice that of A. E, for the reason that the triangle thus formed is one-half of an equilateral triangle.

Frequently off-sets are made in passing small lakes, bends of rivers, etc.: sometimes the distances can be advantageously taken over such obstacles, with the telescope and rod, (see article, Telescopic Measurement.) Also, it often happens that a suitable angle can be taken, and the base to that angle measured afterwards; in such cases the distance can be taken from the traverse table; but if no traverse, or other proper tables are at hand, the following angles, on a right angle base, and the multiplier to it, will give the distance. These may be committed to memory.

Angle 11°, 18′, multiply the base by 5, " 14, 2 multiply the base by 4,

Angle 18, 26, multiply the base by 3,

- " 21, 41, multiply the base by 2.5,
- " 26, 34, multiply the base by 2.

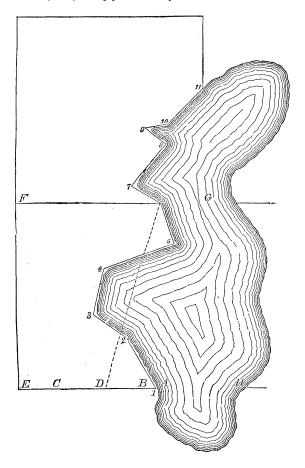


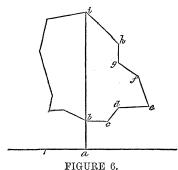
FIGURE 5.

# SHORT METHOD OF FINDING THE AREA OF A MULTANGULAR FIELD.

EXAMPLE, SHOWING HOW TO REDUCE THE PLOT OF A MULTANGULAR FIELD TO A FIELD OF EQUAL AREA HAVING ONLY THREE OR FOUR SIDES, BY WHICH ITS CONTENTS MAY BE READILY FOUND.

To reduce such a field the only instruments required, after the meanders are properly laid down, are a good parallel-rule, \* and a fine protracting point.

In the preceding figure first extend the base EH to an indefinite length; then placing the rule on the angles 1 and 3, move it parallel from the angles 1 and 3 to the angle 2, and mark the exact point of intersection at A, on the base EH. Now place the rule on A and the angle 4, then move it parallel to the angle 3, finding the point B on the base EH; place the rule on B and the angle 5, and move, parallel, to the angle 4, finding the point C on the base EH. Now place the rule on the point C, and the terminating point 6 on the line FC, and move the rule, parallel, to the angle 5, finding the point D on the base EH, from which point draw a line to 6, the process then being complete. The line D 6 thus drawn leaves the same area of lake to the left, that there is of land to the right.



Any figure may be calculated upon the same principle by drawing a base and erecting a perpendicular line from it, passing through

<sup>\*</sup>The triangle and the rule are the best.

the figure. Place the rule at a and c, then move, parallel, back to b, marking the point 1 on the base; then from 1 to d, and move forward to c and so on to the angle at i, leaving a triangle to the right of the perpendicular. Proceed in like manner with that portion of the figure to the left of the perpendicular line, throwing it into two triangles.

### CROSSING RIVERS AND LAKES.

In connexion with convenient methods of measuring distances over lakes and rivers, it is proper to take notice of the means employed, by the most experienced surveyors, for the transit of the surveying party over such waters, when fording them, or travelling around their shores, is impracticable, or causes too much delay.

For this purpose floats or rafts made of logs, of the most dry and buoyant timber at hand is used, and when formed into a raft, its length should be about four times its breadth; with this proportion the raft will steer better, and pass through the water with more ease and expedition, than broad and short rafts.

The following is a safe and expeditious method of constructing these floats:—At a convenient place lay two skids, at a suitable distance apart, parallel to the shore, and near to the water, place on these two logs, twenty feet long and one foot diameter, which are to be the outside logs of the raft, and at about two or three feet from the ends of these, make with an axe a dovetail notch three or four inches deep, and about as wide on their upper sides; then fit into these notches a cross piece, or tie of a suitable size, and wedge them there firmly, so that these logs will not be separated on the water; then before or after launching this into the water, as convenience may suggest, fill in underneath the cross pieces, between the outside logs, with smaller timber of the same length, and tie them to these pieces, or fasten them by means of a dovetail notch. For crossing deep water, where poles cannot be used, paddles, or oars will be needed; they can be split out of a log and hewn into the proper shape in a few minutes.

With the whole force of the surveying party, it will require from one to two hours to construct a raft of a sufficient size to pass them all over a lake or river at one time.



# RUNNING LINES WITH THE SOLAR COMPASS.

In commencing a survey where the latitude, as given by the instrument with which the survey is to be made, is unknown, the survevor should first determine the latitude of his commencing point. He should remember, that in running any other than an east and west line, he is continually changing his latitude, so that every ninety-two chains and thirty links, of northing, or southing, will change his latitude one minute of a degree, or 5' 12" for six miles, and a corresponding change of latitude must be set off on the lati-During the progress of a large survey, the surveyor tude arc. should determine his latitude daily, if practicable, by the meridian passage of the sun, to test the correctness of the adjustments of the latitude and declination arcs.

It is equally important that the sun's declination be truly set off on the declination arc, for the time and longitude of the station, as it is that the latitude are be truly adjusted to the latitude of the place of observation.

The following method of preparing the sun's declination, as taken from the Nautical Almanac, for daily use, in any longitude, will be found useful in practice:

#### EXAMPLE.

To calculate the sun's declination for all hours of the daytime for May 11th, 1854, in latitude 42° N., longitude 120° W., or eight hours before noon, local time, corresponding to Greenwich noon.

```
12 h. - 8 h. = 4 h. A. M., at the place of observation.
                          17° 52′ 11" at Greenwich noon, as per Nautical Almanac,
Sun's declination.
Meridional refraction +
                                    26
                               52
                                    37
                                       4 h. A. M.,
                                                     17º 57' 41" at noon.
Hourly difference +
                                    38
                          17
                               53
                                    15
                                        5 h. A. M.,
                                                     17
                                                         58
                                                              19
                                                                  1 h. p. m.
                                    38
                               53
                                                     17
                                                         58
                          17
                                    53
                                        6 h. a. m.,
                                                              57
                                                                  2 h. p. m.
                                                              38
                                                                  3 h. р. м.
                          17
                               54
                                    31
                                        7 h. A. M.,
                                                     17
                                                         59
                                                              35
                                    38
                                                              38
                          17
                               55
                                        8 h. A. M.,
                                                     18
                                                          0
                                                              13
                                                                  4 h. P. M.
                                    38
                                                              38
                                                    18
                                                             51
                          17
                               55
                                   47
                                        9 h. a. m.,
                                                                  5 h. p. m.
                                   25 10 h. a. m.,
                                                                  6 h. p. m.
                          17
                               56
                                                     18
                                                          1
                                                              29
                               57
                                                           2
                                                               7
                                                                  7 h. p. m.
                           17
                                     3 11 h. a. m.,
                                                     18
                                                           2
```

57 41 12 h. м.,

18

17

45 8 h. p. M.

To calculate the sun's declination for August 25th, 1854, for all hours of the daytime, in latitude 45° N., longitude 90° W., or six hours before noon, local time, corresponding to Greenwich noon.

12 h.—6=	=6 h	Α.	м., at the place	e of	observa	tion.
Sun's declination N., 1	0 48	3' 12	//	10	° 44′ 31′	<sup>7</sup> 11 h. a. m.
*Meridional refraction-		39			52	
10	48	51	6 h. A. M.,	10		12 h. м.
*Hourly difference-		52			52	
10	47		7 h. A. M.,	10	$42\ 47$	1 h. p. m.
		52			52	
10	47	7	8 h. a. m.,	10	41  55	2 h. p. m.
		52			52	
10	46	15	9 h. a. m.,	10	41 3	3 h. p. m.
		52			52	
10	45		10 h. a. m.,	10	40 11	4 h. p. m.
-		52	44.1	40	52	r 1
10	44	: 31	11 h. a. m.,	10	$39 \ 19$	5 h. p. m.

The calculations for the sun's declination for each hour of the day can be made after the preceding forms, on blank leaves placed in the field book, where they would be required through the day.

In the following table the hourly difference of the sun's declination, as given for the day, in the Nautical Almanac, will be found to the nearest second in the left hand column, and the change of declination for any number of hours to twelve, will be found against it, under the hour at the head of the columns.

This table is useful when the sun's declination is required for any number of hours up to twelve, before or in advance of Greenwich noon.

#### EXAMPLE.

Suppose the sun's declination is required for September 6, 1854, at 2 h. P. M., in longitude 120° W., or 8 h. in time W. of Greenwich, then 8+2=10 hours. The sun's declination at Greenwich noon is 6° 28′ 52′′ N.; hourly difference 56′′, against this, in the above table, and under 10 hours, we find 9′ 20′′, which subtract from 6° 28′ 52′′=6° 19′ 32′′ for the sun's declination at the time and place required.

\* The hourly difference of the sun's declination must be added when his declination is increasing, and subtracted when it is decreasing; and the meridional refraction must be added to the declination when the latitude is of the same name, and subtracted when of a contrary name. See method of finding Meridional Refraction.

Table of the increase or decrease of the sun's declination for hourly differences from  $5^{\prime\prime}$  to  $60^{\prime\prime}$ , and from three to twelve hours of time.

DIFF.	3 н.	4 н.	5 н.	6 н.	7 н.	8 н.	9 н.	10 н.	11 н.	12 п.
" 5 6 7 8 9 10	15 18 21 24 27 30	20 24 28 32 36 40	25 30 35 40 45 50	7	7	40 48 56 1 4 1 12 1 20	$^{\prime}$ $^{\prime\prime}$	7	7 " 55 1 06 1 17 1 28 1 39 1 50	1 00 1 12 1 24 1 36 1 48 2 00
11	33	$\begin{array}{c} 44 \\ 48 \\ 52 \\ 56 \\ 1 & 0 \\ 1 & 4 \\ 1 & 8 \\ 1 & 12 \\ 1 & 16 \\ 1 & 20 \\ \end{array}$	55	1 6	1 17	1 28	1 39	1 50	2 1	2 12
12	36		1 00	1 12	1 24	1 36	1 48	2 00	2 12	2 24
13	39		1 5	1 18	1 31	1 44	1 57	2 10	2 23	2 36
14	42		1 10	1 24	1 38	1 52	2 6	2 20	2 34	2 48
15	45		1 15	1 30	1 45	2 00	2 15	2 30	2 45	3 00
16	48		1 20	1 36	1 52	2 8	2 24	2 40	2 56	3 12
17	51		1 25	1 42	1 59	2 16	2 33	2 50	3 7	3 24
18	54		1 30	1 48	2 6	2 24	2 42	3 00	3 18	3 36
19	57		1 35	1 54	2 13	2 32	2 51	3 10	3 29	3 48
20	1 00		1 40	2 00	2 20	2 40	3 00	3 20	3 40	4 00
21	1 3	1 24	1 45	2 6	2 27	2 48	3 9	3 30	3 51	4 12
22	1 6	1 28	1 50	2 12	2 34	2 56	3 18	3 40	4 2	4 24
23	1 9	1 32	1 55	2 18	2 41	3 4	3 27	3 50	4 13	4 36
24	1 12	1 36	2 00	2 24	2 48	3 12	3 36	4 00	4 24	4 48
25	1 15	1 40	2 5	2 30	2 55	3 20	3 45	4 10	4 35	5 00
26	1 18	1 44	2 10	2 36	3 2	3 28	3 54	4 20	4 46	5 12
27	1 21	1 48	2 15	2 42	3 9	3 36	4 3	4 30	4 57	5 24
28	1 24	1 52	2 20	2 48	3 16	3 44	4 12	4 40	5 8	5 36
29	1 27	1 56	2 25	2 54	3 23	3 52	4 21	4 50	5 19	5 48
30	1 30	2 00	2 30	3 00	3 30	4 00	4 30	5 00	5 30	6 00
31	1 33	2 4	2 35	3 6	3 37	4 8	4 39	5 10	5 41	6 12
32	1 36	2 8	2 40	3 12	3 44	4 16	4 48	5 20	5 52	6 24
33	1 39	2 12	2 45	3 18	3 51	4 24	4 57	5 30	6 3	6 36
34	1 42	2 16	2 50	3 24	3 58	4 32	5 6	5 40	6 14	6 48
35	1 45	2 20	2 55	3 30	4 5	4 40	5 15	5 50	6 25	7 00
36	1 48	2 24	3 00	3 36	4 12	4 48	5 24	6 00	6 36	7 12
37	1 51	2 28	3 5	3 42	4 19	4 56	5 33	6 10	6 47	7 24
38	1 54	2 32	3 10	3 48	4 26	5 4	5 42	6 20	6 58	7 36
39	1 57	2 36	3 15	3 54	4 33	5 12	5 51	6 30	7 9	7 48
40	2 00	2 40	3 20	4 00	4 40	5 20	6 00	6 40	7 20	8 00
41	2 3	2 44	3 25	4 6	4 47	5 28	6 9	6 50	7 31	8 12
42	2 6	2 48	3 30	4 12	4 54	5 36	6 18	7 00	7 42	8 24
43	2 9	2 52	3 35	4 18	5 1	5 44	6 27	7 10	7 53	8 36
44	2 12	2 56	3 40	4 24	5 8	5 52	6 36	7 20	8 4	8 48
45	2 15	3 0	3 45	4 30	5 15	6 00	6 45	7 30	8 15	9 00
46	2 18	3 4	3 50	4 36	5 22	6 8	6 54	7 40	8 26	9 12
47	2 21	3 8	8 55	4 42	5 29	6 16	7 3	7 50	8 37	9 24
48	2 24	3 12	4 00	4 48	5 36	6 24	7 12	8 00	8 48	9 36
49	2 27	3 16	4 5	4 54	5 43	6 32	7 21	8 10	8 59	9 48
50	2 30	3 20	4 10	5 00	5 50	6 40	7 30	8 20	9 10	10 00
51 52 53 54 55 56 57 58 59 60	2 33 2 36 2 39 2 42 2 45 2 2 51 2 54 2 57 3 0	3 24 3 28 3 32 3 36 3 40 3 44 3 48 3 52 3 56 4 0	4 15 4 20 4 25 4 30 4 35 4 40 4 45 4 50 4 55 5 0	5 6 5 12 5 18 5 24 5 30 5 36 5 42 5 48 5 54 6 0	5 57 6 4 6 11 6 18 6 25 6 32 6 39 6 46 6 53 7 0	6 48 6 56 7 4 7 12 7 20 7 28 7 36 7 44 7 52 8 0	7 39 7 48 7 57 8 6 8 15 8 24 8 33 8 42 8 51 9 0	8 30 8 40 8 50 9 00 9 10 9 20 9 30 9 40 9 50 10 0	9 21 9 32 9 43 9 54 10 5 10 16 10 27 10 38 10 49 11 0	10 12 10 24 10 36 10 48 11 00 11 12 11 24 11 36 11 48 12 00

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Observations with the solar compass for the purpose of running lines, or to determine the variation of the needle, should not be made when the sun or other celestial object is nearer than 8°, or thirty-two minutes of time from the meridian: nearer than this, the observations may not give the course required sufficiently correct for the ordinary purpose of running lines.

The best part of the year for running lines with the solar compass is the summer season, or when the latitude and the declination of the sun are both of the same name. During this portion of the year there is usually the most fair weather for work of this kind, and the sun's altitude being generally higher through most of the day, affords more frequent opportunities in the forest to adjust the instrument by the sun, to the course of the line. There are, also, more hours of the day in which the solar compass can be used; the advantages of this will be fully realized when running lines in thickly timbered land, or in hilly or mountainous districts, when their summits intervene between the instrument and the sun, until a late hour in the morning and early in the afternoon.

From the principles already given in regard to the use of the solar compass, it will be perceived, that it requires more skill to use it with facility, than it does to use the magnetic compass; therefore, the surveyor should acquire this skill, before entering upon any important survey.

More line can be run with the solar compass in a day, than with the magnetic compass in the same time, if both instruments are properly used; for the reason that it requires less time to adjust the solar compass to the course by the sun, than it does the magnetic compass by the needle.

Much experience has established the fact, that a continual line can be run independently of the needle, through heavy timbered land, without cutting away any timber, except lopping a bush occasionally, between the instrument and the sun. Therefore, lines can be correctly run through any mineral region or other country, however great the local attractions or variations may be on the magnetic needle, with an accuracy not attainable with the magnetic compass. In making the survey of new districts of country, especially where there is considerable local attraction, it is important to determine the variation of the needle frequently, and make a record of the same for future reference.

During the surveys of the mineral region of Lake Superior, it was discovered that all mineral veins in that country had an influence, more or less, on the direction of the magnetic needle, its North end being generally attracted towards the metallic vein. These indications led (and no doubt will to a greater extent in future) to the discovery of mineral veins of various kinds in that and other regions; but the influence of metallic deposits on the magnetic needle, according to their various qualities, courses, distances, depths, &c., from the instrument, are as yet imperfectly understood.

It is to be hoped that this subject will receive, in future, that attention which its importance requires.

These aberrations in proximity to metallic deposits, suggest to the mind that they may be caused by galvanic currents, which circulate around the earth, and become deflected out of their general course by the metallic veins being a better conductor than the surrounding medium.

Galvanic currents conducted by any metallic substance always influence the direction of the magnetic needle, and incline it toward a right angle to its course; metallic deposits may also, in connexion with the various rocks and other substances in which they are immediately enclosed, form in themselves, local galvanic batteries, of greater galvanic intensity than is generally circulating in their vicinity, and thus diffuse an influence around them at considerable distances.

If these suggestions are correct, they seem to point to metallic deposits, in connexion with other substances in which they are enclosed, as the producing cause of the galvanic currents which circulate continually around the earth, nearly at right angles to its axis.

CONVENIENT RULES FOR CORRECTING THE COURSE OF RANDOM LINES, WHEN THE CORRECTION DOES NOT EXCEED 200 LINKS TO EACH MILE.

Rule for half a mile, or forty chains.

From the number of links to be corrected in that distance, subtract one-seventh; the difference will be the number of minutes of a degree required for the correction of the course.

#### EXAMPLE.

Number of links to be corrected, 42-6-36' answer.

Rule for one mile, or eighty chains.

From half of the number of links to be corrected in that distance, subtract one seventh; the difference will be the number of minutes of a degree required for the correction of the course.

#### EXAMPLE.

Number of links to be corrected,  $70 \div 2 = 35 - 5 = 30'$  answer.

Rule for three miles.

Divide the whole number of links to be corrected by seven; the quotient will be the number of minutes of a degree required for the correction of the course.

#### EXAMPLE.

Number of links to be corrected,  $297 \div 7 = 42\frac{3}{7}$  answer.

Rule for six miles.

Divide one half of the number of links to be corrected by seven; the quotient will be the number of minutes required for the correction of the course.

#### EXAMPLE.

Number of links to be corrected,  $370 \div 2 = 185 \div 7 = 26\frac{3}{7}$  ans.\*

The distances given for corrections, in the above examples, are those for which corrections are generally made in the surveys of the public lands, and the calculation for the course of the corrected line, can generally be mentally made by the surveyor, while he is occupied in adjusting his instrument.

For other distances, when the correction does not exceed 1° 45′, divide the distance run, by the number of links to be corrected in the length of the line; the quotient will be the natural co-tangent of the correction to be applied to the random course.

In the following table, the angle of correction is given in the first column from 1' to 1° 40'; and against each angle the departure is given for distances one, forty, eighty, and two hundred and forty chains, or three miles. These distances may be reckoned as tens, hundreds, thousands, if the position of the decimal point in each departure be changed accordingly.

The departure under distance one chain is of course the natural

<sup>\*</sup> The above rules are close approximations.

sine of the angle; therefore, if it be multiplied by the distance run on any angle, the product is the departure.

TABLE, SHOWING THE ANGLE OF CORRECTION FOR RANDOM LINES.

·				1		1			
ai.	Number	Links	Links	Links	o o	Number	Links	Links	Links
Angle.	oflinks	in 40	in 80	in 3	Angle.	oflinks	in 40	in 80	in 3
85	in 1 ch.	ch.	chains.	miles.	9	in 1 ch.	chains,	chains.	miles.
4	III I CH.	en.	chains.	minos.		111 1 (11.	Chama,	CHAILE.	mines.
1'	·000291	1.16	2.33	6.90	51'	014835	59.34	118 68	356.04
2	·000582	2.33	4.66	13.97	52	015126	60.50	121.01	363.02
3	.000873	3.49	6.98	20.95	53	.015417	61.67	123.34	370.01
4	001164	4.66	9.31	27.94	54	.015707	62.83	125.66	376.97
5	.001454	5.82	11.63	34.90	55	.015998	63.99	137.98	383.95
6	.001745	6.98	13.96	41.88	56	016289	65.16	130.31	390.94
7	.002036	8.14	16.29	48.86	57	016580	66.32	132.64	397.92
8	.002327	9.31	18.62	55.85	58	.016871	67.48	134.97	404.90
9	.002618	10.47	20.94	62.83	59	.017162	68.65	137:30	411.89
10	.002909	11.64	23.27	69.82	1.0	017452	69.81	139.62	418.85
11	.003200	12.80	25.60	76.80	1.1	.017743	70.97	141.94	425.83
12	.003491	13.96	27.93	83.78	1. 2	•018034	72.14	144.27	432.82
13	003782	15.13	30.26	90.77	1.3	·018325	73.30	146.60	439.80
14	.004072	16.29	32.58	97.73	1.4	018616	74.46	148.93	446.78
15	.004363	17.45	34.96	104.71	1.5	.018907	75.63	151.26	453.77
16	.004654	18.62	37.23	111.70	1. 6	019197	76.79	153.58	460.73
17	.004945	19.78	39.56	118.68	1. 7	019488	77.95	155.90	467.71
18	.005236	20.94	41.89	125.66	1.8	019779	79.12	158.23	474.70
19	.005527	22.11	44.22	132.65	1. 9	020070	80.28	160.58	481.68
20	.005818	23.27	46.54	139.63	1.10	.020361	81.44	162.89	488.66
21	006109	24.44	48.87	146.62	1.11	020652	82.61	165.22	495.65
22	.006400	25.60	51.20	153.60	1.12	020942	83.77	167.54	502.61
23	.006690	26.76	53.52	160.56	1.13	.021233	84.93	169.86	509.59
24	.006981	27.92	55.85	167.54	1.14	021524	86.10	172.19	516.58
25	007272	29.09	58.18	174.53	1.15	021815	87.26	174.52	523.56
26	.007563	30.25	60.50	181.51	1.16	022106	88.42	176.85	530.54
27	.007854	31.42	62.83	188.50	1.17	.022397	89.59	179.18	537.53
28	008145	32.58	65.16	195.48	1.18	022687	90.75	181 50	544.49
29	.008436	33.74	67.49	202.46	1.19	022978	91.91	183.82	551.47
30	008726	34.90	69.81	209.42	1.20	023269	93.08	186.15	558.46
31	009017	36.07	72.14	216.41	1.21	023560	94.24	188.48	565.44
32	.009308	37.23	74.46	223.39	1.22	023851	95.40	190.81	572.24
33	.009599	38.40	76.79	230.38	1.23	024141	96.56	193.13	579.38
34	.009890	39.56	79.12	237:36	1.24	024432	97.73	195.46	586.37
35	.010181	40.72	81.45	244.34	1.25	024723	98.89	197.78	593 35
36	010472	41.89	83.78	251.33	1.26	025014	100.06	200.11	600 34
37	010763	43.05	86.10	258.31	1.27	.025305	101.22	202.44	607.32
38	.011054	44.22	88.43	265.30	1.28	.025595	102.38	204.76	614.28
39	011344	45.38	90.75	272.26	1.29	025886	103.54	207.09	621.26
40	011635	46.54	93.08	279.24	1.30	026177	104.71	209.42	628.25
41	011926	47.70	95.41	286.22	1.31	026468	105.87	211.74	635.23
42	012217	48.87	97.74	293.21	1.32	026759	107.04	214.07	642.22
43	.012508	50.03	100.06	300.19	1.33	.027049	108.20	216.39	649.18
44	$\cdot 012799$	51.20	102.39	307.18	1.34	.027340	109.36	218.72	656.16
45	·013090	52.36	104.72	313.16	1.35	.027631	110.52	221.05	663.13
46	$\cdot 013381$	53.52	107.05	321.14	1.36	.027922	111.69	223.38	670.13
47	013671	54.68	109.37	328.10	1.37	.028212	112.85	225.70	677.09
48	.013962	55.85	111.70	335.09	1.38	.023503	114.01	228.02	684.07
49	014253	57.01	114.02	342.07	1.39	028794	115.18	230.35	691.06
50	.014544	58.18	116.35	349.06	1.40	029085	116.34	232.68	698.04
1	]	1		1	Į!	!	1	1	1
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# TABLE OF LATITUDES AND LONGITUDES.

In the use of the Solar Compass, it is necessary to know approximately at least, the Longitude of the place where the instrument is used, for the purpose of taking out of the Nautical Almanac, the Sun's declination, &c., and reducing them to a time, and Longitude of the place of observation.

For this purpose, the following tabular statement of the latitude, and longitude from the meridian of Greenwich, of some of the most important places, in North America, are given.

PLACES.	LATITUDE	Longitud	e West.
Throng.	North.	In Degrees.	In Time.
Acapulco, Mex., Albany, (Capitol,) N. Y., Amherst, (Collego,) Mass., Apostle Islands, (Lake Superior,) Augusta, (State House,) Me., Baltimore, (Monument,) Md.,	0 / // 16 50 19 42 39 3 42 22 15 47 00 44 18 43 39 17 48	99 49 9 73 44 49 72 31 28 91 00 69 50 76 36 39	H. M. S. 6 39 16 4 54 59 4 50 6 6 4 4 39 20 5 6 26
Bellevue, (Åm. Fur. Cos.' Trading Post, Missouri River,) Boston, (State House,)	38 8 24 42 21 27 26 6 0 38 2 38 40 4 51 44 27	95 47 46 71 3 30 97 12 103 33 15 74 52 37 73 10	6 23 11 4 44 14 6 28 48 6 54 13 4 59 30 4 52 40
Cape Hancock, (Mouth of Columbia River.)       Oregon,         Charleston, (St. Mich.'s Ch.,)       S. C.,         Chicago,       III.,         Columbus,       Ohio,         Concord, (State House,)       N. H.,	46 16 35 32 46 33 42 00 00 39 57 00 43 12 29	124 1 45 79 55 38 87 35 83 3 71 29	8 16 7 5 19 42 5 50 2 5 32 12 4 45 56
Dalles of the Columbia Missionary Station, 0. T., . Detroit, (St. Paul's Church,) Mich., Dover, Del., .  Ewing Harbour, 0. T., .	45 35 55 42 19 45 39 10 42 44 22	120 55 83 2 30 75 30 124 28 52	8 3 40 5 32 10 5 2 0 8 33 55
Falls of St. Anthony, U. S. Cottage, False Dungeness Bay, Oregon, Fort Boisee, Oregon, Fort Hall, Fort Laramie, Fort Leavenworth, (Landing,) Fort Nez Perce, O. T., Frankfort, Ky., Frederickton, N. B.,	44 58 40 48 7 52 43 49 22 35 47 35 43 1 30 42 12 10 39 21 14 46 3 46 38 14 46 3	93 10 30 123 27 21 116 47 3 95 15 10 112 29 54 104 47 43 94 44 84 40 66 45	6 12 42 8 13 49 7 47 8 6 21 7 29 59 6 59 11 6 18 56 5 38 40 4 27
Galveston, (Court House,)	29 18 14 46 40 41 10 42	87 30	6 19 6 5 50 7 29



		LATITUDE	Longitui	e West.
PLACES.		North.	In Degrees.	In Time.
Halifax,	N. S., Pa.,	0 / // 44 39 20 40 16	63 36 40 76 50	H. M. S. 4 14 26 5 7 20
Indianapolis,	Ind.,	39 55	86 5	5 44 20
Jackson,	Miss., Mo.,	32 23 38 36	90 8 92 8	6 00 32 6 8 32
Kanzas River, Mouth of, Key West Light, Keweenau Point, Lake Superior,) Kingston,	Fa., : : : : : : : : : : : : : : : : : : :	39 6 3 24 33 47 30 44 8	94 33 81 48 88 30 76 40	6 18 11 5 27 12 5 54 5 6 40
Little Rock,	Ark.,	34 40	92 12	6 8 48
Mexico, (City of,) Milledgeville, Milwaukie, Mouth of Missouri River, Mobile, Monterey, Montpelier, Montreal,	Mex.,	19 25 45 33 7 20 43 3 45 38 51 36 30 41 26 25 40 13 44 17 45 31	99 5 6 83 19 45 87 57 90 00 40 88 1 29 100 25 36 72 36 73 35	6 36 20 5 33 19 5 51 48 6 00 3 5 56 2 6 41 42 4 50 24 4 54 20
Nebraska, or Platte River, Junction of North and South Forks, New Orleans, (City Hall,)		41 5 5 29 57 30	101 21 24 90	6 45 25 6
Pittsburg, Point Conception, Point Hudson, Prairie du Chien, Am. Fur Co.'s	Pa.,	40 32 34 26 56 48 7 3	80 2 120 25 39 122 44 33	5 20 8 8 1 42 8 10 58
House,		43 3 6	91 9 19	6 4 37
Quebec, (Citadel,)	C. E.,	46 49 12	71 16	4 45 4
Richmond, (Capitol,)	Va.,	37 32 17	77 27 28	5 9 50
Sacramento City, Sackett's Harbour, St. Paul's, St. Vrain's Fort, San Francisco, (Presidio,) Santa Fe, Scarboro Harbour, Snake River, above Amer. Falls, Springfield,	N. Ý., Min., Indian Ter., Cal., N. M., Wash T.,	88 34 42 43 55 44 52 46 40 16 52 37 47 35 35 41 6 48 21 49 42 47 5 39 48	120 nearly. 75 57 93 4 54 105 12 25 122 26 15 106 1 22 124 37 12 112 40 13 89 33	8 5 3 48 6 12 19 7 48 1 8 9 45 7 4 5 8 18 29 7 30 41 5 58 12
Tallahassee, Toronto or York, (Observ.,) Tuscaloosa,	Fa.,	43 39 35 33 12	84 36 79 21 30 87 42	5 38 24 5 17 26 5 50 48
Washington, (Capitol,)	D. C., .	38 53 34	77 1 30	5 8 6
York,	Me.,	43 10 0	70 40	4 42 40

The latest and best maps of North America show the longitude of all places within its boundary sufficiently near for the purpose of reducing the sun's declination to their meridians.

LENGTHS IN NAUTICAL MILES AND STATUTE MILES OF DEGREES OF LATITUDE AND LONGITUDE IN DIFFERENT LATITUDES.

DEGREE	OF THE PA	RALLEL.	DEGREE	OF THE ME	ERIDIAN.
Latitude of Parallel.	Nautical miles.	Statute miles.	Latitude of middle point.	Nautical miles.	Statute miles.
200	56.404	65.018	200	59.664	68.777
21	56.039	64.598			
22	55.657	64.158	i		
23	55.258	63.698	)		
24	54.843	63.219			
25	54.411	62.721	25	59.706	68.825
26	53.962	62.204			
27	53.497	61.668		,	
28	53.016	61.113	ŀ		
29	52.518	60.540	00	F0 = 10	00.055
30	52.005	59.948	80	59.749	68.875
$\frac{31}{32}$	51.476	59.338			
33	50·931 50·370	58·709 58·063			
34	49.794	57:399			
85	49.794	56.718	35	59.796	68-929
36 36	48.597	56.019	99	99.190	00.929
37	47.976	55.304			
38	47:341	54.571			
39	46.960	53.822			
40	46.026	53.056	40	59.847	68.987
41	45:348	52.274	- TO	00 ST	00 001
42	44.654	51.476			
43	43.949	50.662			
44	43.230	49.833			
45	42.497	48-988	45	59.899	69.048
46	41.752	48.128	1		
47	40.993	47.254			
48	40.222	46.365			
49	39.439	45.462			
50	38.643	44.545	50	59.951	69.108

A degree of longitude at the equator = 69.163 statute miles. A second of time at the equator = 1521.6 feet.

### RUNNING PARALLELS OF LATITUDE.

Parallels of latitude are curved lines, and they increase in curvature from the equator to the poles, and cross all meridians at right angles. All lines run at any angle from the meridian, by courses taken at short intervals, partake more or less (according to the angle) of the curvature of parallels of latitude.

When the compass is set to a true east and west course, in any latitude, the line of sight is at right angles to the meridian, and in consequence of the spheroidical figure of the earth, which causes the curvature of the parallels of latitude, this line of sight will converge

on the equator. Some correction is therefore due to each course taken between stations, to keep the line on the same parallel of latitude. This correction, however, is too small to make any material error in tracing the parallel, if the stations are not more than 30" of longitude apart; but if larger than this, the convergency on the equator should be computed for the distance, and allowed on the side towards the pole. But a more convenient and practical method of running parallels of latitude, or lines at any angle from the meridian, is to back sight on each forward sight, and take half the difference between their courses, when large enough to be perceptible. Thus, the forward and back sights, give double the amount of curvature between the two stations, the one half of which must be set off at the end of the forward sight toward the pole, to keep the line on the same parallel of latitude. Any unusual difference between two equal stations, must be re-examined, and errors corrected if any, as the line advances.

A line run west six miles, or more, with long stations between sights, cannot be retraced by running east in the same manner, for the east line will fall towards the equator; therefore attention should be given to this subject in running the east and west lines of the public lands, when long distances are taken between stations over water, prairies, or open lands.

When running a parallel of latitude, if an object be observed due east or west from any station, the correction of the course to touch the same parallel on the meridian of the object, is equal to one half of the angle of convergency between the two meridians, which pass through the station and the object.

The following table will show the convergency of six miles apart on the parallel of each degree of latitude, and six miles from them towards the poles of the earth.

TABLE.

Parallel of Latitude.	Links of Convergency.	Angle of Convergency.	Parallel of Latitude.	Links of Convergency.	Angle of Convergency.	Parallel of Latitude.	Links of Convergency.	Angle of Convergency.
0		1 //	0		/ //	0		1 11
10	15.0	1· 4 1· 7	27	36.9	2.38	44	70.1	5.01
11	15.7	1.7	28	38.6	2.46	45	72.6	5.12
12	16.5	1.11	. 29	40.2	2.53	46	75.2	5.23
13	17:3	1.14	30	41.9	3· 0 3· 7	47	77.8	5.34
14	18.2	1.18	31	43·6 45·4	3· 7 3·15	48	80·6 83·5	5.46
15 16	19·4 20·7	1.23 1.29	32 33	47.2	3.19	49	86.5	5·59 6·12
17	22.0	1.34	34	49.1	3.31	50 51	89.7	6.25
18	23.4	1.40	35	50.9	3.39	52	93.0	6.40
19	24.9	1.47	36	52.7	3.46	53	96.4	6.55
20	26.5	1.54	37	54.7	3.55	54	100.0	7.10
21	27.8	1.59	38	56.8	4.4	55	103.7	7.26
22	29.3	2.6	39	58.8	4.13	56	107.6	7.43
23	30.8	2.12	40	60.9	4.22	57	111.8	8.00
24	32.3	2.19	41	63.1	4.31	58	116.2	8.19
25	33.8	2.25	42	65.4	4.41	59	120.9	8.40
26	35.4	2.32	43	67.7	4.51	60	125.7	9.00

#### EXPLANATION AND USE OF THE ABOVE TABLE.

To find the convergency and angle for the fractional parts of each degree of latitude, increase the convergency and angle, in proportion to the fractional part required. The convergency of equal lengths of meridians with same latitude are in proportion to their distance apart.

The convergency between any two meridians, whose lengths are equal to their mean distance apart, is in proportion to the square of the distance given in the table (six miles) to the square of the length required.

#### EXAMPLE.

Suppose it is required to find the convergency of two meridians three miles in length and three miles apart, in latitude  $42^{\circ}$  (6<sup>2</sup>):  $65.4:3^{\circ}:16.35$  links.

Suppose a station in latitude 42° N. an object is observed due east eight miles distant; how far north of the object is the same parallel of latitude, of the station from which the observation is made? Proceed as in the above example. 36:65.4::64:116.27. One half of which is 58,14 links nearly, answer. (See rule preceding the above table.) If the angle be required that would touch the same parallel

north of the object, it will be given by the following proportion; 6:44 41":: 8:6' 14". One half of which is 3' 7" or N. 89° 56' 53" E.\*

# CONVERGENCY OF MERIDIANS.

Rule.—As the cosine of any given latitude is to a given distance of longitude, in that latitude, so is the cosine of any other latitude, to the distance of a corresponding longitude; the difference of these numbers will be the convergency.

#### EXAMPLE.

Required the convergency of two range lines that are 6 miles or 480 chains apart, in latitude 42° 30′ north, and extending north ten townships, or to latitude 43° 21′ 48″.

: Log. - 2.675153 = 473.32 subtract from 480. chains = 6.68 chains. The convergency.

TO RUN A LINE PARALLEL TO A GIVEN MERIDIAN, AT ANY DISTANCE EAST OR WEST OF IT.

Find the angle of convergency between the meridians for the distance required, then run the line at the angle thus found, east or west of the meridian as the case requires.

## AMPLITUDE OF CELESTIAL OBJECTS.

All heavenly bodies will rise and set to the north, or to the south of the east and west points of the horizon, as their declination may be north or south.

In consequence of the horizontal refraction of celestial objects, the proper time of taking their amplitude is when their centers appear about 33' above the horizon.

#### TO FIND THE AMPLITUDE.

To the Log, secant of the latitude (rejecting its index,) add the Log-sine of the sun's or star's declination; the sum will be the Log-

<sup>\*</sup> The preceding rules are close approximations to the truth.

sine of the course, the sun or star will rise or set from the east or west point.

#### EXAMPLE.

Latitude 42° 45′ Log. secant,	.134113
Declination 15° 10,' Log. sine,	9.417684
Log sine of Amplitude,	$9.551797 = 20^{\circ} 52.$
Log sine of Ampirtude,	$9.551797 = 20^{\circ} 52.$

### PROBLEMS.

#### TO FIND THE TIME OF THE SUN RISING OR SETTING.

RULE.—To the tangent of the latitude, add the tangent of the sun's or star's declination, and subtract radius from their sum; the remainder is the cosine of the semi-diurnal arc, when the latitude and declination are of different names; and of the semi-nocturnal arc, when both are of the same name.

#### EXAMPLE.

Sun's decl. 18° 20 Latitude 41° 50'	Tangent = 9.520305 Tangent = 9.951896
Subtract radius	$19.472201 \\ 10.000000$

Cosine  $9.472201 = 72^{\circ} 45'$  or 4h. 51min.

Apparent time of sunrise when the latitude and declination are of the same name, or sunset when they are of different names.

TO FIND THE ANGLE THAT THE EQUATORIAL LINES OF THE SOLAR COMPASS, MAKE WITH THE HORIZON IN ANY LATITUDE, WHEN OBSERVING A CELESTIAL OBJECT, AT ANY HOUR ANGLE FROM THE MERIDIAN.

Rule.—As radius is to the cosine of the latitude, so is the sine of the hour angle of the celestial object, to the sine of the angle of the equatorial lines with the horizon.

#### EXAMPLE.

As radius,	10.000000	
: Cosine of lat. 42° 30'	= 9.867631	
:: Sine of H'r angle 30° 00'	V = 9.698970	
	<del>Vagaines and an array and a second a second and a second</del>	
: Sine of angle	$= 9.566601 = 21^{\circ} 38' \text{ nearly}$	<b>y</b> •

TO FIND THE AZIMUTH OF THE POLE STAR AT THE TIME OF ITS GREATEST ELONGATION.

RULE.—As cosine of the latitude, is to radius, so is the cosine of the declination, to the sign of the azimuth or elongation.

# EXAMPLE.

Latitude 40° 20', declination of the pole star, January 1st, 1854, 88° 32' 7".

As cosine of lat. 40° 20.	<b>9.882121</b>
; Radius	10.000000
:: Cosine of Decl. 88° 32′ 7″	= 8.407727
	18.407727
	9.882121
	Management of the second
: Sine of azimuth	$8.525606 = 1^{\circ}, 55', 20''$

TO FIND THE MOON'S PARALLAX IN ALTITUDE, AND TO REDUCE IT TO THE QUANTITY TO BE SUBTRACTED FROM HER DECLINATION WHEN HER LATITUDE IS OF THE SAME NAME, AND ADDED TO IT, WHEN OF A CONTRARY NAME.

Rule.—As radius is to the sine of horizontal parallax, so is the cosine of altitude to the sine of parallax in altitude: subtract the refraction in altitude and the meridional refraction; take the proportional part of this difference from table of proportional parts of refraction, and apply it to her declination as above named.

#### EXAMPLE.

EAA	MI ME.
As Radius,	10.000000
: Sine horizontal parallax 58'	= 8.227134
:: Cos. altitude 36°	<b>9.907958</b>
: Sine parallax in altitude,	= 8.135092 $=$ 46', 55"
Refraction in altitude, 1'20"	-2' 8"
Meridional refraction, 48"	
-	44.' 47" Pro-
2' 8"	portional part in latitude
	36° at 3h. from the meridian,
	82 = 36', 43'' to be applied
	to the Moon's declination.

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# HOW TO FIND THE MERIDIONAL REFRACTION OF CELESTIAL OBJECTS IN ANY LATITUDE.

#### EXAMPLE.

In latitude 42° N., 90°—42—48°, Sun or star's declination north, + 15° 30′

The meridional altitude is 63° 30'.

The refraction of which is 29", (see table of refraction.)

41° 45%.

#### SECOND EXAMPLE.

In latitude 38° N., 90°—38°=52° 00′. Declination south, 10° 15′.

The meridional altitude is the refraction of which is 1'5"

# BAROMETER.

In view of the many hilly and mountainous districts yet to be surveyed, and their chorographical and geological characters defined, as well as for other purposes, the following table and theorems as given by Sir George Shuckburgh, will show in what manner the barometer is used for ascertaining the height of Mountains, Hills, &c.\*

Thermometer.	Factor.	Thermometer.	Factor.	Thermometer.	Factor.
0		0		0	
30	864.4	47	900.2	64	936.1
31	866.5	48	902.3	65	938.2
32	868.5	49	904.5	66	940.3
33	870.6	50	906-6	67	942.4
34	872.7	51	908.7	68	944.5
35	874.9	52	910.8	69	946.7
36	877.0	53	913.0	70	948.8
37	879.1	54	915.1	71	950.9
38	881.3	55	917.2	72	953.0
39	883.4	56	919.3	73	955.1
40	885.4	57	921.4	74	957.2
41	887.5	58	923.5	75	959-3
42	889.6	59	925.6	76	961.4
43	891.7	60	927.7	77	963.5
44	893.8	61	929.8	78	965-6
45	896.0	62	931.9	79	967.7
46	898.1	63	934.0	80	969-9

DEPRESSION OF MERCURY IN GLASS TUBES, OR CORRECTIONS TO BE . . ADDED FOR CAPILLARY ATTRACTION.

	INCHES.							
Diameter of Tube,	0. 25	0. 30	0.40	0. 45	0. 60			
Correction,	0.020	0.015	0.007	0.005	0.002			

<sup>\*</sup> To perform this operation accurately, two persons should take contemporary observations with two barometers and thermometers, the one at the bottom of the hill, and the other at the top.

RULE.—The difference between the two barometers at the bottom and top of the mountain, multiplied by the height of the barometer at the bottom of the mountain; and that product by the tabular difference corresponding to the mean of the thermometers, and divided by the mean between the readings of the barometers, will equal the amount of elevation in feet.

#### EXAMPLE.

Suppose the barometer at the bottom of the mountain to stand at 30 inches, thermometer 60°; and the barometer at the top 26.36 inches, thermometer 46°; required the height of the mountain.

As per rule the mean of the two barometers = 28.18 inches, their difference = 3.64 inches; and the mean of the two thermometers  $= 53^{\circ}$ . The number corresponding to  $53^{\circ}$  in the table is 913.0, hence  $(3.64 \times 30 \times 913.0) \div 28.18 = 3537.92 +$ . The height of the mountain.

The following are extracts from the remarks of the late eminent Dr. Halley:—

- "In calm weather, when the air is inclined to rain, the mercury is commonly low.
- "In serene, good weather, the mercury is generally high. Upon very great winds, though they be not accompanied with rain, the mercury sinks lowest of all, with relation to the point of compass the wind blows upon.
  - "In calm frosty weather, the mercury generally stands high.
- "Within the tropics, and near them, there is very little or no variation of the height of mercury in all weathers.
- "The greater height of the barometer, is occasioned by two contrary winds blowing towards the place of observation, whereby the air of other places is brought thither and accumulated."

In regard to the course of winds, and their effect on the barometer and weather, they are variable in different countries, and therefore omitted here.

Extracts from a Manual published by J. H. Belville of the Royal Observatory of Greenwich.

- "Heat and moisture are the principal causes of the variations in the weight of the atmosphere, and necessarily in the variations in the barometer at the same station."
- "The variations of the barometer, are less within the tropics, than in the temperate and polar regions; they vary in different



countries in the same latitude, and they are greater in mountainous countries, and islands. In Peru, the range of the mercury is about one-third of an inch—in London two and a half inches, and in St. Petersburg, it exceeds three inches."

"It is not so much the absolute height, as the actual rising and falling of the mercury, which determines the kind of weather likely to follow."

"Great depressions at all seasons are followed by change of wind, and by much rain."

"Rain in some quantity may fall with a high pressure, provided the wind be in any of the northerly points."

"No great storm ever sets in with a steady rising barometer."

"The variations of the barometer, are always greater in the winter than in the summer."

"Sudden depressions of the barometer, sometimes occur in weather apparently calm. It is almost an established fact, that storms have a circular motion; and, if when an exhaustion, or sudden diminution of the atmosphere takes place, the mercurial column happens to be in the partial vacuum or centre of motion, the air will be at rest; while the surrounding air at a greater distance from the centre, will be violently agitated with a less fall of the barometer."

N. B.—In all observations for this purpose, the rise and fall of the mercury should be reckoned from its mean height at whatever elevation the station may be above the sea level.

## ANEROID BAROMETER.

The Aneroid Barometer is a new instrument for ascertaining the variations of the atmosphere: its action depends on the effect produced by the pressure of the atmosphere on a metallic box, from which the air has been exhausted and then hermetically sealed: the hand of the Aneroid can be set to correspond with the mercurial barometer, by which it should be compared by turning a screw on its back-side. This screw when turned with, or against the sun, alters the position of the hand, and is not to be touched for any other purpose.

There is another gilt hand, called the register or index, which moves above the other by a nut or thumb piece which projects through the centre of the glass, to enable the observer to register the barometer hand, by which to refer its movement for another time, or in ascending or descending hills, &c.

The Aneroid Barometer can be carried and used through any country



with about the same safety as a watch, and is, therefore, the most suitable barometer of any now in use, for measuring the height of hills and mountains, in new countries.

The corrections for temperature for the Aneroid, are seldom precisely the same as for the mercurial barometer; but the quantity necessary for thermometrical correction can be readily found, by exposing the instrument to the temperature of the external air for twenty or thirty minutes, and set the hands coincident, then place it near the fire until the thermometer is at ninety or a hundred degrees; the variation of the hand, divided by the variation in degrees of the thermometer, will give the quantity for each degree.

#### MEASUREMENTS OF HEIGHTS WITH THE BAROMETER.

The following table, being an extract from the elaborate table of W. Galbraith, A. M., furnishes another expeditious method for this purpose.

In this table, the third column exhibits numbers in English feet, corresponding to the height of the barometer (shown on its left,) in inches, tenths, and hundredths, the proportional parts to thousandths are given in column headed A.

	,	<del>,</del>					,	
A.	Bar. Inch.	English Feet.	A.	Bar. Inch.	English Feet.	A.	Bar. Inch.	English Feet.
+	28.00	27425:3	+	28.20	27611.3	+	28.40	27795.8
0.9	1	27434.6	0.9	1	27620.6	0.9	1	27805.0
1.9	2	27444.0	1.9	2	27629.8	1.8		27814.2
2.8	3	27453.3	2.8	3	27639.1	2.8	3	27823.4
3.7	4	27462.6	3.7	3 5	27648.3	3.7	4	27832.6
4.7	4 5	27471.9	4.6	5	27657.6	4.6	2 3 4 5	27841.8
5.6	6	27481.3	5.6	6	27666.8	5.5	6	27851.0
6.5	7	27490.6	6.5	7	27676.1	6.4	7	27860.2
7.5	8	27499.9	7.4	8	27685.3	7.4	8	27869.3
8.4	9	27509.2	8.3	9	27694.6	8.3	9	27878 5
l		1	li	ł				}
+	28.10	27518.4	+	28.30	27703.7	0.9	28.50	27887.7
0.9	1	27527.7	0.9	1	27712-9		1	27896-9
1.9	2	27537.0	1.8	$\frac{2}{3}$	27722-2	1.8	$\frac{2}{3}$	27906.0
2.8	2 3 4 5	27546.3	2.8	3	27731.4	2.7	3	27915.2
3.7	4	27555.6	3.7	4 5	27740-6	3.7	4 5	27924.3
4.6		27564.9	4.6	5	27749.8	4.6	5	27933.5
5.6	6	$27574 \cdot 2$	5.5	6	27759.1	5.5	6	27942.6
6.5	7	27583.5	6.5	7	27768.3	6.4	7	27951.8
7.4	8	27592.7	7.4	8	27777.5	7.3	8	27960.9
8.4	9	27602.0	8.3	9	27786-7	8.2	9	27970-1
	ŧ.	1	[]	1	ŀ	į	1	

BAROMETRIC TABLE.

A.	Bar. Inch.	English Feet.	A.	Bar. Inch.	English Feet.	A.	Bar. Inch.	English Feet.
+ 0·9 1·8 2·7 3·7 4·6 5·5 6·4 7·3 8·2	28·60 1 2 3 4 5 6 7 8 9	27979·2 27988·3 27997·5 28006·6 28015·7 28024·8 28034·0 28043.1 28052·2 28061.3	+ 0·9 1·8 2·7 3·6 4·5 5·4 6·3 7·2 8·0	29·20 1 2 3 4 5 6 7 8	28521·7 28530·6 28539·6 28548·5 28557·5 28566·4 28584·3 28593·2 28602·2	+0.9 1.8 2.6 3.5 4.4 5.3 6.1 7.0 7.9	29·80 1 2 3 4 5 6 7 8	29053.1 29061-9 29070-6 29079-4 29088.1 29096.9 29105.6 29114.4 29123.1 29131-9
+ 0·9 1·8 2·7 3·6 4·5 5·5 6·4 7·3 8·2	28·70 1 2 3 4 5 6 7 8 9	28070·5 28079·6 28088·7 28097·8 28106·9 28115·9 28125·0 28134·1 28143·2 28152·2	+ 0·9 1·8 2·7 3·6 4·5 5·3 6·2 7·1 8·0	29·30 1 2 3 4 5 6 7 8	28611·1 28620·0 28628·9 28637·8 28646·7 28655·6 28664·5 28673·4 28682·3 28691·2	+ 0·9 1·7 2·6 3·5 4·4 5·2 6·1 7·0 7·8	29·90 1 2 3 4 5 6 7 8	29140·6 29149·3 29158·1 29166·8 29175·5 29184·2 29193·0 29201·7 29210·4 29219·1
+ 0·9 1·8 2·7 3·6 4·5 5·4 6·3 7·2 8·1	28-80 1 2 3 4 5 6 7 8	28161·3 28170·4 28179·4 28188·5 28197·5 28206·6 28215·6 28224.7 28233·7 28242·8	+ 0·9 1·8 2·7 3·6 4·4 5·3 6·2 7·1 8·0	29·40 1 2 3 4 5 6 7 8	28700·0 28708·9 28717·8 28726·6 28735·5 28744·4 28753·3 28762.1 28771·0 28779·9	+ 0.9 1·7 2·6 3·5 4·3 5·2 6·1 7·0 7·8	30·00 1 2 3 4 5 6 7 8	29227·8 29236·5 29245·2 29253·9 29262·6 29271·3 29280·0 2928·7 29297·3 29306·0
+ 0.9 1.8 2.7 3.6 4.5 5.4 6.3 7.2 8.1	28.90 1 2 3 4 5 6 7 8 9	28251·8 28260·8 28260·9 28278·9 28287·9 28296.9 28306·0 28315·0 28324·0 28333·0	+ 0·9 1·8 2·7 3·5 4·4 5·3 6·2 7·1 8·0	29·50 1 2 3 4 5 6 7 8	28788·7 28797·5 28806·4 28815·2 28824·1 28832·9 28841·8 28850·6 28859·4 28868·2	+ 0.9 1.7 2.6 3.5 4.3 5.2 6.1 6.9 7.8	30·10 1 2 3 4 5 6 7 8	29314·7 29323·4 29323·0 29340·7 29349·2 29358·0 29366·7 29375·3 29384·0 29392·6
+ 0·9 1·8 2·7 3.6 4·5 5·4 6·3 7·2 8·1	29·00 1 2 3 4 5 6 7 8	28342·1 28351·1 28360·1 28369·1 28378·1 28396·1 28405·0 28414·0 28423·0	+0.9 1.8 2.6 3.5 4.4 5.3 6.2 7.0 7.9	29·60 1 2 3 4 5 6 7 8	28877-1 28885-9 28894-7 28903-6 28912-4 28921-2 28930-0 28938-8 28947-6 28956-4	+ 0.9 1.7 2.6 3.5 4.3 5.2 6.1 6.9 7.8	30·20 1 2 3 4 5 6 7 8	29401·3 29409·9 29418·6 29427·2 29435·9 29444·5 29453·2 29461·8 29470·4 29479·1
1.8 2.7 3.6 4.5 5.4 6.3 7.2 8.1	29·10 1 2 3 4 5 6 7 8 9	28432·0 28441·0 28450·0 28458·9 28467·9 28476·9 28485·8 28494·8 28503·8 28512·7	+ 0·9 1·8 2·6 3.5 4·4 5·3 6·1 7·0 7·9	29·70 1 2 3 4 5 6 7 8	28965·2 28974·0 28982·8 28991·6 29000·4 29009·1 29017·9 29026·7 29035·5 29044·2	1·7 2·6 3·4 4·3 5·2 6·0 6·9 7·7	30·30 1 2 3 4 5 6 7 8 9	29487·7 29496·3 29504·9 29513·6 29522·2 29530·8 29539·4 29548·0 29556·6 29565·2

A.	Bar. Inch.	English Feet.	A.	Bar. Inch.	English Feet.	A.	Bar. Inch.	English Feet.
+	30.40	29573.8	+	30.60	29745.0	1+	30.80	29915.2
0.9	1	29582.4	0.9	1	29753.5	0.8	1	29923.7
1.7	2	29591.0	1.7	2 3	29762-1	1.7	2	29932.2
2.6	3	29599.6	2.6	3	29770.6	2.5	3	29940.7
3.4	4 5	29608-2	3.4	4 5	29779.1	3.4	4 5	29949.2
4.3	5	29616.7	4.3	5	29787.6	4.2	5	29957.6
5.2	6	29625.3	5.1	6	29796.2	5.1	6	29966.1
6.0	7	29633.9	6.0	7	29804.7	5.9	7	29974.6
6.9	8	29642.5	6.8	8	29813.2	6.8	8	29983.1
7.7	9	29651.0	7.7	9	29821.7	7.6	9	29991.5
	1			1	1	1		l i
0.9	30.50	29659.6	+	30.70	29830.2	0.8	30.90	30000.0
	1	29668.1	0.9	1	29838.7	0.8	1	30008.5
1.7	2	29676.7	1.7	2	29847.2	1.7	2	30016.9
2.6	3	29685.2	2.5	3	29855.7	2.5	3	30025.4
3.4	4 5	29693.8	3.4	4	29864.2	3.4	4 5	30033.8
4.3	5	29702.3	4.3	5	29872.7	4.2	5	30042.3
5.1	6	29710.9	5.1	6	29881.2	5.1	6	30050.7
6.0	7	29719.4	6.0	7	29889.7	5.9	7	30059.2
6.8	8	29727.9	6.8	8	29898-2	6.8	8	30067.6
7.7	9	29736.5	7.7	9	29906.7	7.6	9	30076.1
L	1	1	11 -	1	1	11		

#### EXAMPLE.

At the foot of a hill the barometer indicates 29.54 inches, then carried immediately to the top of the hill reads 28.70 inches. In the table at 29.54 we find 28824.1 feet.

at 28.70 we find

-28070.5 feet,

Height of hill

753.6 feet.

To perform this operation accurately, when the interval of time exceeds ten minutes between the two observations, two persons should take contemporary observations, with two Aneroid Barometers, one at the foot, and the other at the top of the hill, and correct each for temperature.

# SYSTEM OF SURVEYS OF THE U.S. LANDS.

The public lands of the United States are surveyed in a uniform mode established by law, by lines run by the cardinal points of the compass; the north and south lines coinciding with the true meridian, and the east and west lines intersecting them at right angles, giving to the tracts thus surveyed the rectangular form.

The public lands are laid off and surveyed, primarily, into tracts of six miles square as near as practicable, called townships, containing 23040 acres each. The townships are subdivided into thirty-six tracts, called sections, each of which is one mile square, as near as may be, and contains 640 acres. Any number, or series, of contiguous townships, situated north or south of each other, constitute a Range.

To obtain and preserve a convenient and uniform mode of numbering the ranges and townships, it is usual in commencing the survey of an insulated body of public lands to run, or assume two standard lines, as the basis of the survey to be made therein. One of these standard lines is run due north and south, and is called the principal meridian, to which the ranges are parallel, and from which they are numbered eastward and westward. The other standard line is run due east and west, and is called the base line, from which the townships are numbered, northward and southward.

To distinguish from each other, the systems, or series of surveys thus formed, the several principal meridians are designated by progressive numbers. Thus the meridian running north from the mouth of the Great Miami river, is called the first principal meridian: the meridian running north through the centre of the State of Indiana, is called the second principal meridian: that running north from the mouth of the Ohioriver, through the State of Illinois, is called the third principal meridian: that running north from the mouth of the Illinois river, through the States of Illinois and Wisconsin, is called the fourth principal meridian: and that running north from the mouth of the Arkansas river, through the states of Missouri and Iowa, is called the fifth principal meridian.

Correction Lines correct the error that would otherwise arise from the convergency of meridians, and arrest that proceeding from the inaccuracies of measurement. They are run due east and west at stated distances, generally at the end of every tenth township, and each forms a base for the townships north of it. Each range of townships should be made as much over six miles in width on each base and correction line as it will fall short of the same width where it closes, on the next correction line north, the excess or deficiency of width being always thrown into the last half mile, on all of the lines closing out to the west boundary of each township.

This mode of executing the public surveys, conduces more, perhaps, than any other which could be devised, to the simplicity, regularity, and symmetry of the work, and to the ease and certainty with which any tract may be identified.

The public lands are surveyed by Deputy Surveyors, appointed by the Surveyor General of the State or Territory, in which the district assigned to each deputy may be situated; their duties are prescribed by general and special instructions.

## OF SUBDIVIDING TOWNSHIPS.

Each township is laid off and surveyed into thirty-six sections as near as may be of one mile square, by lines running north and south, crossed by others running east and west. The sections are known and designated by progressive numbers, beginning at the north-east corner of the township, and numbering westward and eastward alternately, as shown in the following diagram.

6	5	4	3	2	1
7	8	9	10	11	12
18	17	16	15	14	13
19	20	21	22	23	24
30	29	28	27	26	25
31	32	33	34	35	36

Quarter section corners are established equidistant between the section corners, except on the section lines closing on the north and west boundaries of townships, on which they are set at forty chains from the last section corner, and the excess or deficiency of measure (if any) is carried out into the last half mile, and cast upon the north and west sides of the township, as required by law. Various instructions have been given by Surveyors General, to Deputy Surveyors, for the purpose of accomplishing an equitable and lawful subdivision of townships into sections, none of which, it is believed, will effect this object better than the system adopted in 1850, by the surveyor general of Ohio, Indiana, and Michigan; by which the true course and measurement of every line is given, and the inequalities of measurement proportionally carried to every sectional This, together with the closing of the section lines at post on the north and west boundaries of the townships, (which were formerly closed at the intersection of the lines run to them, whether at post or not,) has much improved the symmetry and equality of the subdivision of townships.

An act of Congress of the 24th May, 1824, authorizes a departure from the ordinary mode of surveying the public land, on any river, lake, or bayou, whenever, in the opinion of the President of the United States, the public interest would be promoted thereby, so as to survey such lands, in tracts of two acres in width fronting on such river, lake, or bayou, and running back to the depth of forty acres.

ON SUBDIVIDING SECTIONS, AND RE-ESTABLISHING OF EXTINCT LINES
AND CORNERS: DEDUCED FROM THE ACTS OF CONGRESS, IN REGARD
TO THE SURVEYS OF THE PUBLIC LANDS; AND THE CONSTRUCTIONS
AND USAGES THEREON.

The general principles on which the public lands are surveyed, have already been given; but the county surveyors and purchasers of these lands, are more immediately interested in the proper method of subdividing sections into such tracts as are sold to purchasers from the United States land offices; and the re-establishing of extinct lines and corners, when from any cause they are lost or cannot be found.

In the regular surveys of the public lands, no other lines are actually run and marked by the Deputy Surveyors of the United States, than township lines, and sections, or subdivisional lines of

townships, into sections; on all of these lines, no other than section and quarter section corners are established; except meander corners at the end of all fractional section lines which close on rivers, lakes, &c.

All sections in a full township, except those which are bounded by its north and west sides, are treated as full sections in their sales and subdivisions; and also, the south half of sections on the north boundary, and the east half of sections on the west boundary of each full township, are sold and subdivided as full half sections. Section sixteen in each township is reserved for school purposes, and is not, therefore, subject to private entry.

From various causes (elsewhere treated of in this work) section lines do not always correctly coincide with the cardinal points; nor will their measurement in all cases be found exactly eighty chains or one mile in length. (See article on measurement with the chain.) Quarter section corners, especially in the older surveys, may not always be found equidistant between the section corners. This defect arises in most cases, it is believed, from difficult or careless measurement with the chain.

Notwithstanding such errors, all corners that can be identified by the original field notes, or other unquestionable testimony, must be regarded as the original corners, and for that purpose should be perpetuated with new posts and bearings when the old ones decay.

## EXTINCT LINES AND CORNERS.

When a Section corner cannot be identified by the original field notes, or by clear and unquestionable testimony, run a right line between the nearest noted station trees, north and south, and east and west of the lost section corner, if there be any such trees within the distance of the nearest quarter section, or section corners; but if no station trees be found, then between the nearest quarter section or section corners, and at the point of intersection of these two lines re-establish the section corner, with new bearings from it to the nearest and most durable objects; which of course should be recorded with the survey.

Extinct Quarter Section corners, except on fractional section lines, if not identified as above stated for section corners, must be re-established equidistant between the section corners, in a right line between the nearest noted station trees each side of it, if there be

any; but if none are found, then in right line between the section corners.

Extinct Quarter Section corners, on section line, which close on the north and west boundaries of townships, must be re-established according to the original measurement thereof, at forty chains from the last interior section corner towards the township line. For an example, suppose the line between sections 3 and 4, or 18 and 19, to be 81.30 chains, according to the original survey, and by the measurement of the county survey, 80.90 chains. Then say as 81.30: 80.90:: 40.00 to = 39.81½. Thus 39 chains and 81½ links is the distance the quarter section corner must be established from the last interior section corner, according to the measure of the county surveyor.

Lost or extinct Township corners, except on correction lines, should be restored in the same manner as already given for section corners; and extinct quarter section corners on township lines, should be restored in the same manner as those on interior section lines.

In subdividing townships into sections, the section lines which close on the north and west boundaries of townships, have not always been closed at the section corners which were established on the survey of the township lines; but at such points on their boundaries, as the first lines run to them may have intersected.

Wherever this has been done on the north and west boundaries of townships, a new quarter section corner must be established, equidistant between the corners of all such irregular closing lines; for, the section and quarter section corners established on the survey of these boundaries, belong exclusively to the adjoining township. Consequently, to restore lost or extinct section corners, that were established on the north and west boundaries of townships, during their subdivisions into sections as above mentioned, the section lines closing at these corners, must be retraced to them. But to restore lost section, or quarter section corners, that were established on the original survey of the township lines, these boundaries should be carefully retraced and measured, and the lost section and quarter section corners should be re-established at their proportional distance from each other, between known corners. The only exception to this rule is, when it is clear that the section lines have been regularly run according to instructions, and can be correctly retraced to the township line. The section corners should then be re-established at such intersections.



Extinct or obliterated lines may be restored by running right lines between re-established and other known corners; except noted station trees be found between them, when the lines between corners must conform to the noted station trees.

It may be remarked here that no surveyor can legally alter or correct the original surveys. It is his duty to restore them as far as practicable to their original condition.—In making resurveys of the public lands, such directions and absolute length must be given to each line as were given to them by the original surveyor, whether the retracing, courses and measurements, agree with the original survey or not; except otherwise directed by the Surveyor General, or the Commissioner of the general Land Office.

## BEARING TREES, &c.

Bearing trees, to corners, have a blaze with a notch in them near the ground and facing the corner; sometimes the letters B T are found in the blaze above or below the notch, which are the initials of Bearing Tree. Their size, kind of timber, course and distance from the corner post, is given in the field notes of the survey.

Section, and quarter section trees are "faced off" on the side towards the corner, four or five feet from the ground. The quarter section trees are marked thus ½ S. At section corners these trees are marked with the number of the Range, Township and Section, thus, R. 24 W. T. 45 N. S. 15.\* There is no note made of these trees in the field books, unless they are bearing trees also; they are marked for the purpose of giving information at the corner, of the number of the sections which corner there, and also, the number of the township and range. Station trees on the lines, are notched with two notches on each side in the direction of the line, and their size, kind of timber, and distance from the last section corner are given in the field notes.

#### SUBDIVISION LINES OF SECTIONS.

The subdivisions of whole sections into such tracts as are sold by the land officers of the United States, to purchasers of public lands, are made by running right lines between the quarter section corners, on the north and south, and east and west sides of the section; and at the intersection of these lines is established the common corner for

<sup>\*</sup> In prairies, the posts set in mounds for corners are marked in like manner.



its four quarters, without regard to the quantity of land contained in each of them. These quarter sections are sold as containing 160 acres each, and are designated as the N. E., N. W., S. E. and S. W. quarters.

Quarter sections are divided into halves, by a north and south line, equidistant by measurement between its east and west corners. These tracts of land are supposed to contain eighty acres each, and are designated as the east and west half of the quarter section.

Furthermore a quarter section is, also, divided into quarters by lines run north and south, and east and west, equidistant between its four corners, and at the intersection of these lines at the centre of the quarter section, is established the common corner to its four quarters. These quarters of a quarter section are supposed to contain forty acres each, and are described as the N. E., N. W., S. E. and S. W. quarters of the quarter section.

The following diagram of the subdivision of a whole section, will more clearly show the method of subdividing such section.

		79	68		
1	39	·84	19.91	19.91	
	39.96	00	00.02 19.96 <sup>1</sup> / <sub>2</sub>	70.00 19·96 <sup>1</sup> /2	
2	88 40	00.04	00 10 00 00 00 20 02	20·02	œ
79-92	20.02	20.02	20 02	2002	80.08
1-	86-61 20-07		, 20	4	
	19-98	40.00	40.02	40-04	
	20.12	20.12	20.12	20.12	
		80	48		

Quarter sections adjoining the north and west boundaries of townships, are deemed to be fractional, and therefore, may contain more or less land, than is given to other quarter sections within the townships; they are sold or surveyed according to their plats in the land offices.

### ON SUBDIVIDING FRACTIONAL SECTIONS.

Fractional section lines which close on meandered rivers and lakes, or on reservations, &c., are required by law to be run north and south, or east and west, as the case requires. These lines like those before mentioned in the subdivisions of townships into sections, may not precisely agree with the cardinal points of the compass.—Therefore, in subdividing fractional sections embraced by fractional section lines, which close on meandered streams, lakes, &c.; the quarter section line should be run with an intermediate course between the section lines; and the fractional quarter sections thereof, should be divided in like manner.

The subdivisions of fractional sections, are indicated on the maps of surveys, in the land offices.

# AN ACT CONCERNING THE MODE OF SURVEYING THE PUBLIC LANDS OF THE UNITED STATES.

¿ I. Be it enacted, &c. That the Surveyor General shall cause all those lands north of the river Ohio, which, by virtue of the act entitled, "An act providing for the sale of the lands of the United States in the territory northwest of the river Ohio, and above the mouth of the Kentucky river," were subdivided, by running through the townships parallel lines, each way, at the end of every two miles, and by marking a corner on each of the said lines, at the end of every mile, to be subdivided into sections, by running straight lines, from the mile corners thus marked to the opposite corresponding corners, and by marking, on each of the said lines, intermediate corners, as near as possible equidistant from the corners of the sections of the same. And the said Surveyor General shall also cause the boundaries of all the half section, which had been purchased previous to the first day of July last, and on which the surveying fees had been paid according to law by the purchaser, to be surveyed and marked, by running straight lines from the half mile corners heretofore marked, to the opposite corresponding corners; and intermediate corners shall at the same time, be marked on each of the said dividing lines, as nearly as possible equidistant from the corners of the half section on the same line: Provided, That the whole expense of surveying and marking the lines, shall not exceed three dollars for every mile which has not yet been surveyed, and which shall be actually run, sur-

veyed and marked, by virtue of this section. And the expense of making the subdivisions directed by this section, shall be defrayed out of the moneys appropriated, or which may be hereafter appropriated, for completing the surveys of the public lands of the United States.

¿ II. That the boundaries and contents of the several sections. half sections, and quarter sections, of the public lands of the United States, shall be ascertained in conformity with the following principles, any act or acts to the contrary notwithstanding:-1st. All the corners marked in the surveys returned by the Surveyor General, or by the surveyor of the land south of the state of Tennessee respectively, shall be established as the proper corners of sections, or subdivisions of sections, which they were intended to designate; and the corners of half and quarter sections, not marked on said surveys, shall be placed as nearly as possible equidistant from those two corners which stand on the same line. 2d. The boundary lines, actually run and marked in the surveys returned by the Surveyor General, or by the surveyor of the land south of the state of Tennessee, respectively, shall be established as the proper boundary lines of the sections, or subdivisions for which they were intended; and the length of such lines, as returned by either of the surveyors aforesaid, shall be held and considered as the true length thereof. And the boundary lines which shall not have been actually run and marked as aforesaid, shall be ascertained by running straight lines from the established corners to the opposite corresponding corners; but in those portions of the fractional townships, when no such opposite corresponding corners have been or can be fixed, the said boundary lines, shall be ascertained by running from the established corners. due north and south or east and west lines, as the case may be, to the water course, Indian boundary line, or other external boundary of such fractional township. 3d. Each section, or subdivision of section, the contents whereof shall have been, or by virtue of the first section of this act, shall be returned by the Surveyor General, or by the surveyor of the public lands south of the state of Tennessee, respectively, shall be held and considered as containing the exact quantity expressed in such return or returns; and the half sections and quarter sections, the contents whereof shall not have been thus returned, shall be held and considered as containing the one half, or the one fourth part, respectively, of the returned contents of the section of which they make part.  $\mathsf{Hosted}\,\mathsf{by}\,Google$ 

₹ III. That so much of the act, entitled "An act making provision for the disposal of the lands of Indiana territory, and for other purposes," as provides the mode of ascertaining the true contents of sections, or subdivisions of sections, and prevents the issue of final certificates, unless the said contents shall have been ascertained, and a plot certified by the District Surveyor, lodged with the register, be, and the same is hereby repealed. [Approved, February 11, 1805.]

# GEOLOGICAL AND TOPOGRAPHICAL IN CONNEXION WITH LINEAR SURVEYS.

#### GEOLOGICAL SURVEYS.

In connexion with the linear surveys of new districts of country, the surveyors have good opportunities to make geological examinations, and to collect specimens of minerals that may be discovered in the course of their work. Such specimens, when submitted to a scientific and practical geologist, will enable him to determine the true character of such new districts, and what kinds of products may be expected to be derived from them.

It is, therefore, of much importance, that surveyors of the public land should possess or acquire, at least a sufficient knowledge of geology, to enable them to make a proper collection of geological specimens; and also, to observe the character, stratifications, dip, &c., of any rocks in place, or other mineral deposits.

Such services afford pleasure and profit to the surveyors, while they contribute to the public interest, and to science. A system of surveys for this purpose has been partly tested; but while in successful progress, it was interrupted by the death of the geologist, the lamented Dr. Douglass Houghton, while he was engaged in prosecuting a geological, in connexion with the linear survey, of the south coast of Lake Superior.

This system possesses many advantages over any other that has been adopted, for obtaining a general geological knowledge of new and unsettled countries, the expense of which is trifling compared with an independent geological survey; also, such surveys are of great value when known, in directing emigrants to the country suitable for their occupation or enterprise, and thus effect an early and judicious development of its resources.

A system of linear and geological surveys may be satisfactorily prosecuted, by the appointment of a competent geologist to a clerkship in each Surveyor General's office: the Deputy Surveyors being made assistant geologists to execute the field work, under a well digested system for that purpose, who should make their report, and return their specimens to the Surveyor General, when the geologist under him can investigate such reports, and embody the whole in one connected geological report, so far as such surveys extend.

By this system, it will be seen that the position of all mineral deposits from which specimens are taken, may be precisely located by measure on the survey, and be as easily found as the various section, quarter section, and other subdivisions themselves, a consideration of much importance, which any independent geological or other system yet adopted fails to do.

#### TOPOGRAPHICAL SURVEYS.

The general topographical features of new districts of country are of much interest to the public, and especially to emigrants. surveys can be made with but little expenditure of time while the linear surveys are in progress, by a proper use of the Aneroid Barometer, for the purpose of determining on the lines, the height of hills, ledges, &c., above the valleys; (see article on the use of the Aneroid Barometer) and by observing also, the course and angle of elevation or depression of distant noticeable objects, on the summits of hills, mountains, ledges, &c., and in the valleys below them; which can be seen from two or more stations on the lines at the time they And further, when running the meanderings of are being run. the shores of rivers or lakes, bearings and angles of elevation may be also taken to conspicuous objects on islands, rocks, sand-bars, &c., which can be seen from their shores. To these observations should be added, sketches of landscapes, ledges, and whatever else may interest the inquiring mind.

Such bearings, and angles of elevation and depression, form triangles with a given base to each, which are good data for mapping, or trigonometrical calculations, to establish the course, distance, elevation or depression, from a fixed point within the survey of every object with which they are connected.\*

<sup>\*</sup> In making calculations for the heights of distant objects, the table for corrections for curvature and refraction, will give the number of feet to be added to their height; on the account of the difference of the apparent and true level from the point of observation.  $\mathbf{G} * \mathbf{Hosted} \text{ by Google}$ 

TABLE OF CORRECTIONS FOR CURVATURE AND REFRACTION, SHOWING THE DIFFERENCE OF THE APPARENT AND TRUE LEVEL, IN FEET AND DECIMALS OF A FOOT, FOR DISTANCES IN FEET AND MILES.

Feet.	CORRI	ection in	FEET.		CORR	LECTION IN F	CET.		
Distances in	For Curvature.	For Refraction.	For Curra- ture and Refraction.	Distances in Miles.	For Curvature.	For Refraction.	For Curva- ture and Refraction.		
100	·00024	.00004	*00020	1/4	·0417	·0060	·0857		
150	·00054	.00008	*00046	1/5	·1668	·0238	·1430		
200	·00094	.00013	*00083	3/4	·3752	·0536	·3216		
250	·00149	.00021	*00128	1	·6670	·0953	·5717		
300	·00215	.00031	*00184	1/ <sub>2</sub>	<b>1</b> ·5008	·2144	1·2864		
350 400 450 500 550	.00293 .00383 .00484 .00598 .00724	.00042 .00055 .00069 .00085 .00103	.00251 .00328 .00415 .00513 .00621	$\begin{array}{c c} 2 \\ 2^{1}/2 \\ 3 \\ 3^{1}/2 \\ 4 \end{array}$	2 6680 4 1688 6 0030 8 1708 10 6720	•3811 •5955 •8561 1•1673 1•5246	$\begin{array}{c} 2.2869 \\ 3.5733 \\ 5.1469 \\ 7.0035 \\ 9.1474 \end{array}$		
600	*00861	*00123	*00738	$ \begin{array}{c c} 4^{1}/_{2} \\ 5 \\ 5^{1}/_{2} \\ 6 \\ 6^{1}/_{2} \end{array} $	13·5468	1·9295	11·5773		
650	*01010	*00144	*00866		16·6750	2·3821	14·2929		
700	*01172	*00167	*01005		20·1769	2·8824	17·2945		
750	*01345	*00192	*01153		24·0120	3·4303	20·5817		
800	*01531	*00219	*01312		28·1809	4·0258	24·1551		
850	·01728	·00247	·01481	7	32·6830	4·6690	28·0143		
900	·01938	·00277	·01661	7 <sup>1</sup> / <sub>2</sub>	37·5190	5·3599	32·1591		
950	·02159	·00308	·01851	8	42·6880	6·0997	36·5883		
1000	·02392	·00333	·02059	8 <sup>1</sup> / <sub>2</sub>	48·1910	6·8844	41·3066		
1050	·02638	·00377	·02261	9	54·0270	7·7181	46·3089		
1100	·02895	*00414	·02481	$ \begin{array}{c c} 9\frac{1}{2} \\ 10 \\ 11 \\ 12 \\ 13 \end{array} $	60·1971	8·5996	51·5975		
1150	·03164	*00452	·02712		66·7000	9·5286	57·1714		
1200	·03445	*00492	·02953		80·7070	11·5296	69·1774		
1250	·03738	*00534	·03204		96·0480	13·7211	82·3269		
1300	·04043	*00578	·03465		112·7230	16·1033	96·6197		
1350	•04361	.00623	·03738	14	130·7320	18·6760	112·0560		
1400	•04689	.00670	·04019	15	150·0750	21·4393	128·6357		
1450	•05030	.00719	·04311	16	170·7520	24·3931	146·3589		
1500	•05383	.00769	·04614	17	192·7630	27·5376	165·2254		
1550	•05748	.00821	·04927	18	216·1086	30·8727	185·2359		
1600 1650 1700 1750 1800	*06125 *06514 *06914 *07327 *07792	*00875 *00931 *00988 *01047 *01107	*05250 *05583 *05926 *06280 *06645	19 20 For a	240·7870 266·8000	34·3981 38·1143 pproximation	206·3889 228·6857		
1850	·08188	·01170	.07018	Correction for Curvature in feet $=\frac{2}{3}$ D being distance in miles.					
1900	·08637	·01234	.07403						
1950	·09098	·01300	.07798						
2000	·09570	·01367	.08203						

A useful application of a series of triangles can be made across lakes, bays, harbours, &c., commencing from a correctly measured base, on or near their coasts, so connected with every point or object on their shores or within their waters, that the meanderings of their shores, and position of islands, sand-bars, soundings or other objects can be correctly delineated on a map, by course and distance from any known point of survey. A full description of the above principles with proper examples, would occupy too much space to be admitted here, but it is believed that the well qualified practical surveyor, will find but little, if any difficulty in applying these principles to any survey that may require their use.

# OUTFIT FOR A SURVEYING COMPANY OF SIX MEN FOR FOUR MONTHS IN THE PUBLIC SURVEYS.

## SUPPLIES OF PROVISION.

The following quantity and kinds, or a substitute for them, is generally required.

- 8 barrels of flour.
- $2\frac{1}{2}$  do. of clear pork.
- 3 bushels of beans.
- 2 do. of dried apples.
- 120 lbs. of good dry sugar.
  - 70 lbs. of ground coffee, or a substitute for it.
  - 10 lbs. of saleratus, or its substitute.
  - 1 lb. of ground pepper.
  - 1 small bag of table salt.
  - 25 lbs. of rice.
  - 4 lbs. of Castile soap.

## CAMP FURNITURE.

- 1 large tent for the surveying company.
- 1 small tent for the packmen.
- 6 Mackinaw blankets.
- 3 common blankets to spread underneath them.
- 2 dozen boxes of matches. (best kind.)
- 1 good chopping axe.
- 4 tin pails, made to fit into each other.
- 14 tin basins.
- 1 set of knives and forks. (Small size.)
- 1 butcher, or meat knife.

- 7 spoons.
- 3 light frying pans.
- 2 half round cans, made to fit inside of the pails,—for lard and saleratus.
- 2 tin pepper boxes, with covers to fit closely over the sieve.
- 6 "soldiers' drinking cups," also needles, awls, thread, twine, small cord, &c.
- 2 mixing cloths, made of heavy cotton drilling, one yard square each.
- 4 papers of 3 oz. tacks for nailing boots.

## FOR PACKING, ETC.\*

- 1 or 2 good horses, or mules, as circumstances require; one pack saddle; a bell and spancil for each.
- 20 stout bags, that hold one and a half bushels each.
  - 4 linen bags, for pork.
  - 6 small bags, for beans, dried apples, knives and forks, &c.
  - 3 India Rubber bags for sugar and coffee. (Should be lined.)
  - 2 strong drilling cloths, two or two and one half, yards square, to do up the camp equipage into packs; also, strap and cords, to secure the packs to the horse and saddle.

### SURVEYING INSTRUMENTS, ETC.

- 1 solar compass.
- 1 case of drawing instruments.
- 1 measuring chain.
- 1 standard chain.
- 11 tally pins.
- 1 tape measure.
- 1 Telescope 16 or 18 inches in length.
- 2 marking tools.
- 2 pocket compasses.
- 2 marking axes, weighing three and a half pounds each.
- 1 hatchet, and two whetstones.
- 2 three-cornered files, for sharpening axes, &c.
- 2 small round files for sharpening marking tools. Also, field books, mapping and writing paper, ink, pens, pencils, India rubber, mouth glue, and a small valise (or box) to carry them in.

<sup>\* &</sup>quot;Packing." This word is used by surveyors of the public lands, both for making up and conveying packs.

### Remarks.

Camp pails, or kettles, should be made of heavy tin, and the covers and ears riveted, where they would be likely to separate when exposed to the fire.

The most approved form of a camp pail is an elliptical, or oblong bottom, with upright sides. The largest pail should be made about nine inches in depth, and to hold twelve quarts, or more; the other three of a less size, so as to fit inside of the largest one.

The basins are made six or seven inches in diameter, and one and a half inch in depth; they serve in the place of plates, cups, soup and meat dishes, &c. The knives, forks, and spoons, should be of a small size, except one large spoon for mixing bread, &c.

Flour is mixed for bread on a cloth of cotton drilling, of about one yard square. It is done as follows:—

Spread the cloth on a blanket, folded and laid on the ground; pour enough flour upon it for a mixing, and make a hollow in it; then pour in some lard from the can, and add saleratus and salt dissolved in warm water, stirring the flour with a spoon to a proper consistency for kneading with the hand, taking care not to reach the bottom of the flour so as to wet the cloth.—Bake the loaves in the frying pans before the fire, and when done, fold the cloth, and lay it aside for future use.

#### TENTS.

The soldiers' tent made of good firm cotton drilling, will answer the purpose very well, in any country. The Marquée, however, is better in a prairie country. Another tent, much approved by some surveyors, for a timbered country, is made of good cotton drilling: when pitched, nearly resembles a little more than one half of a steep roofed building, with its share of the ends. It can be quickly pitched with poles, and crotches, by having suitable eyelets, and strings at the bottom, and at the ridge, and front. It has four or five breadths of cloth, about four and one third yards in length; the end may be made of cotton sheeting, of the form above indicated. This tent possesses the advantage of being less in weight and bulk, than any other in use among surveyors: therefore, very suitable to be used when the carrying is done by men.



## CONVEYING PACKS WITH HORSES OR MULES.

The man who manages the pack horse, should be an experienced woodsman, capable of finding his way with the help of a pocket compass, to any point within the district to be surveyed, that may be designated by the surveyor.

The "sack Indian saddle" is the best in use for the purpose of packing, but pack saddles may be made in the form of those used by most of the Indian tribes. They should have attached to them a stout girt, breast strap, and breeching, and be well padded, or have a folded blanket under it, when in use.

Suitable straps with buckles should be provided, to tightly buckle around near the ends of each bag, or articles done up with a wrapper and cord, which are intended for side packs. Before buckling these straps, a loop made of strong cord about ten inches long, should be slipped on to each; after buckling the straps, these loops will be hitched over the horns of the saddle, and wound around them if too long: thus each side pack lies lengthwise of the horse, suspended by the loops from the horns of the saddle.

Between the side packs other loose articles may be placed, such as tin pails, frying pans, &c. These bags and other loading, should be well balanced, and bound to the horse and saddle, with a cord of suitable length. That the horse may be easily found when not at work, a small bell should be fastened to his neck, with a strap and buckle. A "spancil" should also be provided, made of leather with two buckles, for fastening the forefeet of the animal nearly together, that he may not go astray.

#### CONVEYING PACKS WITH MEN.

When packs cannot be carried on horses, or mules, men are employed for that purpose, and should be provided with suitable pack straps. The "portage strap" is sometimes used: it is made of leather, and is ten or twelve feet in length; the middle part is two feet long, and three inches broad in the middle, and tapers each way; at each end of this broad part is secured a thong of leather, sufficiently strong to support the pack. Each end of the portage strap is tied around the pack to be carried: the broad part passes over the forehead, or chest of the person who conveys it.

Another "pack strap" in common use, is made of five straps;

two of them are buckled around the pack near each end, and two are slipped under them and sewed together, in such a manner, as when buckled, to form shoulder straps; the fifth strap is about three inches broad at the middle, and tapers each way, and is buckled at each end to the other straps, in such a manner as to pass over the forehead when in use; the pack is put on in a similar manner to that of a peddler's pack.

Packs which are carried by men, to supply a surveying company in the field, usually weigh from seventy-five to a hundred and twenty pounds each.

### SURVEYORS' WEARING APPAREL.

The common wool hat is best for any season of the year, especially in timbered land.

Trowsers should be made large, and of strong cloth.

A light coat, or frock, should be provided, well supplied with waterproof pockets, to keep books and papers dry in wet weather, and a light India rubber, or water proof cape should also be provided to keep the compass dry, when travelling in wet weather.

Flannel for under clothes, is preferable to cotton, for all seasons and kinds of weather.

Boots may be made of good kip skin, and rather larger than for ordinary use; the fronts of the legs should be cut narrower, and the backs wider, than is usual to cut them. A thick single sole projecting about one quarter of an inch from under the upper leather, and well nailed over the bottoms with sparables, or tacks, are the most durable. The nails keep the feet from slipping, and the broad sole protects the upper leather from wearing against bushes, grass, &c. A large silk handkerchief, of any colour but red, to tie over the ears and neck, is a good protection from flies and musquitoes.

#### DEPOTS IN ADVANCE OF A SURVEY.

Much difficulty has sometimes been experienced by surveyors in new and unsettled countries, in providing an ample supply of provisions for their parties while engaged in large surveys of exterior township lines. This difficulty can be overcome in a great measure by the use of the solar compass. The latitude of the township corner, which is to be the commencing point of the survey, must be determined with the instrument to be used in executing the work;



then convey the supplies by the most feasible route, to the desired position within the district to be surveyed, and deposit it securely from storms and wild animals, on or near some stream, lake, Indian trail, or other conspicuous object that can be recognised, in the latitude of any east and west township line; which may be determined by allowing 5' 12" of latitude for each township of six miles north or south of the commencing corner of the survey. If the township line, when run, should pass a few chains to the right or left of the depot thus made, it can be found in a few minutes.

This method of depositing supplies of provisions in advance of the surveyed lines, has been successfully practised by the author.

## TRAVERSE TABLE.

SHOWING THE DIFFERENCE OF

## LATITUDE AND DEPARTURE

FOR

DISTANCES BETWEEN 1 AND 100;

AND FOR

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61 62 63 64 65 66 67 68 69 70	60·99 61·99 62·99 63·99 64·99 65·99 66·99 67·99 68·99 69·99	1.06 1.08 1.10 1.12 1.13 1.15 1.17 1.19 1.20 1.22	60·99 61·99 62·99 63·98 64·98 65·98 66·98 67·98 68·98 69·98	1·33 1·35 1·37 1·40 1·42 1·44 1·46 1·48 1·51 1·53	60.98 61.98 62.98 63.98 64.98 65.98 66.98 67.98 68.98 69.98	1.60 1.62 1.65 1.68 1.70 1.73 1.75 1.78 1.81	60.97 61.97 62.97 63.97 64.97 65.97 66.97 67.97 68.97 69.97	1.86 1.89 1.92 1.95 1.99 2.02 2.05 2.08 2.11	61 62 63 64 65 66 67 68 69 70
71 72 73 74 75 76 77 78 80	70·99 71·99 72·99 73·99 74·99 75·99 76·99 77·99 78·99 79·99	$\begin{array}{c} 1 \cdot 24 \\ 1 \cdot 26 \\ 1 \cdot 27 \\ 1 \cdot 29 \\ 1 \cdot 31 \\ 1 \cdot 33 \\ 1 \cdot 34 \\ 1 \cdot 36 \\ 1 \cdot 38 \\ 1 \cdot 40 \end{array}$	70.98 71.98 72.98 73.98 74.98 75.98 76.98 77.98 78.98 79.98	1.55 1.57 1.59 1.61 1.64 1.66 1.68 1.70 1.72 1.75	70.98 71.98 72.97 73.97 74.97 75.97 76.97 77.97 78.97 79.97	1.86 1.88 1.91 1.94 1.96 1.99 2.02 2.04 2.07 2.09	70.97 71.97 72.97 73.97 74.97 75.96 76.96 77.96 78.96 79.96	2·17 2·20 2·23 2·26 2·29 2·32 2·35 2·38 2·41 2·44	71 72 73 74 75 76 77 78 79 80
81 82 83 84 85 86 87 88 89 90	80·99 81·99 82·99 83·99 84·99 85·99 86·99 87·99 88·99	1·41 1·43 1·45 1·47 1·48 1·50 1·52 1·54 1·55	80·98 81·98 82·98 83·98 84·96 85·98 86·98 87·98 88·98 89·98	1.77 1.79 1.81 1.83 1.85 1.88 1.90 1.92 1.94 1.96	80-97 81-97 82-97 83-97 84-97 85-97 86-97 87-97 88-97 89-97	2·12 2·15 2·17 2·20 2·23 2·25 2·28 2·30 2·33 2·36	80.96 81.96 82.96 83.96 84.96 85.96 86.96 87.96 88.96 89.96	2·47 2·50 2·53 2·57 2·60 2·63 2·66 2·60 2·72 2·75	81 82 83 84 85 86 87 88 89 90
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91 92 93 94 95 96 97 98 99 100	90·78 91·78 92·77 93·77 94·77 96·76 97·76 98·76 99·76	6·35 6·42 6·49 6·56 6·63 6·70 6·77 6·84 6·91 6·98	90·75 91·75 92·74 93·74 94·74 95·74 96·73 97·73 98·73 99·73	6·74 6·82 6·89 6·97 7·04 7·11 7·19 7·26 7·34 7·41	90·72 91·72 92·71 93·71 94·71 95·70 96·70 97·70 98·69 99·69	7·14 7·22 7·30 7·38 7·45 7·53 7·61 7·69 7·77 7·85	90·69 91·68 92·68 93·68 94·67 95·67 96·67 97·66 98·66 99·66	7.54 7.62 7.70 7.78 7.87 7.95 8.03 8.12 8.20 8.28	91 92 93 94 95 96 97 98 99 100
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(	3	2.99	0.26	2.99	0.27	2.99	0.29	2.98	0.30	$\bar{s}$
(	4.	3.98	0.35	3.98	0.37	3.98	0·38 0·48	3·98 4:97	0.40	4 /
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{	11	10.96	0.96	10.95	1·01 1·10	10.95	1.05	10.94	1.10	$\left.\begin{array}{c} 11 \\ 12 \end{array}\right\}$
(	$\frac{12}{13}$	11.95	1·05 1·13	11.95	1·10 1·19	11·94 12·94	1·15 1·25	11·94 12·93	1·20 1·30	$\begin{pmatrix} 12 \\ 13 \end{pmatrix}$
<b>(</b> -	14	12·95 13·95	1.22	12·95 13·94	1.28	13.94	1.34	13.93	1.40	14 2
(	15	14.94	1.31	14.94	1·28 1·37	14.93	1.44	14.92	1.50	15 /
5	16	15.94	1.39	15.93	1.46	15.93	1.53 1.63 1.73	15.92	1:60 1:70	16 }
5	17 18	16.94 17.93	1·48 1·57	16.93 17.92	1.56 1.65	16.92 17.92	1.73	16·91 17·91	1.70	18
5	19	18 93	1.66	18.92	1.74	18.91	1.82	18.90	1 90	19 (
>	20	19.92	1.74	19.92	1.83	19.91	1.92	19.90	2.00	20
ζ	21	20.92	1.83	20.91	1.92	20.90	2.01	20.89	2.10	21 2
5	$\frac{21}{22}$	21.92	1.92	21.91	2.01	21.90	2.11	21.89	2.20	22
ς	$\frac{23}{24}$	22.91	2·00 2·09	22·90 23·90	2·10 2·20 2·29	22·89 23·89	2·20 2·30	22·88 23·88	2·30 2·40	$\left.\begin{array}{c} \overline{23} \\ 24 \end{array}\right\}$
5	24 25	$23.91 \\ 24.90$	2.18	24.90	2.29	24.88	2.40	24.87	2.50	25
5	26	25.90	2.27	25.89	2.38	25.88	2.49	25.87	2:60	26 (
>	27 28	26.90	2.35	26.89	2·47 2·56	26.88	2·59 2·68	26.86 27.86	2.71	27 (
>	28	27·89 28·89	2·44 2·53	27·88 28·88	2.65	27·87 28·87	2.78	28.85	2·81 2·91	$\begin{array}{c c} 28 & \\ 29 & \\ \end{array}$
ζ	29 30	29.89	2.61	29.87	2.75	29.86	2.88	29.85	3.01	30
>	31	30.88	2.70	30.87	2.84	30.86	2·97 3·07	30.84	3.11	31
(	$\frac{32}{33}$	31·88 32·87	2·79 2·88	31·87 32·86	2·93 3·02	31·85 32·85	3:16	31·84 32·83	3·21 3·31	32 33
7	34	33.87	2.88	33.86	3.11	33.84	3.26	33.83	3.41	34
(	35	34.87	3.05 3.14	34.85	3.20	34.84	3.35	34.82	3.51	35
(	36	35.86	3.14	35.85	3.29	35.83	3.45	35.82	3.61	36
(	$\frac{37}{38}$	36·86 37·86	3·22 3·31	36·84 37·84	3·39 3·48	36·83 37·83	3·55 3·64	36·81 37·81	3·71 3·81	37 38
5	39	38.85	3.40	38.84	3.57	38.82	3.74	38.80	3.91	39
{	40	39.85	3.49	39.83	3.66	39.82	3.83	39.80	4.01	40 (
ζ	41	40.84	3.57	40.82	3.75	40.81	3.93	40.79	4.11	41
5	42	41.84	3.66	41.82	3.84	41.81	4.03	41.79	4.21	42
5	$\frac{43}{44}$	42·84 43·83	3·75 3·83	42·82 43·82	3·93 4·03	42·80 43·80	4·12 4·22	42·78 43·78	4·31 4·41	43 44
5	44	44.83	3.92	44.81	4 12	44.79	4.31	44.77	4.51	45
5	46	45.82	4.01	45.81	4.21	45.79	4.41	45.77	4.61	46
>	47	46.82	4·10 4·18	46.80	4.30	46.78	4.50	46.76	4.71	47
>	$\frac{48}{49}$	47·82 48·81	4·18 4.27	47:80 48:79	4·39 4·48	47·78 48·77	4·60 4·70	47·76 48·75	4·81 4·91	48 (
ζ	50	48.81	4.27	49.79	4.48	49.77	4.79	49.75	5.01	50
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nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
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61 62 63 64 65 65 66 67 68 69 70	60·77 61·76 62·76 63·76 64·75 65·75 66·75 67·74 68·74 69·73	5·32 5·40 5·49 5·58 5·67 5·75 5·84 5·93 6·01 6·10	60·74 61·74 62·74 63·73 64·73 65·72 66·72 67·71 68·71 69·71	5.58 5.67 5.76 5.86 5.95 6.04 6.13 6.22 6.31 6.41	60·72 61·71 62·71 63·71 64·70 65·70 66·69 67·69 68·68 69·68	5·85 5·94 6·04 6·13 6·23 6·33 6·42 6·52 6·61 6·71	60·69 61·69 62·68 63·68 64·67 65·67 66·66 67·66 68·65 69·65	6·11 6·21 6·31 6·41 6·51 6·61 6·71 6·81 6·91 7·01	61 62 63 64 65 66 67 68 69 70
71 72 73 74 75 76 77 78 80	70·73 71·73 72·72 73·72 74·71 75·71 76·71 77·70 78·70 79·70	6·19 6·28 6·36 6·45 6·54 6·62 6·71 6·80 6·89	70·70 71·70 72·69 73·69 74·69 75·68 76·68 77·67 78·67 79·66	6·50 6·59 6·68 6·77 6·86 6·95 7·05 7·14 7·23 7·32	70.67 71.67 72.66 73.66 74.65 75.65 76.65 77.64 78.64 79.63	6·81 6·90 7·00 7·09 7·19 7·28 7·38 7·48 7·57 7·67	70·64 71·64 72·63 73·63 74·62 75·62 76·61 77·61 78·60 79·60	7·11 7·21 7·31 7·41 7·51 7·61 7·71 7·81 7·91 8·02	71 72 73 74 75 76 77 78 79 80
81 82 83 84 85 86 87 88 89	80·69 81·69 82·68 83·68 84·68 85·67 86·67 87·67 88·66 89·66	7·06 7·15 7·23 7·32 7·41 7·50 7·58 7·67 7·76 7·84	80·66 81·66 82·65 83·65 84·64 85·64 86·64 87·63 88·63 88·63	7·41 7·50 7·59 7·69 7·78 7·87 7·96 8·05 8·14 8·24	80·63 81·62 82·62 83·61 84·61 85·60 86·60 87·59 88·59 89·59	7·76 7·86 7·96 8·05 8·15 8·24 8·34 8·53 8·63	80·59 81·59 82·58 83·58 84·57 85·57 86·56 87·56 88·55 89·55	8·12 8·22 8·32 8·42 8·52 8·62 8·72 8·82 9·02	81 82 83 84 85 86 87 88 89 90
91 92 93 94 95 96 97 98 99 100	90·65 91·65 92·65 93·64 94·64 95·63 96·63 97·63 98·62 99·62	7·93 8·02 8·11 8·19 8·28 8·37 8·45 8·54 8·63 8·72	90·62 91·61 92·61 93·61 94·60 95·60 96·59 97·59 98·59 99·58	8·33 8·42 8·51 8·60 8·69 8·78 8·88 8·97 9·06 9·15	90·58 91·58 92·57 93·57 94·56 95·56 96·55 97·55 98·54 99·54	8·72 8·82 8·91 9·01 9·11 9·20 9·30 9·49 9·58	90·54 91·54 92·53 93·53 94·52 95·52 96·51 97·51 98·50 99·50	9·12 9·22 9·32 9·42 9·52 9·62 9·72 9·82 9·92 10·02	91
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	1 2 3 4 5 6 7 8 9 10	0·99 1·99 2·98 3·98 4·97 5·97 6·96 7·96 8·95	0·10 0·21 0·31 0·41 0·52 0·63 0·73 0·84 0·94 1·05	0.99 1.99 2.98 3.98 4.97 5.96 6.96 7.95 8.95 9.94	0·11 -0·22 0·33 0·44 0·54 0·65 0·76 0·87 0·98 1·09	0.99 1.99 2.98 3.97 4.97 5.96 6.96 7.95 8.94 9.94	0·11 0·23 0·34 0·45 0·57 0·68 0·79 0·91 1·02 1·13	0.99 1.99 2.98 3.97 4.97 5.96 6.95 7.94 8.94 9.93	0·12 0·24 0·35 0·47 0·59 0·71 0·82 0·94 1·06 1·18	1 2 3 4 5 6 7 8 9
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· · · · · · · · · · · · · · · · · · ·	21 22 23 24 25 26 27 28 29 30	20·88 21·88 22·87 23·87 24·86 25·86 26·85 27·85 28·84 29·84	2·20 2·30 2·40 2·51 2·61 2·72 2·82 2·93 3·03 3·14	20·88 21·87 22·86 23·86 24·85 25·85 26·84 27·83 28·83 29·82	2·29 2·40 2·50 2·61 2·72 2·83 2·94 3·05 3·16 3·27	20·87 21·86 22·85 23·85 24·84 25·83 26·83 27·82 28·81 29·81	2·38 2·49 2·60 2·72 2·83 2·94 3·06 3·17 3·28 3·40	20·85 21·85 22·84 23·83 24·83 25·82 26·81 27·81 28·80 29·79	2:47 2:59 2:70 2:82 2:94 3:06 3:17 3:29 3:41 3:53	21 22 23 24 25 26 27 28 29 30 2
	31 32 33 34 35 36 37 38 39 40	30·83 31·82 32·82 33·81 34·81 35·80 36·80 37·79 38·79 39·78	3·24 3·34 3·45 3·55 3·66 3·76 3·87 4·08 4·18	30·82 31·81 32·80 33·80 34·79 35·79 36·78 37·77 38·77	3·37 3·48 3·59 3·70 3·81 3·92 4·03 4·14 4·25 4·35	30·80 31·79 32·79 33·78 34·78 35·77 36·76 37·76 38·75 39·74	3·51 3·62 3·74 3·85 3·96 4·08 4·19 4·30 4·41 4·53	30·79 31·78 32·77 33·76 34·76 35·75 36·75 37·74 38·73 39·72	3·64 3·76 3·88 4·00 4·11 4·23 4·35 4·47 4·58 4·70	31 32 33 34 35 36 37 38 39 40
	41 42 43 44 45 46 47 48 49 50	40·78 41·77 42·76 43·76 44·75 45·75 46·74 47·74 48·73 49·73	4·29 4·39 4·49 4·60 4·70 4·81 4·91 5·02 5·12 5·23	40·76 41·75 42·74 43·74 44·73 46·72 47·71 48·71 49·70	4 46 4 57 4 68 4 79 4 90 5 01 5 12 5 23 5 34 5 44	40·74 41·73 42·72 43·72 44·71 45·70 46·70 47·69 48·69 49·68	4·64 4·76 4·87 4·98 5·09 5·21 5·32 5·43 5·55 5·66	40·72 41·71 42·70 43.70 44·69 45·68 46·67 47·67 48·66 49·65	4·82 4·94 5·05 5·17 5·29 5·41 5·52 5·64 5·76 5·88	41 42 43 44 45 46 47 48 49 50
{	Distance.	Dep. 84	Deg.	Dep. 833/2	Lat.	Bep. 831/2	Lat.	Dep.	. 83 <sup>1</sup> / <sub>4</sub>	Distance.

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51 52 53 54 54 55 56 57 58 59 60	50·72 51·72 52·71 53·70 54·70 55·69 56·69 57·68 58·68 59·67	5·33 5·44 5·54 5·64 5·75 5·85 5·96 6·06 6·17 6·27	50·70 51·69 52·68 53·68 54·67 55·67 56·66 57·66 58·65 59·64	5·55 5·66 5·77 5·88 5·99 6·10 6·21 6·31 6·42 6·53	50·67 51·67 52·66 53·65 54·65 55·64 56·63 57·63 58·62 59·61	5·77 5·89 6·00 6·11 6·23 6·34 6·45 6·57 6·68 6·79	50.65 51.64 52.63 53.63 54.62 55.61 56.60 57.60 58.59 59.58	5·99 6·11 6·23 6·35 6·46 6·58 6·70 6·82 6·93 7·05	51 (52 (53 (54 (55 (55 (55 (55 (55 (55 (55 (55 (55
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71 72 73 74 75 76 77 78 79 80	70·61 71·61 72·60 73·59 74·59 76·58 76·58 77·57 78·57 79·56	7·42 7·53 7·63 7·74 7·84 7·94 8·05 8·15 8·26 8·36	70·58 71·57 72·57 73·56 74·55 75·55 76·54 77·54 78·53 79·53	7·73 7·84 7·95 8·06 8·17 8·27 8·38 8·49 8·60 8·71	70·54 71·54 72·53 73·52 74·52 75·51 76·51 77·50 78·49 79·49	8·04 8·15 8·26 8·38 8·49 8·60 8·72 8·83 8·94 9·06	70·51 71·50 72·49 73·49 74·48 75·47 76·47 77·46 78·45 79·45	8·35 8·46 8·58 8·70 8·82 8·93 9·05 9·17 9·29 9·40	71 72 73 74 75 76 77 78 79 80
81 82 83 84 85 86 87 88 89 90	80·56 81·55 82·55 83·54 84·53 85·53 86·52 87·52 88·51 89·51	8·47 8·57 8·68 8·78 8·88 8·99 9·09 9·20 9·30 9·41	80·52 81·51 82·51 83·50 84·50 85·49 86·48 87·48 88·47 89·47	8·82 8·93 9·04 9·14 9·25 9·36 9·47 9·58 9·69 9·80	80·48 81·47 82·47 83·46 84·45 85·45 86·44 87·43 88·43 89·42	9·17 9·28 9·40 9·51 9·62 9·74 9·85 9·96 10·08 10·19	80·44 81·43 82·42 83·42 84·41 85·40 86·40 87·39 88·38 89·38	9·52 9·64 9·76 9·87 9·99 10·11 10·23 10·34 10·46 10·58	81 82 83 84 85 86 87 88 89 90
91 92 93 94 95 96 97 98 99 100	90·50 91·50 92·49 93·49 94·48 95·47 96·47 97·46 98·46 99·45	9·51 9·62 9·72 9·83 9·93 10·03 10·14 10·24 10·35 10·45	90·46 91·45 92·45 93·44 94·44 95·43 96·42 97·42 98·41 99·41	9·91 10·02 10·12 10·23 10·34 10·45 10·56 10·67 10·78 10·89	90·42 91·41 92·40 93·40 94·39 95·38 96·38 97·37 98·36 99·36	10·30 10·41 10·53 10·64 10·75 10·87 10·98 11·09 11·21 11·32	90·37 91·36 92·36 93·35 94·34 95·33 96·33 97·32 98·31 99·31	10·70 10·81 10·93 11·05 11·17 11·28 11·40 11·52 11·64 11·75	91 92 93 94 95 96 97 98 99
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12	11.91	1·46	11.90	1·51	11·90	1 57	11·89	1·62	12
13	12.90	1·58	12.90	1·64	12·89	1 70	12·88	1·75	13
14	13.90	1·71	13.89	1·77	13·88	1 83	13·87	1·89	14
15	14.89	1·83	14.88	1·89	14·87	1 96	14·86	2·02	15
16	15.88	1·95	15.87	2·02	15·86	2 09	15·85	2·16	16
17	16.87	2·07	16.86	2·15	16·85	2 22	16·84	2·29	17
18	17.87	2·19	17.86	2·27	17·85	2 35	17·84	2·43	18
19	18.86	2·32	18.85	2·40	18·84	2 48	18·83	2·56	19
20	19.85	2·44	19.84	2·52	19·83	2 61	19·82	2·70	20
21	20·84	2:56	20·83	2·65	20·82	2·74	20·81	2·83	21
22	21·84	2:68	21·82	2·78	21·81	2·87	21·80	2·97	22
23	22·83	2:80	22·82	2·90	22·80	3·00	22·79	3·10	23
24	23·82	2:92	23·81	3·03	23·79	3·13	23·78	3·24	24
25	24·81	3:05	24·80	3·15	24·79	3·26	24·77	3·37	25
26	25·81	3:17	25·79	3·28	25·78	3·39	25·76	3·51	26
27	26·80	3:29	26·78	3·41	26·77	3·52	26·75	3·64	27
28	27·79	3:41	27·78	3·53	27·76	3·65	27·74	3·78	28
29	28·78	3:53	28·77	3·66	28·75	3·79	28·74	3·91	29
30	29·78	3:66	29·76	3·79	29·74	3·92	29·73	4·05	30
31	30·77	3·78	30·75	3·91	30·73	4·05	30·72	4·18	31
32	31·76	3·90	31·74	4·04	31·73	4·18	31·71	4·32	32
33	32·75	4·02	32·74	4·16	32·72	4·31	32·70	4·45	33
34	33·75	4·14	33·73	4·29	33·71	4·44	33·69	4·58	34
35	34·74	4·27	34·72	4·42	34·70	4·57	34·68	4·72	35
36	35·73	4·39	35·71	4·54	35·69	4·70	35·67	4·85	36
37	36·72	4·51	36·70	4·67	36·68	4·83	36·66	4·99	37
38	37·72	4·63	37·70	4·80	37·67	4·96	37·65	5·12	38
39	38·71	4·75	38·69	4·92	38·67	5·09	38·64	5·26	39
40	39·70	4·87	39·68	5·05	39·66	5·22	39·63	5·39	40
41	40·70	5·00	40·67	5·17	40·65	5·35	40·63	5·53	41
42	41·69	5·12	41·66	5·30	41·64	5·48	41·62	5·66	42
43	42·68	5·24	42·66	5·43	42·63	5·61	42·61	5·80	43
44	43·67	5·36	43·65	5·55	43·62	5·74	43·60	5·93	44
45	44·67	5·48	44·64	5·68	44·62	5·87	44·59	6·07	45
46	45·66	5·61	45·63	5·81	45·61	6·00	45·58	6·20	46
47	46·65	5·73	46·62	5·93	46·60	6·13	46·57	6·34	47
48	47·64	5·85	47·62	6·06	47·59	6·27	47·56	6·47	48
49	48·63	5·97	48·61	6·18	48·58	6·40	48·55	6·61	49
50	49·63	6·09	49·60	6·31	49·57	6·53	49·54	6·74	50
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•	61 62 63 64 65 66 67 68 69 70	60·55 61·54 62·53 63·52 64·52 65·51 66·50 67·49 68·49 69·48	7·43 7·56 7·68 7·80 7·92 8·04 8·17 8·29 8·41 8·53	60·51 61·50 62·50 63·49 64·48 65·47 66·46 67·46 68·45 69·44	7·70 7·82 7·95 8·08 8·20 8·33 8·46 8·58 8·71 8·83	60·48 61·47 62·46 63·45 64·44 65·44 66·43 67·42 68·41 69·40	7.96 8.09 8.22 8.35 8.48 8.61 8.75 8.88 9.01 9.14	60·44 61·43 62·42 63·42 64·41 65·40 66·39 67·38 68·37 69·36	8·23 8·36 8·50 8·63 8·77 8·90 9·04 9·17 9·30 9·44	61 62 63 64 65 66 67 68 69 70
	71 72 73 74 75 76 77 78 79	70·47 71·46 72·46 73·45 74·44 75·43 76·43 77·42 78·41 79·40	8.65 8.77 8.90 9.02 9.14 9.26 9.38 9.51 9.63 9.75	70·43 71·42 72·42 73·41 74·40 75·39 76·38 77·38 78·37 79·36	8.96 9.09 9.21 9.34 9.46 9.59 9.72 9.84 9.97	70·39 71·38 72·38 73·37 74·36 75·35 76·34 77·33 78·32 79·32	9·27 9·40 9·53 9·66 9·79 9·92 10·05 10·18 10·31 10·44	70·35 71·34 72·33 73·32 74·31 75·31 76·30 77·29 78·28 79·27	9·57 9·71 9·84 9·98 10·11 10·25 10·38 10·52 10·65 10·79	71 72 78 74 75 76 77 78 79 80
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	91 92 93 94 95 96 97 98 99	90·32 91·31 92·31 93·30 94·29 95·28 96·28 97·27 98·26 99·25	11·09 11·21 11·33 11·46 11·58 11·70 11·82 11·94 12·07 12·19	90·27 91·26 92·26 93·25 94·24 95·23 96·22 97·22 98·21 99·20	11·48 11·61 11·74 11·86 11·99 12·12 12·24 12·24 12·49 12·62	90·22 91·21 92·20 93·20 94·19 95·18 96·17 97·16 98·15 99·14	11·88 12·01 12·14 12·27 12·40 12·53 12·66 12·79 12·92 13·05	90·17 91·16 92·15 93·14 94·13 95·12 96·11 97·10 98·10 99.09	12·27 12·41 12·54 12·68 12·81 12·95 13·08 13·22 13·35 13·49	91. 92 93 94 95 96 97 98 99 100
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11	10·89	1.53	10·89	1.58	10·88	1·63	10·87	1.67	11 12 13 14 15 16 17 18 19 20
12	11·88	1.67	11·88	1.72	11·87	1·77	11·86	1.83	
13	12·87	1.81	12·87	1.87	12·86	1·92	12·85	1.98	
14	13·86	1.95	13·86	2.01	13·85	2·07	13·84	2.13	
15	14·85	2.09	14·85	2.15	14·84	2·22	14·83	2.28	
16	15·84	2.23	15·84	2.30	15·82	2·36	15·81	2.43	
17	16·83	2.37	16·83	2.44	16·81	2·51	16·80	2.59	
18	17·82	2.51	17·81	2.58	17·80	2·66	17·79	2.74	
19	18·82	2.64	18·80	2.73	18·79	2·81	18·78	2.89	
20	19·81	2.78	19·79	2.87	19·78	2·96	19·77	3.04	
21	20·80	2·92	20·78	3·01	20·77	3·10	20·76	3·19	21
22	21·79	3·06	21·77	3·16	21·76	3·25	21·74	3·35	22
23	22·78	3·20	22·76	3·30	22·75	3·40	22·73	3·50	23
24	23·77	3·34	23·75	3·44	23·74	3·55	28·72	3·65	24
25	24·76	3·48	24·74	3·59	24·73	3·70	24·71	3·80	25
26	25·75	3·62	25·73	3·73	25·71	3·84	25·70	3·96	26
27	26·74	3·76	26·72	3·87	26·70	3·99	26·69	4·11	27
28	27·73	3·90	27·71	4·02	27·69	4·14	27·67	4·26	28
29	28·72	4·04	28·70	4·16	28·68	4·29	28·66	4·41	29
30	29·71	4·18	29·69	4·30	29·67	4·43	29·65	4·56	30
31	30·70	4·31	30·68	4·45	30·66	4·58	30·64	4·72	31
32	31·69	4·45	31·67	4·59	31·65	4·73	31·63	4·87	32
33	32·68	4·59	32·66	4·74	32·64	4·88	32·62	5·02	33
34	33·67	4·73	33·65	4·88	33·63	5·03	33·60	5·17	34
35	34·66	4·87	34·64	5·02	34·62	5·17	34·59	5·32	35
36	35·65	5·01	35·63	5·17	35·60	5·32	35·58	5·48	36
37	36·64	5·15	36·62	5·31	36·59	5·47	36·57	5·63	37
38	37·63	5·29	37·61	5·45	37·58	5·62	37·56	5·78	38
39	38·62	5·43	38·60	5·60	38·57	5·76	38·55	5·93	39
40	39·61	5·57	39·59	5·74	39·56	5·91	39·53	6·08	40
41	40·60	5·71	40·58	5·88	40·55	6·06	40·52	6·24	41 42 43 44 45 46 47 48 49 49 50
42	41·59	5·85	41·57	6·03	41·54	6·21	41·51	6·39	
43	42·58	5·98	42·56	6·17	42·53	6·36	42·50	6·54	
44	43·57	6·12	43·54	6·31	43·52	6·50	43·49	6·69	
45	44·56	6·26	44·53	6·46	44·51	6·65	44·48	6·85	
46	45·55	6·40	45·52	6·60	45·49	6·80	45·46	7·00	
47	46·54	6·54	46·51	6·74	46·48	6·95	46·45	7·15	
48	47·53	6·68	47·50	6·89	47·47	7·09	47·44	7·30	
49	48·52	6·82	48·49	7·03	48·46	7·24	48·43	7·45	
50	49·51	6·96	49·48	7·17	49·45	7·39	49·42	7·61	
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Distance	9 D	eg.	91/4	Deg.	9½	Deg.	934	Deg.	} Distance.
unce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nec.
51	50·87	7.98	50·34	8·20	50·30	8·42	50·26	8 64	51
52	51·36	8.13	51·32	8·36	51·29	8·58	51·25	8 81	52
53	52·35	8.29	52·31	8·52	52·27	8·75	52·23	8 98	53
54	53·34	8.45	53·30	8·68	53·26	8·91	53·22	9 14	54
55	54·32	8.60	54·28	8·84	54·25	9·08	54·21	9 31	55
56	55·31	8.76	55·27	9·00	55·23	9·24	55·19	9 48	56
57	56·30	8.92	56·26	9·16	56·22	9·41	56·18	9 65	57
58	57·29	9.07	57·25	9·32	57·20	9·57	57·16	9 82	58
59	58·27	9.23	58·23	9·48	58·19	9·74	58·15	9 99	59
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72	71·11	11·26	71·06	11·57	71·01	11·88	70·96	12·19	
73	72·10	11·42	72·05	11·73	72·00	12·05	71·95	12·36	
74	73·09	11·58	73·04	11·89	72·99	12·21	72·93	12·53	
75	74·08	11·73	74·02	12·06	73·97	12·38	73·92	12·70	
76	75·06	11·89	75·01	12·22	74·96	12·54	74·90	12·87	
77	76·05	12·05	76·00	12·38	75·94	12·71	75·89	13·04	
78	77·04	12·20	76·99	12·54	76·93	12·87	76·87	13·21	
79	78·03	12·36	77·97	12·70	77·92	13·04	77·86	13·38	
80	79·02	12·51	78·96	12·86	78·90	13·20	78·84	13·55	
81	80·00	12·67	79·95	13·02	79·89	13·37	79·83	13·72	81 82 83 84 85 86 87 88 89 90 90
82	80·99	12·83	80·93	13·18	80·88	13·53	80·82	13·89	
83	81·98	12·98	81·92	13·34	81·86	13·70	81·80	14·06	
84	82·97	13·14	82·91	13·50	82·85	13·86	82·79	14·23	
85	83·95	13·30	83·89	13·66	83·83	14·03	83·77	14·39	
86	84·94	13·45	84·88	13·82	84·82	14·19	84·76	14·56	
87	85·93	13·61	85·87	13·98	85·81	14·36	85·74	14·73	
88	86·92	13·77	86·86	14·15	86·79	14·52	86·73	14·90	
89	87·90	13·92	87·84	14·31	87·78	14·69	87·71	15·07	
90	88·89	14·08	88·83	14·47	88·77	14·85	88·70	15·24	
91	89.88	14·24	\$9.82	14·63	89·75	15·02	89·69	15·41	91
92	90.87	14·39	90.80	14·79	90·74	15·18	90·67	15·58	92
93	91.86	14·55	91.79	14·95	91·72	15·35	91·66	15·75	93
94	92.84	14·70	92.78	15·11	92·71	15·51	92·64	15·92	94
95	93.83	14·86	93.76	15·27	93·70	15·68	93·63	16·09	95
96	94.82	15·02	94.75	15·43	94·68	15·84	94·61	16·26	96
97	95.81	15·17	95.74	15·59	95·67	16·01	95·60	16·43	97
98	96.79	15·33	96.73	15·75	96·66	16·17	96·58	16·60	98
99	97.78	15·49	97.71	15·91	97·64	16·34	97·57	16·77	99
100	98.77	15·64	98.70	16·07	98·63	16·50	98·56	16·93	100
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21 22 22 23 24 25 26 27 28 29 30	20·68 21·67 22·65 23·64 24·62 25·61 26·59 27·57 28·56 29·54	3·65 3·82 3·99 4·17 4·34 4·51 4·69 4·86 5·04 5·21	20·66 21·65 22·63 23·62 24·60 25·59 26·57 27·55 28·54 29·52	3·74 3·91 4·09 4·27 4·45 4·63 4·80 4·98 5·16 5·34	20·65 21·63 22·61 23·60 24·58 25·56 26·55 27·53 28·51 29·50	3·83 4·01 4·19 4·37 4·56 4·74 4·92 5·10 5·28 5·47	20·63 21·61 22·60 23·58 24·56 25·54 26·53 27·51 28·49 29·47	3·92 4·10 4·29 4·48 4·66 4·85 5·04 5·22 5·41 5·60	21 22 23 24 25 26 27 28 29 30
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ince.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nuce.
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Distance	11 1	Deg.	111/4	Deg.	11½	Deg.	113/4	Deg.	} Distance
) nee.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
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52	51·04	9·92	51·00	10·14	50·96	10·37	50·91	10·59	
53	52·03	10·11	51·98	10·34	51·94	10·57	51·89	10·79	
54	53·01	10·30	52·96	10·53	52·92	10·57	52·87	11·00	
55	53·99	10·49	53·94	10·73	53·90	10·97	53·85	11·20	
56	54·97	10·69	54·92	10·93	54·88	11·16	54·83	11·40	
57	55·95	10·88	55·90	11·12	55·86	11·36	55·81	11·61	
58	56·93	11·07	56·89	11.32	56·84	11·56	56·78	11·81	
59	57·92	11·26	57·87	11·51	57·82	11·76	57·76	12·01	
60	58·90	11·45	58·85	11·71	58·80	11·96	58·74	12·22	
61	59·88	11.64	59·83	11·90	59·78	12·16	59·72	12·42	61
62	60·86	11.83	60·81	12·10	60·76	12·36	60·70	12·63	62
63	61·84	12.02	61·79	12·29	61·74	12·56	61·68	12·83	63
64	62·82	12.21	62·77	12·49	62·72	12·76	62·66	13·03	64
65	63·81	12.40	63·75	12·68	63·70	12·96	63·64	13·24	65
66	64·79	12.59	64·73	12·88	64·68	13·16	64·62	13·44	66
67	65·77	12.78	65·71	13·07	65·66	13·36	65·60	13·64	67
68	66·75	12.98	66·69	13·27	66·63	13·56	66·58	13·85	68
69	67·73	13.17	67·67	13·46	67·61	13·76	67·55	14·05	69
70	68·71	13.36	68·66	13·66	68·59	13·96	68·53	14·25	70
71	69·70	13·55	69:64	13·85	69·57	14·16	69·51	14·46	71
72	70·68	13·74	70:62	14·05	70·55	14·35	70·49	14·66	
73	71·66	13·93	71:60	14·24	71·53	14·55	71·47	14·87	
74	72·64	14·12	72:58	14·44	72·51	14·75	72·45	15·07	
75	73·62	14·31	73:56	14·63	73·49	14·95	73·43	15·27	
76	74·60	14·50	74:54	14·83	74·47	15·15	74·41	15·48	
77	75·59	14·69	75:52	15·02	75·45	15·35	75·39	15·68	
78	76·57	14·88	76:50	15·22	76·43	15·55	76·37	15·88	
79	77·55	15·07	77:48	15·41	77·41	15·75	77·34	16·09	
80	78·53	15·26	78:46	15·61	78·39	15·95	78·32	16·29	
81	79·51	15·46	79·44	15·80	79·37	16·15	79·30	16·49	81
82	80·49	15·65	80·42	16·00	80·35	16·35	80·28	16·70	82
83	81·48	15·84	81·41	16·19	81·33	16·55	81·26	16·90	83
84	82·46	16·03	82·39	16·39	82·31	16·75	82·24	17·11	84
85	83·44	16·22	83·37	16·58	83·29	16·95	83·22	17·31	85
86	84·42	16·41	84·35	16·78	84·27	17·15	84·20	17·51	86
87	85·40	16·60	85·33	16·97	85·25	17·35	85·18	17·72	87
88	86·38	16·79	86·31	17·17	86·23	17·54	86·16	17·92	88
89	87·36	16·98	87·29	17·36	87;21	17·74	87·14	18·12	89
90	88·35	17·17	88·27	17·56	88·19	17·94	88·11	18·33	90
91 92 93 94 95 96 97 98 99 100	89·33 90·31 91·29 92·27 93·25 94·24 95·22 96·20 97·18 98·16	17·36 17·55 17·75 17·94 18·13 18·32 18·51 18·70 18·89 19·08	89·25 90·23 91·21 92·19 93·17 94·16 95·14 96·12 97·10 98·08	17·75 17·95 18·14 18·34 18·53 18·73 18·92 19·12 19·31 19·51	89·17 90·15 91·13 92·11 93·09 94·07 95·05 96·03 97·01 97·99	18·14 18·34 18·54 18·74 18·94 19·14 19·54 19·74 19·94	89·09 90·07 91·05 92·03 93·01 93·99 94·97 95·95 96·93 97·90	18·53 18·74 18·94 19·14 19·35 19·55 19·75 19·96 20·16 20·36	91 (92 (93 (94 (95 (97 (98 (99 (99 (99 (99 (99 (99 (99 (99 (99
Distance.	Dep. 79	Lat.	Dep.	Lat.	Dep.	Lat.	Dep. 781/2	Lat.	Distance.

) Dista	District 12 Deg.	oeg.	121/4	Deg.	121/2	Deg.	123/4	Deg.	$\left. \left. \left\langle \right\rangle \right\rangle \right\rangle $ Distance
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	rce.
1 2 3 4 5 6 7 8 9	0.98 1.96 2.93 3.91 4.89 5.87 6.85 7.83 8.80 9.78	0·21 0·42 0·62 0·83 1·04 1·25 1·46 1·66 1·87 2·08	0.98 1.95 2.93 3.91 4.89 5.86 6.84 7.82 8.80 9.77	0·21 0·42 0·64 0·85 1·06 1·27 1·49 1·70 1·91 2·12	0.98 1.95 2.93 3.91 4.88 5.86 6.83 7.81 8.79 9.76	0·22 0·43 0·65 0·87 1·08 1·30 1·52 1·73 1·95 2·16	0.98 1.95 2.93 3.90 4.88 5.85 6.83 7.80 8.78 9.75	0·22 0·44 0·66 0·88 1·10 1·32 1·54 1·77 1·99 2·21	1 2 3 4 5 6 7 8 9 10
11 12 13 14 15 16 17 18 19 20	10·76 11·74 12·72 13·69 14·67 15·65 16·63 17·61 18·58 19·56	2·29 2·49 2·70 2·91 3·12 3·33 3·53 3·74 3·95 4·16	10·75 11·73 12·70 13·68 14·66 15·64 16·61 17·59 18·57 19·54	2·33 2·55 2·76 2·97 3·18 3·39 3·61 3·82 4·03 4·24	10·74 11·72 12·69 13·67 14·64 15·62 16·60 17·57 18·55 19·53	2·38 2·60 2·81 3·03 3·25 3·46 3·68 3·90 4·11 4·33	10·73 11·70 12·68 13·65 14·63 15·61 16·58 17·56 18·53 19·51	2·43 2·65 2·87 3·09 3·31 3·53 3·75 3·97 4·19 4·41	11 12 13 14 15 16 17 18 19
21 22 23 24 25 26 27 28 29 30	20·54 21·52 22·50 23·48 24·45 25·43 26·41 27·39 28·37 29·34	4·37 4·57 4·78 4·99 5·20 5·41 5·61 5·82 6·03 6·24	20·52 21·50 22·48 23·45 24·43 25·41 26·39 27·36 28·34 29·32	4·46 4·67 4·88 5·09 5·30 5·52 5·73 5·94 6·15 6·37	20·50 21·48 22·45 23·43 24·41 25·38 26·36 27·34 28·31 29·29	4·55 4·76 4·98 5·19 5·41 5·63 5·84 6·06 6·28 6·49	20·48 21·46 22·43 23·41 24·38 25·36 26·33 27·31 28·28 29·26	4·63 4·86 5·08 5·30 5·52 5·74 5·96 6·18 6·40 6·62	21 (22 (23 (24 (25 (26 (27 (28 (29 (29 (29 (29 (29 (29 (29 (29 (29 (29
31 32 33 34 35 36 37 38 39 40	30·32 31·30 32·28 33·26 34·24 35·21 36·19 37·17 38·15 39·13	6.45 6.65 6.86 7.07 7.28 7.48 7.69 7.90 8.11 8.32	30·29 31·27 32·25 33·23 34·20 35·18 36·16 37·13 38·11 39·09	6·58 6·79 7·00 7·21 7·43 7·64 7·85 8·06 8·27 8·49	30·27 31·24 32·22 33·19 34·17 35·15 36·12 37·10 38·08 39·05	6·71 6·93 7·14 7·36 7·58 7·79 8·01 8·22 8·44 8·66	30·24 31·21 32·19 33·16 34·14 35·11 36·09 37·06 38·04 39·01	6·84 7·06 7·28 7·50 7·72 7·95 8·17 8·39 8·61 8·83	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	40·10 41·08 42·06 43·04 44·02 44·99 45·97 46·95 47·93 48·91	8·52 8·73 8·94 9·15 9·36 9·56 9·77 9·98 10·19 10·40	40·07 41·04 42·02 43·00 43·98 44·95 45·93 46·91 47·88 48·86	8·70 8·91 9·12 9·34 9·55 9·76 9·97 10·18 10·40 10·61	40·03 41·00 41·98 42·96 43·93 44·91 45·89 46·86 47·84 48·81	8·87 9·09 9·31 9·52 9·74 9·96 10·17 10·39 10·61 10·82	39·99 40·96 41·94 42·92 43.89 44·87 45·84 46·82 47·79 48·77	9·05 9·27 9·49 9·71 9·93 10·15 10·37 10·59 10·81 11·03	41 42 43 44 45 46 47 48 49 50
Distance.	Dep. 78	Lat.	Dep.	Lat.	Dep. 771	Lat.	Dep. 771/2	Lat.	Distance.

Distance.	12 1	Deg.	121/4	Deg.	121/2	Deg.	123/4	Deg.	$\left. \left. \left\langle \right\rangle \right\rangle \right. \left. \left\langle \right\rangle \right$
псе.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nec.
51	49·89	10·60	49·84	10·82	49·79	11·04	49·74	11·26	51
52	50·86	10·81	50·82	11·03	50·77	11·25	50·72	11·48	52
53	51·84	11·02	51·79	11·25	51·74	11·47	51·69	11·70	53
54	52·82	11·23	52·77	11·46	52·72	11·69	52·67	11·92	54
55	53·80	11·44	53·75	11·67	53·70	11·90	53·64	12·14	55
56	54·78	11·64	54·72	11·88	54·67	12·12	54·62	12·36	56
57	55·75	11·85	55·70	12·09	55·65	12·34	55·59	12·58	57
58	56·73	12·06	56·68	12·31	56·63	12·55	56·57	12·80	58
59	57·71	12·27	57·66	12·52	57·60	12·77	57·55	13·02	59
60	58·69	12·47	58·63	12·73	58·58	12·99	58·52	13·24	60
61	59·67	12·68	59·61	12.94	59·55	13·20	59·50	13·46	61
62	60·65	12·89	60·59	13.16	60·53	13·42	60·47	13·68	62
63	61·62	13·10	61·57	13.37	61·51	13·64	61·45	13·90	63
64	62·60	13·31	62·54	13.58	62·48	13·85	62·42	14·12	64
65	63·58	13·51	63·52	13.79	63·46	14·07	63·40	14·35	65
66	64·56	13·72	64·50	14.00	64·44	14·29	64·37	14·57	66
67	65·54	13·93	65·47	14.22	65·41	14·50	65·35	14·79	67
68	66·51	14·14	66·45	14.43	66·39	14·72	66·32	15·01	68
69	67·49	14·35	67·43	14.64	67·36	14·93	67·30	15·23	69
70	68·47	14·55	68·41	14.85	68·34	15·15	68·27	15·45	70
71	69·45	14·76	69.38	15·06	69·32	15·37	69·25	15·67	71
72	70·43	14·97	70·36	15·28	70·29	15·58	70·22	15·89	72
73	71·40	15·18	71·34	15·49	71·27	15·80	71·20	16·11	73
74	72·38	15·39	72·32	15·70	72·25	16·02	72·18	16·33	74
75	73·36	15·59	73·29	15·91	73·22	16·23	73·15	16·55	75
76	74·34	15·80	74·27	16·13	74·20	16·45	74·13	16·77	76
77	75·32	16·01	75·25	16·34	75·17	16·67	75·10	16·99	77
78	76·30	16·22	76·22	16·55	76·15	16·88	76·08	17·21	78
79	77·27	16·43	77·20	16·76	77·13	17·10	77·05	17·44	79
80	78·25	16·68	78·18	16·97	78·10	17·32	78·03	17·66	80
81	79·23	16·84	79·16	17:19	79·08	17-53	79·00	17.88	81
82	80·21	17·05	80·13	17:40	80·06	17-75	79·98	18.10	82
83	81·19	17·26	81·11	17:61	91·03	17-96	80·95	18.32	83
84	82·16	17·46	82·09	17:82	82·01	18-18	81·93	18.54	84
85	83·14	17·67	83·06	18:04	82·99	18-40	82·90	18.76	85
86	84·12	17·88	84·04	18:25	83·96	18-61	83·88	18.98	86
87	85·10	18·09	85·02	18:46	84·94	18-83	84·85	19.20	87
88	86·08	18·30	86·00	18:67	85·91	19-05	85·83	19.42	88
89	87·06	18·50	86·97	18:88	86·89	19-26	86·81	19.64	89
90	88·03	18·71	87·95	19:10	87·87	19-48	87·78	19.86	90
91	89·01	18·92	88.93	19·31	88·84	19·70	88·76	20·08	91 (92 (93 (94 (95 (95 (95 (95 (95 (95 (95 (95 (95 (95
92	89·99	19·13	89.91	19·52	89·82	19·91	89·73	20·30	
93	90·97	19·54	90.88	19·73	90·80	20·13	90·71	20·52	
94	91·95	19·54	91.86	19·94	91·77	20·35	91·68	20·75	
95	92·92	19·75	92.84	20·16	92·75	20·56	92·66	20·97	
96	93·90	19·96	93.81	20·37	93·72	20·78	93·63	21·19	
97	94·88	20·17	94.79	20·58	94·70	20·99	94·61	21·41	
98	95·86	20·38	95.77	20·79	95·68	21·21	95·58	21·63	
99	96·84	20·58	96.75	21·01	96·65	21·43	96·56	21·85	
100	97·81	20·79	97.72	21·22	97·63	21·64	97·53	22·07	
Distance.	78	Deg.	773/2	Lat.	77½	Lat.	771/2	Lat.	Distance.

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}	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
	1 2 3 4 5 6 7 8 9	0.97 1.95 2.92 3.90 4.87 5.85 6.82 7.80 8.77 9.74	0·23 0·45 0·67 0·90 1·12 1·35 1·57 1·80 2·02 2·25	0.97 1.95 2.92 3.89 4.87 5.84 6.81 7.79 8.76 9.73	0·23 0·46 0·69 0·92 1·15 1·38 1·60 1·83 2·06 2·29	0.97 1.95 2.92 3.89 4.86 5.83 6.81 7.78 8.75 9.72	0·23 0·47 0·70 0·93 1·17 1·40 1·63 1·87 2·10 2·33	0.97 1.94 2.91 3.89 4.86 5.83 6.80 7.77 8.74 9.71	0·24 0·48 0·71 0·95 1·19 1·43 1·66 1·90 2·14 2·38	1 2 3 4 5 6 7 8 9 10 4
}	11 12 13 14 15 16 17 18 19 20	10·72 11·69 12·67 13·64 14·62 15·59 16·57 17·54 18·51 19·49	2·47 2·70 2·92 3·15 3·37 3·60 3·82 4·05 4·27 4·50	10·71 11·68 12·65 13·63 14·60 15·57 16·55 17·52 18·49 19·47	2·52 2·75 2·98 3·21 3·44 3·67 3·90 4·13 4·35 4·58	10·70 11·67 12·64 13·61 14·59 15·56 16·53 17·50 18·48 19·45	2·57 2·80 3·03 3·27 3·50 3·74 3·97 4·20 4·44 4·67	10·68 11·66 12·63 13·60 14·57 15·54 16·51 17·48 18·46 19·43	2·61 2·85 3·09 3·33 3·57 3·80 4·04 4·28 4·52 4·75	11 \ 12 \ 13 \ 14 \ 15 \ 16 \ 17 \ 18 \ 19 \ 20 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
}	21 22 23 24 25 26 27 28 29 30	20·46 21·44 22·41 23·38 24·36 25·33 26·31 27·28 28·26 29·23	4·72 4·95 5·17 5·40 5·62 5·85 6·07 6·30 6·52 6·75	20·44 21·41 22·39 23·36 24·33 25·31 26·28 27·25 28·23 29·20	4·81 5·04 5·27 5·50 5·73 5·96 6·19 6·42 6·65 6·88	20·42 21·39 22·36 23·34 24·31 25·28 26·25 27·23 28·20 29·17	4·90 5·14 5·37 5·60 5·84 6·07 6·30 6·54 6·77 7·00	20·40 21·37 22·34 23·31 24·28 25·25 26·23 27·20 28·17 29·14	4·99 5·23 5·47 5·70 5·94 6·18 6·42 6·66 6·89 7·13	21 22 23 24 25 26 27 28 29 30 2
~~~~~~	31 32 33 34 35 36 37 38 39 40	30·21 31·18 32·15 33·13 34·10 35·08 36·05 37·03 38·00 38·97	6.97 7.20 7.42 7.65 7.87 8.10 8.32 8.55 8.77 9.00	30·17 31·15 32·12 33·09 34·07 35·04 36·02 36·99 37·96 38·94	7·11 7·33 7·56 7·79 8·02 8·25 8·48 8·71 8·94 9·17	30·14 31·12 32·09 33·06 34·03 35·01 35·98 36·95 37·92 38·89	7·24 7·47 7·70 7·94 8·17 8·40 8·64 8·87 9·10 9·34	30·11 31·08 32·05 33·03 34·00 34·97 35·94 36·91 37·88 38·85	7·37 7·61 7·84 8·08 8·32 8·56 8·79 9·03 9·27 9·51	31 32 33 34 35 36 37 38 39 40 3
}	41 42 43 44 45 46 47 48 49 50	39·95 40·92 41·90 42·87 43·85 44·82 45·80 46·77 47·74 48·72	9·22 9·45 9·67 9·90 10·12 10·35 10·57 10·80 11·02 11·25	39·91 40·88 41·86 42·83 43·80 44·78 46·75 46·72 47·70 48·67	9·40 9·63 9·86 10·08 10·31 10·54 10·77 11·00 11·23 11·46	39·87 40·84 41·81 42·78 43·76 41·73 45·70 46·67 47·65 48·62	9·57 9·80 10·04 10·27 10·51 10·74 10·97 11·21 11·44 11·67	39·83 40·80 41·77 42·74 43·71 44·68 45·65 46·62 47·60 48·57	9·75 9·98 10·22 10·46 10·70 10·93 11·17 11·41 11·65 11·88	41 42 43 44 45 46 47 48 49 50
	Distance.	77 I	Lat.	763/4	Lat. Deg.	Dep. 76½		76½	Deg.	Distance.

Distance	13	Deg.	131/4	Deg.	13½	Deg.	133/4	Deg.	Distance
{	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51 52 53 54 54 55 56 57 58 59 60	49.69 50·67 51·64 52·62 53·59 54·56 55·54 56·51 57·49 58·46	11·47 11·70 11·92 12·15 12·37 12·60 12·82 13·05 13·27 13·50	49·64 50·62 51·59 52·56 58·54 54·51 55·48 56·46 57·43 58·40	11·69 11·92 12·15 12·38 12·61 12·84 13·06 13·29 13·52 13·75	49·59 50·56 51·54 52·51 53·48 54·45 55·43 56·49 57·37 58·34	11.91 12.14 12.37 12.61 12.84 13.07 13.31 13.54 13.77 14.01	49·54 50·51 51·48 52·45 53·42 54·40 55·37 56·34 57·31 58·28	12·12 12·36 12·60 12·84 13·07 13·31 13·55 13·79 14·02 14·26	51 (52 (53 (54 (55 (55 (55 (55 (55 (55 (55 (55 (55
61 62 63 64 65 66 66 67 68 69 70	59.44 $60.41$ $61.39$ $62.36$ $63.33$ $64.31$ $65.28$ $66.26$ $67.23$ $68.21$	13·72 13·95 14·17 14·40 14·62 14·85 15·07 15·30 15·52 15·75	59·38 60·35 61·32 62·30 63·27 64·24 65·22 66·19 67·16 68·14	13.98 14.21 14.44 14.67 14.90 15.13 15.36 15.59 15.81 16.04	59·31 60·29 61·26 62·23 63·20 64·18 65·15 66·12 67·09 68·07	14·24 14·47 14·71 14·94 15·17 15·41 15·64 15·87 16·11 16·34	59·25 60·22 61·19 62·17 63·14 64·11 65·08 66·05 67·02 67·99	14·50 14·74 14·97 15·21 15·45 15·69 15·93 16·16 16·40 16·64	61 62 63 64 65 66 66 67 68 69 70 6
71 72 73 74 75 76 77 78 79 80	69·18 70·15 71·13 72·10 73·08 74·05 75·03 76·00 76·98 77·95	15·97 16·20 16·42 16·65 16·87 17·10 17·32 17·55 17·77 18·00	69·11 70·08 71·06 72·03 73·00 73·98 74·95 75·92 76·90 77·87	16·27 16·50 16·73 16·96 17·19 17·42 17·65 17·88 18·11 18·34	69·04 70·01 70·98 71·96 72·93 73·90 74·87 75·84 76·82 77·79	16·57 16·81 17·04 17·28 17·50 17·74 17·98 18·21 18·44 18·68	68.97 69.94 70.91 71.88 72.85 73.82 74.79 75.76 76.74 77.71	16·88 17·11 17·35 17·59 17·83 18·06 18·30 18·54 18·78 19·01	71 (72 (73 (74 (75 (77 (78 (79 (80 (79 (79 (79 (79 (79 (79 (79 (79 (79 (79
81 82 83 84 85 86 87 88 89 90	78.92 79.90 80.87 81.85 82.82 83.80 84.77 85.74 86.72 87.69	18·22 18·45 18·67 18·90 19·12 19·35 19·57 19·80 20·02 20·25	78·84 79·82 80·79 81·76 82·74 83·71 84·68 85·66 86·63 87·60	18·57 18·79 19·02 19·25 19·48 19·71 19·94 20·17 20·40 20·63	78·76 79·73 80·71 81·68 82·65 83·62 84·60 85·57 86·54 87·51	18·91 19·14 19·38 19·61 19·84 20·08 20·31 20·54 20·78 21·01	78·68 79·65 80·62 81·59 82·56 83·54 84·51 85·48 86·45 87·42	19·25 19·49 19·73 19·97 20·20 20·44 20·68 20·92 21·15 21·39	81 82 83 84 85 86 87 88 89 90 8
91 92 93 94 95 96 97 98 99 100	88·67 89·64 90·62 91·59 92·57 93·54 94·51 95·49 96·46 97·44	20·47 20·70 20·92 21·15 21·37 21·60 21·82 22·05 22·27 22·50	88·58 89·55 90·52 91·50 92·47 93·44 94·42 95·39 96·36 97·34	20·86 21·09 21·32 21·54 21·77 22·00 22·23 22·46 22·69 22·92	88·49 89·46 90·43 91·40 92·38 93·35 94·32 95·29 96·26 97·24	21·24 21·48 21·71 21·94 22·18 22·41 22·64 22·88 23·11 23·34	88·39 89·36 90·33 91·31 92·28 93·25 94·22 95·19 96·16 97·13	21.63 21.87 22.10 22.34 22.58 22.82 23.06 23.29 23.53 23.77	91 ( 92 ( 93 ( 94 ( 95 ( 96 ( 97 ( 98 ( 99 ( 100 (
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.

{	Distance	14 ]	Deg.	141/4	Deg.	141/2	Deg.	143/4	Deg.	Distance
3	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
	1 2 3 4 5 6 7 8 9	0.97 1.94 2.91 3.88 4.85 5.82 6.79 7.76 8.73 9.70	0·24 0·48 0·73 0·97 1·21 1·45 1·69 1·94 2·18 2·42	0.97 1.94 2.91 3.88 4.85 5.82 6.78 7.75 8.72 9.69	0·25 0·49 0·74 0·98 1·23 1·48 1·72 1·97 2·22 2·46	0·97 1·94 2·90 3·87 4·84 5·81 6·78 7·75 8·71 9·68	0·25 0·50 0·75 1·00 1·25 1·50 1·75 2·00 2·25 2·50	0.97 1.93 2.90 3.87 4.84 5.80 6.77 7.74 8.70 9.67	0·25 0·51 0·76 1·02 1·27 1·53 1·78 2·04 2·29 2·55	1 2 3 4 4 5 6 7 8 9 10 5
	11 12 13 14 15 16 17 18 19 20	10·67 11·64 12·61 13·58 14·55 15·52 16·50 17·47 18·44 19·41	2·66 2·90 3·15 3·39 3·63 3·87 4·11 4·35 4·60 4·84	10·66 11·63 12·60 13·57 14·54 15·51 16·48 17·45 18·42 19·38	2·71 2·95 3·20 3·45 3·69 3·94 4·18 4·43 4·68 4·92	10·65 11·62 12·59 13·55 14·52 15·49 16·46 17·43 18·39 19·36	$\begin{array}{c} 2 \cdot 75 \\ 3 \cdot 00 \\ 3 \cdot 25 \\ 3 \cdot 51 \\ 3 \cdot 76 \\ 4 \cdot 01 \\ 4 \cdot 26 \\ 4 \cdot 51 \\ 4 \cdot 76 \\ 5 \cdot 01 \end{array}$	10·64 11·60 12·57 13·54 14·51 15·47 16·44 17·41 18·37 19·34	2·80 3·06 3·31 3·56 3·82 4·07 4·33 4·58 4·84 5·09	11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ \}
· · · · · · · · · · · · · · · · · · ·	21 22 23 24 25 26 27 28 29 30	20·38 21·35 22·32 23·29 24·26 25·23 26·20 27·17 28·14 29·11	5.08 5.32 5.56 5.81 6.05 6.29 6.53 6.77 7.02 7.26	20·35 21·32 22·29 23·26 24·23 25·20 26·17 27·14 28·11 29·08	5·17 5·42 5·66 5·91 6·15 6·40 6·65 6·89 7·14 7·38	20·33 21·30 22·27 23·24 24·20 25·17 26·14 27·11 28·08 29·04	5·26 5·51 5·76 6·01 6·26 6·51 6·76 7·01 7·26 7·51	20·31 21·28 22·24 23·21 24·18 25·14 26·11 27·08 28·04 29·01	5·35 5·60 5·86 6·11 6·37 6·62 6·87 7·13 7·38	21. 22. 23. 24. 25. 26. 27. 28. 29. 30.
~~~~~	31 32 33 34 35 36 37 38 39 40	30·08 31·05 32·02 32·99 33·96 34·93 35·90 36·87 37·84 38·81	7·50 7·74 7·98 8·23 8·47 8·71 8·95 9·19 9·44 9·68	30·05 31·02 31·98 32·95 33·92 34·89 35·86 36·83 37·80 38·77	7·63 7·88 8·12 8·37 8·62 8·86 9·11 9·35 9·60 9·85	80·01 30·98 31·95 32·92 33·89 34·85 85·82 36·79 87·76 38·73	7.76 8.01 8.26 8.51 8.76 9.01 9.26 9.51 9.76 10.02	29·98 30·95 31·91 32·88 33·85 34·81 35·78 36·75 87·71 38·68	7·\$9 8·15 8·40 8·66 8·91 9·17 9·42 9·67 9·93 10·18	31 32 33 34 35 36 37 38 39 40
	41 42 43 44 45 46 47 48 49 50	39·78 40·75 41·72 42·69 43·66 44·63 45·60 46·57 47·54 48·51	9·92 10·16 10·40 10·64 10·89 11·13 11·37 11·61 11·85 12·10	39·74 40·71 41·68 42·65 43·62 44·58 45·55 46·52 47·49 48·46	10·09 10·34 10·58 10·83 11·08 11·32 11·57 11·82 12·06 12·31	39·69 40·66 41·63 42·60 43·57 44·53 45·50 46·47 47·44 48·41	10·27 10·52 10·77 11·02 11·27 11·52 11·77 12·02 12·27 12·52	39·65 40·62 41·58 42·55 43·52 44·48 45·45 46·42 47·39 48·35	10·44 10·69 10·95 11·20 11·46 11·71 11·97 12·22 12·48 12·73	41 42 43 44 45 46 47 48 49 50
\{\}	Distance.	Dep. 76	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.

Distance.	14 3	Deg.	141/4	Deg.	$14\frac{1}{2}$	Deg.	143/4	Deg.	Distance.
e.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	1ce.
51	49·49	12·34	49·43	12·55	49·38	12·77	49·32	12·98	51
52	50·46	12·58	50·40	12·80	50·34	13·02	50·29	13·24	52
53	51·43	12·82	51·37	13·05	51·31	13·27	51·25	13·49	53
54	52·40	13·06	52·34	13·29	52·28	13·52	52·22	13·75	54
55	53·37	13·31	53·31	13·54	53·25	13·77	53·19	14·00	55
56	54·34	13·55	54·28	13·78	54·22	14·02	54·15	14·26	56
57	55·31	13·79	55·25	14·03	55·18	14·27	55·12	14·51	57
58	56·28	14·03	56·22	14·28	56·15	14·52	56·09	14·77	58
59	57·25	14·27	57·18	14·52	57·12	14·77	57·06	15·02	59
60	58·22	14·52	58·15	14·77	58·09	15·02	58·02	15·28	60
61	59·19	14·76	59·12	15·02	59·06	15·27	58-99	15·53	61 62 63 64 65 66 67 68 69 70
62	60·16	15·00	60·09	15·26	60·03	15·52	59-96	15·79	
63	61·13	15·24	61·06	15·51	60·99	15·77	60-92	16·04	
64	62·10	15·48	62·03	15·75	61·96	16·02	61-89	16·29	
65	63·07	15·72	63·00	16·00	62·93	16·27	62-86	16·55	
66	64·04	15·97	63·97	16·25	63·90	16·53	63-83	16·80	
67	65·01	16·21	64·94	16·49	64·87	16·78	64-79	17·06	
68	65·98	16·45	65·91	16·74	65·83	17·03	65-76	17·31	
69	66·95	16·69	66·88	16·98	66·80	17·28	66-73	17·57	
70	67·92	16·93	67·85	17·23	67·77	17·53	67-69	17·82	
71	68·89	17·18	68·82	17·48	68·74	17·78	68.66	18·08	71
72	69·86	17·42	69·78	17·72	69·71	18·03	69.63	18·33	72
73	70·83	17·66	70·75	17·97	70·67	18·28	70.59	18·59	73
74	71·80	17·90	71·72	18·22	71·64	18·53	71.56	18·84	74
75	72·77	18·14	72·69	18·46	72·61	18·78	72.58	19·10	75
76	73·74	18·39	73·66	18·71	73·58	19·03	73.50	19·35	76
77	74·71	18·63	74·63	18·95	74·55	19·28	74.46	19·60	77
78	75·68	18·87	75·60	19·20	75·52	19·53	75.43	19·86	78
79	76·65	19·11	76·57	19·45	76·48	19·78	76.40	20·11	79
80	77·62	10·35	77·54	19·69	77·45	20·03	77.36	20·37	80
81	78·59	10·60	78·51	19·94	78·42	20·28	78·33	20·62	81 \ 82 \ 83 \ 84 \ 85 \ 86 \ 87 \ 88 \ 89 \ 90 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
82	79·56	10·84	79·48	20·18	79·39	20·53	79·30	20·88	
83	80·53	20·08	80·45	20·43	80·36	20·78	80·26	21·13	
84	81·50	20·32	81·42	20·68	81·32	21·03	81·23	21·39	
85	82·48	20·56	82·38	20·92	82·29	21·28	82·20	21·64	
86	83·45	20·81	83·35	21·17	83·26	21·53	83·17	21·90	
87	84·42	21·05	84·32	21·42	84·23	21·78	84·13	22·15	
88	85·39	21·29	85·29	21·66	85·20	22·03	85·10	22·41	
89	86·36	21·53	86·26	21·91	86·17	22·28	86·07	22·66	
90	87·33	21·77	87·23	22·15	87·13	22·53	87·03	22·91	
91	88·30	22·01	88·20	22·40	88·10	22·78	88.00	23·17	91
92	89·27	22·26	89·17	22·65	89·07	23·04	88.97	23·42	92
93	90·24	22·50	90·14	22·89	90·04	23·29	89.94	23·68	93
94	91·21	22·74	91·11	23·14	91·01	23·54	90.90	23·93	94
95	92·18	22·98	92·08	23·38	91·97	23·79	91.87	24·19	95
96	93·15	23·22	93·05	23·63	92·94	24·04	92.84	24·44	96
97	94·12	23·47	94·02	23·88	93·91	24·29	93.80	24·70	97
98	95·09	23·71	94·98	24·12	94·88	24·54	94.77	24·95	98
99	96·06	23·95	95·95	24·37	95·85	24·79	95.74	25·21	99
100	97·03	24·19	96·92	24·62	96·81	25·04	96.70	25·46	100
Diee.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nee.
Distance	76:	Deg.	753/4	Deg.	751/2	Deg.	751/4	Deg.	\ Distance

{	Distance	15 I	Deg.	151/4	Deg.	15½	Deg.	153/4	Deg.	Distance
}	псе.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
	1 2 3 4 5 6 7 8 9	0.97 1.93 2.90 3.86 4.83 5.80 6.76 7.73 8.69 9.66	0·26 0·52 0·78 1·04 1·29 1·55 1·81 2·07 2·33 2·59	0.96 1.93 2.89 3.86 4.82 5.79 6.75 7.72 8.68 9.65	0·26 0·53 0·79 1·05 1·32 1·58 1·84 2·10 2·37 2·63	0.96 1.93 2.89 3.85 4.82 5.78 6.75 7.71 8.67 9.64	0·27 0·53 0·80 1·07 1·34 1·60 1·87 2·14 2·41 2·67	0.96 1.92 2.89 3.85 4.81 5.77 6.74 7.70 8.66 9.62	0·27 0·54 0·81 1·09 1·36 1·63 1·90 2·17 2·44 2·71	1 2 3 4 5 6 7 8 9 10 }
· · · · · · · · · · · · · · · · · · ·	11 12 13 14 15 16 17 18 19 20	10·63 11·59 12·56 13·52 14·49 15·45 16·42 17·39 18·35 19·32	2·85 3·11 3·36 3·62 3·88 4·14 4·40 4·66 4·92 5·18	10·61 11·58 12·54 13·51 14·47 15·44 16·40 17·37 18·33 19·30	2·89 3·16 3·42 3·68 3·95 4·21 4·47 4·73 5·00 5·26	10·60 11·56 12·53 13·49 14·45 15·42 16·38 17·35 18·31 19·27	2·94 3·21 3·47 3·74 4·01 4·28 4·54 4·81 5·08 5·34	10·59 11·55 12·51 13·47 14·44 15·40 16·36 17·32 18·29 19·25	2·99 3·26 3·53 3·80 4·07 4·34 4·61 4·89 5·16 5·43	11
· · · · · · · · · · · · · · · · · · ·	21 22 23 24 25 26 27 28 29 30	20·28 21·25 22·22 23·18 24·15 25·11 26·08 27·05 28·01 28·98	5·44 5·69 5·95 6·21 6·47 6·73 6·99 7·25 7·51 7·76	20·26 21·23 22·19 23·15 24·12 25·08 26·05 27·01 27·98 28·94	5.52 5.79 6.05 6.31 6.58 6.84 7.10 7.36 7.63	20·24 21·20 22·16 23·13 24·09 25·05 26·02 26·98 27·95 28·91	5·61 5·88 6·15 6·41 6·68 6·95 7·22 7·48 7·75 8·02	20·21 21·17 22·14 23·10 24·06 25·02 25·99 26·95 27·91 28·87	5·70 5·97 6·24 6·51 6·79 7·06 7·33 7·60 7·87 8·14	21 22 23 24 25 26 27 28 29 30
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	41 42 43 44 45 46 47 48 49	39·60 40·57 41·53 42·50 43·47 44·43 45·40 46·36 47·33 48·30	10·61 10·87 11·13 11·39 11·65 11·91 12·16 12·42 12·68 12·94	39·56 40·52 41·49 42·45 43·42 44·38 45·35 46·31 47·27 48·24	10·78 11·05 11·31 11·57 11·84 12·10 12·36 12·63 12·89 13·15	39·51 40·47 41·44 42·40 43·36 44·33 45·29 46·25 47·22 48·18	10.96 11.22 11.49 11.76 12.03 12.29 12.56 12.83 13.09 13.36	39·46 40·42 41·39 42·35 43·31 44·27 45·24 46·20 47·16 48·12	11·13 11·40 11·67 11·94 12·21 12·49 12·76 13·03 13·30 13·57	41 42 43 44 45 46 47 48 49 50
}	.eoun	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Eace.
{	Distance.	75	Deg.	743/2	Leg.	741/	∑ Deg.	741/4	Deg.	Distance

Distance	15 I	Oeg.	$15\frac{1}{4}$	Deg.	15½	Deg.	153/4	Deg.	} Distance,
псе.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce,
51	49·26	13·20	49·20	13·41	49·15	13·63	49·09	13·84	51
52	50·23	13·46	50·17	13·68	50·11	13·90	50·05	14·11	52
53	51·19	13·72	51·13	13·94	51·07	14·16	51·01	14·39	53
54	52·16	13·98	52·10	14·20	52·04	14·43	51·97	14·66	54
55	53·13	14·24	53·06	14·47	53·00	14·70	52·94	14·93	55
56	54·09	14·49	54·03	14·73	53·96	14·97	53·90	15·20	56
57	55·06	14·75	54·99	14·99	54·93	15·23	54·86	15·47	57
58	56·02	15·01	55·96	15·26	55·89	15·50	55·82	15·74	58
59	56·99	15·27	56·92	15·52	56·85	15·77	56·78	16·01	59
60	57·96	15·53	57·89	15·78	57·82	16·03	57·75	16·29	60
61	58-92	15·79	58·85	16·04	58·78	16·30	58·71	16·56	61
62	59-89	16·05	59·82	16·31	59·75	16·57	59·67	16·83	62
63	60-85	16·31	60·78	16·57	60·71	16·84	60·63	17·10	63
64	61-82	16·56	61·75	16·83	61·67	17·10	61·60	17·87	64
65	62-79	16·82	62·71	17·10	62·64	17·37	62·56	17·64	65
66	63-75	17·08	63·68	17·36	63·60	17·64	63·52	17·92	66
67	64-72	17·34	64·64	17·62	64·56	17·90	64·48	18·19	67
68	65-68	17·60	65·61	17·89	65·53	18·17	65·45	18·46	68
69	66-65	17·86	66·57	18·15	66·49	18·44	66·41	18·73	69
70	67-61	18·12	67·54	18·41	67·45	18·71	67·37	19·00	70
71	68·58	18·38	68·50	18·68	68·42	18·97	68·33	19·27	71
72	69·55	18·63	69·46	18·94	69·38	19·24	69·30	19·54	72
73	70·51	18·89	70·43	19·20	70·35	19·51	70·26	19·82	73
74	71·48	19·15	71·39	19·46	71·31	19·78	71·22	20·09	74
75	72·44	19·41	72·36	19·73	72·27	20·04	72·18	20·36	75
76	73·41	19·67	73·32	19·99	73·24	20·31	73·15	20·63	76
77	74·38	19·93	74·29	20·25	74·20	20·58	74·11	20·90	77
78	75·34	20·19	75·25	20·52	75·16	20·84	75·07	21·17	78
79	76·31	20·45	76·22	20·78	76·13	21·11	76·03	21·44	79
80	77·27	20·71	77·18	21·04	77·09	21·38	77·00	21·72	80
81	78·24	20.96	78-15	21·31	78.05	21·65	77.96	21·99	81 82 83 84 85 86 87 88 89 90 90
82	79·21	21.22	79-11	21·57	79.02	21·91	78.92	22·26	
83	80·17	21.48	80-08	21·83	79.98	22·18	79.88	22·53	
84	81·14	21.74	81-04	22·09	80.94	22·45	80.85	22·80	
85	82·10	22.00	82-01	22·36	81.91	22·72	81.81	23·07	
86	83·07	22.26	82-97	22·62	82.87	22·98	82.77	23·34	
87	84·04	22.52	83-94	22·88	83.84	23·25	83.73	23·62	
88	85·00	22.78	84-90	23·15	84.80	23·52	84.70	23·89	
89	85·97	23.03	85-87	23·41	85.76	23·78	85.66	24·16	
90	86·93	23.29	86-83	23·67	86.73	24·05	86.62	24·43	
91	87.90	23·55	87:80	23·94	87·69	24·32	87.58	24·70	91
92	88.87	23·81	88:76	24·20	88·65	24·59	88.55	24·97	92
93	89.83	24·07	89:73	24·46	89·62	24·85	89.51	25·24	93
94	90.80	24·33	90:69	24·72	90·58	25·12	90.47	25·52	94
95	91.76	24·59	91:65	24·99	91·54	25·39	91.43	25·79	95
96	92.73	24·85	92:62	25·25	92·51	25·65	92.40	26·06	96
97	93.69	25·11	93:58	25·51	93·47	25·92	93.36	26·33	97
98	94.66	25·36	94:55	25·78	94·44	26·19	94.32	26·60	98
99	95.63	25·62	95:51	26·04	95·40	26·46	95.28	26·87	99
100	96.59	25·88	96:48	26·30	96·36	26·72	96.25	27·14	100
Distance.	Dep. 75	Lat.	Dep. 743/2	Lat.	Dep. 74 ½	Lat.	Dep. 741/2	Lat.	Distance.

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}	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
	1 2 3 4 5 6 7 8 9	0.96 1.92 2.88 3.85 4.81 5.77 6.73 7.69 8.65 9.61	0·28 0·55 0·83 1·10 1·38 1·65 1·93 2·21 2·48 2·76	0.96 1.92 2.88 3.84 4.80 5.76 6.72 7.68 8.64 9.60	0·28 0·56 0·84 1·12 1·40 1·68 1·96 2·24 2·52 2·80	0.96 1.92 2.88 3.84 4.79 5.75 6.71 7.67 8.63 9.59	0·28 0·57 0·85 1·14 1·42 1·70 1·99 2·27 2·56 2·84	0.96 1.92 2.87 3.83 4.79 5.75 6.70 7.66 8.62 9.58	0·29 0·58 0·56 1·15 1·44 1·73 2·02 2·31 2·59 2·88	1 2 3 4 5 6 7 8 9 10 5
	11 12 13 14 15 16 17 18 19 20	10·57 11·54 12·50 13·46 14·42 15·38 16·34 17·30 18·26 19·23	3·03 3·31 3·58 3·86 4·13 4·41 4·69 4·96 5·24 5·51	10·56 11·52 12·48 13·44 14·40 15·36 16·32 17·28 18·24 19·20	3·08 3·64 3·92 4·20 4·48 4·76 5·04 5·32 5·60	10·55 11·51 12·46 13·42 14·38 15·34 16·30 17·26 18·22 19·18	3·12 3·41 3·69 3·98 4·26 4·54 4·83 5·11 5·40 5·68	10·53 11·49 12·45 13·41 14·36 15·32 16·28 17·24 18·19 19·15	3·17 3·46 3·75 4·03 4·32 4·61 4·90 5·19 5·48 5·76	11
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· · · · · · · · · · · · · · · · · · ·	31 32 33 34 35 36 37 38 39 40	29·80 30·76 31·72 32·68 33·64 34·61 35·57 36·53 37·49 38·45	8·54 8·82 9·10 9·37 9·65 9·92 10·20 10·47 10·75 11·03	29·76 30·72 31·68 32·64 33·60 34·56 35·52 36·48 37·44 38·40	8.67 8.95 9.23 9.51 9.79 10.07 10.35 10.63 10.91 11.19	29·72 30·68 31·64 32·60 33·56 34·52 35·48 36·44 37·39 38·35	8·80 9·09 9·37 9·66 9·94 10·22 10·51 10·79 11·08 11·36	29·68 30·64 31·60 32·56 33·51 34·47 35·43 36·39 37·35 38·30	8.93 9.22 9.51 9.80 10.09 10.38 10.66 10.95 11.24 11.53	31 32 33 34 35 36 37 38 39 40
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52	49.45	16·07	49·38	16·28	49:31	16·50	49·24	16·71	52
53	50·41	16·38	50·33	16·60	50:26	16·82	50·19	17·04	53
54	51·36	16·69	51·28	16·91	51:21	17·13	51·13	17·36	54
55	52·31	17·00	52·23	17·22	52:16	17·45	52·08	17·68	55
56	53·26	17·30	53·18	17·54	53:11	17·77	53·03	18·00	56
57	54·21	17·61	54·13	17·85	54:05	18·09	53·98	18·32	57
58	55·16	17·92	55·08	18·16	55:00	18·40	54·92	18·64	58
59	56·11	18·23	56·03	18·48	55:95	18·72	55·87	18·96	59
60	57·06	18·54	56·98	18·79	56:90	19·04	56·82	19·29	60
61	58·01	18·85	57·93	19·10	57·85	19·36	57·76	19·61	61 62 63 64 65 66 67 68 69 70
62	58·97	19·16	58·88	19·42	58·80	19·67	58·71	19·93	
63	59·92	19·47	59·83	19·73	59·74	19·99	59·66	20·25	
64	60·87	19·78	60·78	20·04	60·69	20·31	60·60	20·57	
65	61·82	20·09	61·73	20·36	61·64	20·62	61·55	20·89	
66	62·77	20·40	62·68	20·67	62·59	20·94	62·50	21·22	
67	63·72	20·70	63·63	20·98	63·54	21·26	63·44	21·54	
68	64·67	21·01	64·58	21·30	64·49	21·58	64·39	21·86	
69	65·62	21·32	65·53	21·61	65·43	21·89	65·34	22·18	
70	66·57	21·63	66·48	21·92	66·38	22·21	66·29	22·50	
71	67·53	21·94	67·43	22·23	67·33	22·53	67·23	22·82	71
72	68·48	22·25	68·38	22·55	68·28	22·85	68·18	23·14	72
73	69·43	22·56	69·33	22·86	69·23	23·16	69·13	23·47	73
74	70·38	22·87	70·28	23·17	70·18	23·48	70·07	23·79	74
75	71·33	23·18	71·23	23·49	71·12	23·80	71·02	24·11	75
76	72·28	23·49	72·18	23·80	72·07	24·12	71·97	24·43	76
77	73·23	23·79	73·13	24·11	73·02	24·43	72·91	24·75	77
78	74·18	24·10	74·08	24·43	73·97	24·75	73·86	25·07	78
79	75·13	24·41	75·03	24·74	74·92	25·07	74·81	25·39	79
80	76·08	24·72	75·98	25·05	75·87	25·38	75·75	25·72	80
81	77.04	25·03	76.93	25·37	76·81	25·70	76·70	26·04	81 82 83 84 85 86 87 88 89 90 \$
82	77.99	25·34	77.88	25·68	77·76	26·02	77·65	26·36	
83	78.94	25·65	78.83	25·99	78·71	26·34	78·60	26·68	
84	79.89	25·96	79.77	26·31	79·66	26·65	79·54	27·00	
85	80.84	26·27	80.72	26·62	80·61	26·97	80·49	27·32	
86	81.79	26·58	81.67	26·93	81·56	27·29	81·44	27·64	
87	82.74	26·88	82.62	27·25	82·50	27·61	82·38	27·97	
88	83.69	27·19	83.57	27·56	83·45	27·92	83·33	28·29	
89	84.64	27·50	84.52	27·87	84·40	28·24	84·28	28·61	
90	85.60	27·81	85.47	28·18	85·35	28·56	85·22	_28·93	
91	86·55	28·12	86·42	28·50	86·30	28.87	86·17	29·25	91
92	87·50	28·43	87·37	28·81	87·25	29.19	87·12	29·57	92
93	88·45	28·74	88·32	29·12	88·19	29.51	88·06	29·89	93
94	89·40	29·05	89·27	29·44	89·14	29.83	89·01	30·22	94
95	90·35	29·36	90·22	29·75	90·09	30.14	89·96	30·54	95
96	91·30	29·67	91·17	30·06	91·04	30.46	90·91	30·86	96
97	92·25	29·97	92·12	30·38	91·99	30.78	91·85	31·18	97
98	93·20	30·28	93·07	30·69	92·94	31.10	92·80	31·50	98
99	94·15	30·59	94·02	31·00	93·88	31.41	93·75	31·82	99
100	95·11	30·90	94·97	31·32	94·83	31.73	94·69	32·14	100
Distance.	72	Lat.	Dep. 713/4	Lat.	71½	Lat.	71½	Lat.	Distance.

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Distance	19 I	Deg.	191/4	Deg.	19½	Deg.	1934	Deg.	Distance
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1 2 3 4 5 6 7 8 9	0.95 1.89 2.84 3.78 4.73 5.67 6.62 7.56 8.51 9.46	0·33 0·65 0·98 1·30 1·63 1·95 2·28 2·60 2·93 3·26	0.94 1.89 2.83 3.78 4.72 5.66 6.61 7.55 8.50 9.44	0·33 0·66 0·99 1·32 1·65 1·98 2·31 2·64 2·97 3·30	0.94 1.89 2.83 3.77 4.71 5.66 6.60 7.54 8.48 9.43	0.33 0.67 1.00 1.34 1.67 2.00 2.34 2.67 3.00 3.34	0.94 1.88 2.82 3.76 4.71 5.65 6.59 7.53 8.47 9.41	0.84 0.68 1.01 1.35 1.69 2.03 2.37 2.70 3.04 3.38	1 2 3 4 5 6 7 8 9
11 12 13 14 15 16 17 18 19 20	$\begin{array}{c} 10\cdot 40 \\ 11\cdot 35 \\ 12\cdot 29 \\ 13\cdot 24 \\ 14\cdot 18 \\ 15\cdot 13 \\ 16\cdot 07 \\ 17\cdot 02 \\ 17\cdot 96 \\ 18\cdot 91 \end{array}$	3·58 3·91 4·23 4·56 4·88 5·21 5·53 5·86 6·19 6·51	10·38 11·33 12·27 13·22 14·16 15·11 16·05 16·99 17·94 18·88	3.63 3.96 4.29 4.62 4.95 5.28 5.60 5.93 6.26 6.59	10·37 11·31 12·25 13·20 14·14 15·08 16·02 16·97 17·91 18·85	3·67 4·01 4·34 4·67 5·01 5·34 5·67 6·01 6·34 6·68	10·35 11·29 12·24 13·18 14·12 15·06 16·00 16·94 17·88 18·82	3·72 4·06 4·39 4·73 5·07 5·41 5·74 6·08 6·42 6·76	11 (12 (13 (14 (15 (15 (15 (15 (15 (15 (15 (15 (15 (15
21 22 23 24 25 26 27 28 29 30	19·86 20·80 21·75 22·69 23·64 24·58 25·53 26·47 27·42 28·37	6·84 7·16 7·49 7·81 8·14 8·46 8·79 9·12 9·44 9·77	19·83 20·77 21·71 22·66 23·60 24·55 25·49 26·43 27·38 28·32	6·92 7·25 7·58 7·91 8·24 8·57 8·90 9·23 9·56 9·89	19·80 20·74 21·68 22·62 23·57 24·51 25·45 26·39 27·34 28·28	7·01 7·34 7·68 8·01 8·35 8·68 9·01 9·35 9·68 10·01	19·76 20·71 21·65 22·59 23·53 24·47 25·41 26·85 27·29 28·24	7·10 7·43 7·77 8·11 8·45 8·79 9·12 9·46 9·80 10·14	21 (22 (23 (24 (25 (27 (28 (29 (29 (29 (29 (29 (29 (29 (29 (29 (29
31 32 33 34 35 36 37 38 39 40	29·31 30·26 31·20 32·15 33·09 34·04 34·98 35·93 36·88 87·82	10·09 10·42 10·74 11·07 11·39 11·72 12·05 12·37 12·70 13·02	29·27 30·21 31·15 32·10 33·04 33·99 34·93 35·88 36·82 37·76	10·22 10·55 10·88 11·21 11·54 11·87 12·20 12·53 12·86 13·19	29·22 30·16 31·11 32·05 32·99 33·94 34·88 35·82 36·76 37·71	10·35 10·68 11·02 11·35 11·68 12·02 12·35 12·68 13·02 13·35	29·18 30·12 31·06 32·00 32·94 33·88 34·82 35·76 36·71 37·65	10·48 10·81 11·15 11·49 11·83 12·17 12·50 12·84 13·18 13·52	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	38·77 39·71 40·66 41·60 42·55 43·49 44·44 45·38 46·33 47·28	13·35 13·67 14·00 14·32 14·65 14·98 15·30 15·63 15·95 16·28	38·71 39·65 40·60 41·54 42·48 43·43 44·37 45·32 46·26 47·20	13·52 13·85 14·18 14·51 14·84 15·17 15·50 15·83 16·15 16·48	38·65 39·59 40·53 41·48 42·42 43·36 44·30 45·25 46·19 47·13	13·69 14·02 14·35 14·69 15·02 15·36 15·69 16·02 16·36 16·69	38·59 39·53 40·47 41·41 42·35 43·29 44·24 45·18 46·12 47·06	13·85 14·19 14·53 14·87 15·21 15·54 15·88 16·22 16·56 16·90	41 42 43 44 45 46 47 48 49 50
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61 62 63 64 65 66 67 68 69 70	57.68 58.62 59.57 60.51 61.46 62.40 63.35 64.30 65.24 66.19	19·86 20·19 20·51 20·84 21·16 21·49 21·81 22·14 22·46 22·79	57·59 58·53 59·48 60·42 61·37 62·31 63·25 64·20 65·14 66·09	20·11 20·44 20·77 21·10 21·43 21·76 22·09 22·42 22·75 23·08	57·50 58·44 59·39 60·33 61·27 62·21 63·16 64·10 65·04 65·98	20·36 20·70 21·03 21·36 21·70 22·03 22·37 22·70 23·03 23·37	57·41 58·35 59·29 60·24 61·18 62·12 63·06 64·00 64·94 65·88	20·61 20·95 21·29 21·63 21·96 22·30 22·64 22·98 23·32 23·65	61 62 63 64 65 66 66 67 68 69 70
71 72 73 74 75 76 77 78 80	67·13 68·08 69·02 69·97 70·91 71·86 72·80 73·75 74·70 75·64	23·12 23·44 23·77 24·09 24·42 24·74 25·07 25·39 25·72 26·05	67.03 67.97 68.92 69.86 70.81 71.75 72.69 73.64 74.58 75.53	23·41 23·74 24·07 24·40 24·73 25·06 25·39 25·72 26·05 26·38	66.93 67.87 68.81 69.76 70.70 71.64 72.58 73.53 74.47 75.41	23·70 24·03 24·37 24·37 25·04 25·37 25·70 26·04 26·37 26·70	66·82 67·76 68·71 69·65 70·59 71·53 72·47 73·41 74·35 75·29	23·99 24·33 24·67 25·01 25·34 25·68 26·02 26·36 26·70 27·03	71
81 82 83 84 85 86 87 88 89 90	76·59 77·53 78·48 79·42 80·37 81·31 82·26 83·21 84·15 85·10	26·37 26·70 27·02 27·35 27·67 28·00 28·32 28·65 28·98 29·30	76·47 77·42 78·36 79·30 80·25 81·19 82·14 83·08 84·02 84·97	26·70 27·03 27·36 27·69 28·02 28·35 28·68 29·01 29·34 29·67	76·35 77·30 78·24 79·18 80·12 81·07 82·01 82·95 83·90 84·84	27·04 27·37 27·71 28·04 28·37 28·71 29·04 29·37 29·71 30·04	76·24 77·18 78·12 79·06 80·00 80·94 81·88 82·82 83·76 84·71	27·37 27·71 28·05 28·39 28·72 29·06 29·40 29·74 30·07 30·41	81 82 83 84 85 86 87 88 89 90 \$
91 92 93 94 95 96 97 98 99 100	86·04 86·99 87·93 88·88 89·82 90·77 91·72 92·66 93·61 94·55	29·63 29·95 30·28 30·60 30·93 31·25 31·58 31·91 32·23 32·56	85·91 86·86 87·80 88·74 89·69 90·63 91·58 92·52 93·46 94·41	30·00 30·33 30·66 30·99 31·32 31·65 31·98 32·31 32·64 32·97	85·78 86·72 87·67 88·61 89·55 90·49 91·44 92·38 93·32 94·26	30·38 30·71 31·04 31·38 31·71 32·05 32·38 32·71 33·05 33·38	85·65 86·59 87·53 88·47 89·41 90·35 91·29 92·24 93·18 94·12	30·75 31·09 31·43 31·76 32·10 32·44 32·78 33·12 33·45 33·79	91 92 93 94 95 96 97 98 99 100
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Bice.
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	1 2 3 4 5 6 7 8 9	0.94 1.88 2.82 3.76 4.70 5.64 6.58 7.52 8.46 9.40	0·34 0·68 1·03 1·37 1·71 2·05 2·39 2·74 3·08 3·42	0.94 1.88 2.81 3.75 4.69 5.63 6.57 7.51 8.44 9.38	0·35 0·69 1·04 1·38 1·73 2·08 2·42 2·77 3·12 3·46	0.94 1.87 2.81 3.75 4.68 5.62 6.56 7.49 8.43 9.37	0·35 0·70 1·05 1·40 1·75 2·10 2·45 2·80 3·15 3·50	0·94 1·87 2·81 3·74 4·68 5·61 6·55 7·48 8·42 9·35	0·35 0·71 1·06 1·42 1·77 2·13 2·48 2·83 3·19 3·54	1 2 3 4 5 6 7 8 9
· · · · · · · · · · · · · · · · · · ·	11 12 13 14 15 16 17 18 19 20	10·34 11·28 12·22 13·16 14·10 15·04 15·97 16·91 17·85 18·79	3·76 4·10 4·45 4·79 5·13 5·47 5·81 6·16 6·50 6·84	10·32 11·26 12·20 13·13 14·07 15·01 15·95 16·89 17·83 18·76	3·81 4·15 4·50 4·85 5·19 5·54 5·88 6·23 6·58 6·92	10·30 11·24 12·18 13·11 14·05 14·99 15·92 16·86 17·80 18·73	3·85 4·20 4·55 4·90 5·25 5·60 5·95 6·30 6·65 7·00	10·29 11·22 12·16 13·09 14·03 14·96 15·90 16·83 17·77 18·70	3·90 4·25 4·61 4·96 5·31 5·67 6·02 6·38 6·73 7·09	11 2 13 14 15 16 17 18 19 20 \$
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· · · · · · · · · · · · · · · · · · ·	31 32 33 34 35 36 37 38 39 40	29·13 30·07 31·01 31·95 32·89 33·83 34·77 35·71 36·65 37·59	10·60 10·94 11·29 11·63 11·97 12·31 12·65 13·00 18·34 13·68	29·08 30·02 30·96 31·90 32·84 33·77 34·71 35·65 36·59 37·53	10·73 11·08 11·42 11·77 12·11 12·46 12·81 13·15 13·50 13·84	29·04 29·97 30·91 31·85 32·78 33·72 34·66 35·59 36·53 37·47	10·86 11·21 11·56 11·91 12·26 12·61 12·96 13·31 13·66 14·01	28·99 29·92 30·86 31·79 32·73 33·66 34·60 35·54 36·47 37·41	10.98 11.34 11.69 12.05 12.40 12.75 13.11 13.46 13.82 14.17	31 32 33 34 35 36 37 38 38 39 40
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52         4.886         17.79         48.79         18.90         48.71         18.21         48.63         18.42         52         53         49.90         18.13         49.72         18.34         49.64         18.56         49.56         18.78         53         55         51.68         18.81         19.64         18.56         52.62         19.15         52.61         19.44         51.52         19.26         51.43         19.73         53.39         19.96         53.30         20.19         57           58         54.50         19.64         54.42         20.07         54.33         20.31         54.24         20.56         58         59         55.44         20.18         55.55         20.24         55.26         20.66         55.17         20.96         59         56.60         20.63         58         20.52         56.29         20.77         56.26         20.66         56.71         20.96         56.36         20.65         58         60         56.23         21.11         57.14         21.36         56.91         22.26         66         66.26         62.22         12.51         58.71         21.41         57.14         21.41         57.42         12.61         61         22	}-										(
53         49-80         18-13         40-72         18-34         49-64         18-56         40-56         18-78         53           54         50-74         18-47         50-66         18-90         50-55         18-91         50-56         19-15         50-56         19-15         50-54         19-14         51-52         19-26         51-33         19-49         55           56         52-62         19-15         52-54         19-61         52-37         19-84         56           57         53-56         19-50         53-48         19-73         53-99         19-96         53-30         20-19         57           60         56-38         20-52         25-77         56-20         20-66         55-17         20-90         56         66-56-36         55-29         20-77         56-20         21-01         56-11         21-20         60         56-38         20-22         20-27         56-20         21-01         57-14         21-61         61         67-32         20-86         57-22         21-11         57-41         57-44         21-61         61         62-62         21-21         58-71         21-46         68-60         56-46         21-21         58-71	}.	52		17.79		18.00	48.71	18.21	48.63	18.42	52
55         5168         1881         5160         1904         5152         1926         5143         1948         556         566         5262         1915         5254         1973         53245         1973         5323         1996         5330         2019         57           58         5450         1984         5442         2007         5433         2031         5424         2055         58           60         5638         2052         5529         2077         5620         2101         5611         2123         60           61         5732         2086         5723         2111         5714         2136         5704         2161         61         626         6826         2121         5817         2146         8807         2171         5704         2161         61         661         2121         5817         2146         8807         22717         5704         2161         61         626         6826         2121         5817         2146         5807         2171         5704         2161         61         6265         62231         6014         2189         6044         2215         5995         2241         5985         2247	2	53						18.56			53
56         5262         19·15         52·54         19·38         52·45         19·61         52·37         19·84         56           57         53·56         19·60         53·49         19·73         53·39         19·66         53·39         20·19         53·39         20·19         53·39         20·19         55·55         58·24         20·07         54·33         20·31         54·24         20·55         58           60         56·38         20·52         55·39         20·77         56·20         21·01         56·11         22·29         69           61         57·32         20·86         57·23         21·11         57·14         21·36         57·04         21·61         61           62         68·26         21·21         58·17         21·46         58·07         21·71         57·98         21·97         62           63         69·20         21·55         59·11         21·61         58·17         21·11         57·14         21·36         58·19         22·21         66         66·202         22·57         61·92         22·81         61·82         23·11         61·13         61·96         22·25         61·96         22·81         61·82         23·11 <td>7</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>19:13</td> <td>54</td>	7									19:13	54
58         5450         1984         5442         2007         5433         2031         5424         2009         58           60         5638         20-52         5629         20-77         56-20         21-01         56-11         21-26         60           61         57-32         20-86         57-23         21-11         57-14         21-36         57-04         21-61         61           62         58-26         21-21         58-17         21-46         58-07         21-71         57-98         21-97         62           63         69-20         21-55         59-11         21-81         59-01         22-60         58-91         22-32         64           64         60-14         21-89         60-04         22-15         59-95         22-41         59-55         22-67         64           65         61-98         22-23         60-98         22-76         69-86         23-11         61-72         23-33         66           66         62-92         22-25         66-86         23-21         66-69         23-49         66-67         24-23         65-67         24-23         66-62         23-44         67           <	7	56	51.68		55.54	10.38		19.20	52.27	10.84	56
58         5450         1984         5442         2007         5433         2031         5424         2009         58           60         5638         20-52         5629         20-77         56-20         21-01         56-11         21-26         60           61         57-32         20-86         57-23         21-11         57-14         21-36         57-04         21-61         61           62         58-26         21-21         58-17         21-46         58-07         21-71         57-98         21-97         62           63         69-20         21-55         59-11         21-81         59-01         22-60         58-91         22-32         64           64         60-14         21-89         60-04         22-15         59-95         22-41         59-55         22-67         64           65         61-98         22-23         60-98         22-76         69-86         23-11         61-72         23-33         66           66         62-92         22-25         66-86         23-21         66-69         23-49         66-67         24-23         65-67         24-23         66-62         23-44         67           <	7	57	53:56	19.50	53:48	19.73	53.39	19.96	53:30	20.19	57
Color	(	58				20.07	54.33	20.31	54.24	20.55	58
State	(										
62 58-26 21-21 58-37 21-46 58-07 21-71 57-98 21-97 62 63 68-90 21-255 59-11 21-81 59-90 1 22-06 58-91 22-32 63 64 60-14 21-89 60-04 22-15 59-95 22-41 59-95 22-37 64 65-66 61-98 22-23 60-98 22-50 60-88 22-76 60-78 23-03 65-66 62-02 22-57 61-92 22-64 61-82 23-11 61-72 23-88 66 66 62-02 22-57 61-92 22-64 61-82 23-11 61-72 23-88 66 68 63-90 22-25 63-80 23-16 62-76 23-46 62-05 23-74 67 68 63-90 22-25 63-80 23-54 63-69 23-81 63-92 4-09 68 63-90 22-25 63-80 23-54 63-69 23-81 63-92 4-09 68 69-04-84 23-60 64-74 23-83 64-63 24-16 64-62 24-43 60-70 65-78 23-94 65-67 24-23 65-57 24-51 65-46 24-80 70 65-78 23-94 65-67 24-23 65-57 24-51 65-46 24-80 70 70 65-78 23-94 65-67 24-23 65-57 24-51 65-46 24-80 70 71 66-72 24-28 66-61 24-57 66-50 24-86 66-39 25-15 71 72 67-66 24-63 67-55 24-92 67-44 25-21 67-33 25-51 72 73 68-60 24-97 68-49 25-27 68-32 25-57 68-26 25-86 73 74 69-54 25-31 69-43 25-61 69-31	5	60	56.38	20.52	56.29	20.77	56.20	21.01	56.11	21 26	60
68	>	61.	57.32	20.86		21.11	57.14	21.36		21.61	61
64         60-14         21-89         60-04         22-15         59-95         22-41         59-85         22-67         64           65         61-08         22-257         61-92         22-58         60-88         22-76         60-93         23-33         66           67         62-96         22-92         62-86         23-10         62-76         22-46         62-65         23-11         61-72         23-38         66           68         63-90         22-25         63-80         23-81         63-69         28-18         63-69         24-90         68         63-90         22-25         65-67         24-23         65-67         24-23         66-62         22-44-50         69-40         26-67         70         65-78         24-28         66-61         24-57         66-50         24-86         66-63         25-15         71         71         66-72         24-28         66-61         24-57         66-50         24-86         66-63         25-15         71           71         66-72         24-28         66-61         24-57         66-50         24-86         66-63         25-15         71           72         66-62         24-80         25-27	$\rangle$	62	58.26	21.21	58.17	21.46	50.01	21.71	59.01	21.97	62
65         61.08         22.23         (60.98)         22.50         60.88         22.76         66.72         22.57         61.92         22.84         61.82         23.11         61.72         23.38         66           67         62.96         22.92         62.86         23.10         62.76         23.46         62.65         23.74         67           68         63.90         23.26         63.80         23.61         63.69         24.90         68           69         64.84         23.60         64.74         23.88         64.63         24.16         64.52         24.45         69           70         65.78         23.94         65.67         24.23         65.67         24.51         66.61         24.57         66.60         24.86         66.99         25.15         71           72         67.62         24.93         67.52         24.92         67.44         25.21         66.39         25.15         71           73         68.60         24.97         68.49         25.27         68.38         25.67         68.26         25.86         73           74         69.54         25.65         70.35         25.96         70.25         2	7			21.89							64
66 6 6202 2257 6192 2258 6182 2310 6182 2311 6172 2338 66 67 6206 2392 6258 2310 6276 2346 6265 2374 67 68 6390 23:26 6380 23:54 63:69 23:81 63:59 24:90 68 69 64:84 23:60 64:74 23:88 64:63 24:16 64:52 24:45 69 70 65:78 2394 65:67 24:23 65:57 24:51 65:46 24:80 70 70 65:78 2394 65:67 24:23 65:57 24:51 65:46 24:80 70 70 70 70 70 70 70 70 70 70 70 70 70	7			22.23		22.50				23.03	65
68         63-90         23-26         63-80         23-54         63-69         24-90         68           69         64-84         23-60         64-74         23-88         64-63         24-16         64-52         24-45         69           70         65-78         23-94         65-67         24-23         65-57         24-51         65-64         24-80         70           71         66-72         24-28         66-61         24-57         66-50         24-86         66-39         25-15         71           73         76-66         24-63         67-55         24-92         67-44         25-21         68-38         25-57         68-32         25-58         73           74         69-54         25-31         69-43         25-61         69-31         25-92         69-20         26-22         74           75         70-48         25-65         70-33         25-96         70-25         26-27         70-14         26-67         75-76         71-42         25-99         71-30         26-30         71-19         26-62         71-07         26-93         76         77         79-36         26-34         72-24         26-65         72-12 <td< td=""><td>(</td><td>66</td><td>62.02</td><td>22:57</td><td>61.92</td><td>22.84</td><td></td><td>23.11</td><td>61.72</td><td>23.38</td><td>66</td></td<>	(	66	62.02	22:57	61.92	22.84		23.11	61.72	23.38	66
69         64-84         23-60         64-74         23-88         64-63         24-16         64-62         24-48         69           70         65-78         23-94         65-67         24-23         65-57         24-51         66-62         24-80         70           71         66-72         24-28         66-61         24-57         66-50         24-86         66-39         25-15         71           72         66-66         24-97         68-49         25-27         68-38         25-57         68-20         25-86         73           74         69-54         25-31         69-43         25-61         69-31         25-92         69-20         26-22         74           75         70-48         25-69         70-33         25-96         70-25         26-27         70-14         26-57         75           76         71-42         25-99         71-30         26-30         71-10         22-62         71-01         26-67         71-01         26-67         71-01         26-67         71-01         26-67         71-01         26-67         71-01         26-67         71-01         26-67         71-01         26-67         71-01         26-67	7	67	62.96							23.74	67
T1	(	68					64.69		63.59	24.09	
74 69-54 25-31 69-43 25-96 70-72-5 26-27 70-14 26-77 75-76 70-18 25-65 70-35 25-96 70-70-5 26-27 70-14 26-67 75-76 71-14 25-99 71-30 26-30 71-19 26-62 71-07 26-93 76-77 72-36 26-34 72-24 26-65 72-12 26-97 72-01 27-28 77-78 73-30 26-68 73-18 27-00 73-06 27-32 72-94 27-63 78-78 73-30 26-68 73-18 27-00 73-06 27-32 72-94 27-63 78-78 73-70 74-24 27-02 74-12 27-34 74-00 27-67 73-88 27-99 79-78 80 75-18 27-36 75-05 27-09 74-93 28-02 74-81 28-34 80 80 75-18 27-36 75-09 28-04 75-87 28-37 75-75 28-70 79-88 27-90 79-98 28-04 75-87 28-37 75-75 28-70 81 82-77 77-95 28-39 77-87 28-73 77-74 29-07 77-62 29-95 78-81 29-07 78-68 29-42 78-55 29-76 84 78-93 28-93 77-87 29-07 79-75 29-42 79-62 29-77 79-49 30-11 85-8 88-82-99 30-10 82-56 30-46 82-74 30-47 81-38 30-82 87 81-75 29-76 81-62 30-11 81-49 30-47 81-38 30-82 87 81-75 29-76 81-62 30-11 81-49 30-47 81-38 30-82 87 81-75 30-78 84-44 31-15 84-30 31-52 84-10 31-89 90 84-57 30-78 84-44 31-15 84-30 31-52 84-10 31-89 90 84-57 30-78 84-44 31-15 84-30 31-52 84-10 31-89 90 94 88-83 31-81 88-83 30-82 87 88-32 87 30-82 88-32 88-33 31-81 88-32 88-33 31-81 88-32 88-32 88-33 31-81 88-32 88-32 88-33 31-81 88-32 88-32 88-33 31-81 88-32 88-32 88-32 88-33 31-81 88-32 88-32 88-32 88-33 31-81 88-32 88-32 88-32 88-33 31-81 88-32 88-32 88-32 88-33 31-81 88-32 88-32 88-32 88-33 31-81 88-32 88-	ζ.	70		23.94				24.51	65.46	24.80	70
74 69-54 25-31 69-43 25-96 70-72-5 26-27 70-14 26-77 75-76 70-18 25-65 70-35 25-96 70-70-5 26-27 70-14 26-67 75-76 71-14 25-99 71-30 26-30 71-19 26-62 71-07 26-93 76-77 72-36 26-34 72-24 26-65 72-12 26-97 72-01 27-28 77-78 73-30 26-68 73-18 27-00 73-06 27-32 72-94 27-63 78-78 73-30 26-68 73-18 27-00 73-06 27-32 72-94 27-63 78-78 73-70 74-24 27-02 74-12 27-34 74-00 27-67 73-88 27-99 79-78 80 75-18 27-36 75-05 27-09 74-93 28-02 74-81 28-34 80 80 75-18 27-36 75-09 28-04 75-87 28-37 75-75 28-70 79-88 27-90 79-98 28-04 75-87 28-37 75-75 28-70 81 82-77 77-95 28-39 77-87 28-73 77-74 29-07 77-62 29-95 78-81 29-07 78-68 29-42 78-55 29-76 84 78-93 28-93 77-87 29-07 79-75 29-42 79-62 29-77 79-49 30-11 85-8 88-82-99 30-10 82-56 30-46 82-74 30-47 81-38 30-82 87 81-75 29-76 81-62 30-11 81-49 30-47 81-38 30-82 87 81-75 29-76 81-62 30-11 81-49 30-47 81-38 30-82 87 81-75 30-78 84-44 31-15 84-30 31-52 84-10 31-89 90 84-57 30-78 84-44 31-15 84-30 31-52 84-10 31-89 90 84-57 30-78 84-44 31-15 84-30 31-52 84-10 31-89 90 94 88-83 31-81 88-83 30-82 87 88-32 87 30-82 88-32 88-33 31-81 88-32 88-33 31-81 88-32 88-32 88-33 31-81 88-32 88-32 88-33 31-81 88-32 88-32 88-33 31-81 88-32 88-32 88-32 88-33 31-81 88-32 88-32 88-32 88-33 31-81 88-32 88-32 88-32 88-33 31-81 88-32 88-32 88-32 88-33 31-81 88-32 88-32 88-32 88-33 31-81 88-32 88-	>	71	66.72	24.28	66-61	24.57	66:50	24.86	66:39	25:15	71
74 69-54 25-31 69-43 25-96 70-72-5 26-27 70-14 26-77 75-76 70-18 26-56 70-53 25-96 70-70-5 26-27 70-14 26-57 75-76 71-14-2 25-99 71-30 26-30 71-19 26-62 71-07 26-93 76-77 72-36 26-34 72-24 26-65 72-72 26-72 72-94 27-23 76-77 72-36 26-36 73-18 27-00 73-06 27-32 72-94 27-63 78-78 78-78 26-68 73-18 27-00 73-06 27-32 72-94 27-63 78-78 78-	7	$7\bar{2}$							67.33		72
75 70-48 25-65 70-33 25-96 70-25 26-27 70-14 26-57 75-76 76 71-12 25-99 71-30 26-30 71-119 25-62 71-07 26-93 76-77 72-36 26-34 72-24 26-65 72-12 26-97 72-01 27-28 77-78 78 78-30 26-68 78-18 27-00 73-66 27-32 72-94 27-63 78 77-74-24 27-02 74-12 27-34 74-00 27-67 73-88 27-90 79 80 75-18 27-36 75-05 27-69 74-93 28-02 74-81 28-34 80 75-18 27-36 75-09 28-04 75-87 28-73 75-75 28-70 79-75 28-70 28-70 79-75	7	73	68.60	24.97		25.27			68.26	25.86	73
Tell	7	74		25.31				25.92	69.20	26.22	74
77         79.36         26.34         72.24         26.65         72.12         26.97         72.01         27.28         77           78         73.30         26.68         73.18         27.00         73.06         27.32         72.04         27.63         78           80         75.18         27.36         75.00         27.90         74.93         28.02         72.61         27.88         27.90         79           81         76.12         27.70         75.99         28.04         75.67         28.77         75.75         28.70         81           82         77.05         28.05         76.99         28.94         75.67         28.77         75.75         28.70         81           82         77.05         28.05         76.99         28.93         76.81         28.77         75.75         28.78         81           84         78.93         28.73         78.81         29.07         77.62         29.41         83           84         78.93         28.73         78.81         29.07         78.68         29.42         78.55         29.76         84           85         79.87         29.07         79.75         29.42	7					29.30	70.25	26.62			76
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	(									27.28	77
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	(	78	73.30	26.68	73.18	27.00	73.06	27:32	72.94	27.63	78
81         7612         27.70         75.99         28.04         75.87         28.37         75.75         28.70         81           82         77.95         28.36         76.93         23.38         76.81         28.72         76.68         29.05         82           83         77.99         28.39         77.87         28.73         77.74         29.07         77.62         29.41         83           84         78.93         28.73         78.81         29.07         78.68         29.42         78.55         29.76         29.41         83           85         79.87         29.07         79.75         29.42         79.62         29.77         79.49         30.11         85           86         80.81         29.14         80.82         29.77         79.49         30.11         85           87         81.75         29.76         81.62         30.11         81.49         30.47         81.63         30.82         87           88         32.69         30.10         82.63         30.44         83.50         30.80         83.36         31.18         88           89         38.63         30.44         83.50         30.80	ζ.	79	74.24		74.12	27.34	74.00	27.67	73.88	27.99	79
82         77-95         28-05         76-93         28-38         76-81         28-72         76-68         29-04         83           83         77-99         28-39         77-87         28-73         77-74         20-07         77-62         29-41         83           84         78-93         28-73         78-81         29-07         78-68         29-42         78-52         29-76         84           85         79-87         29-07         79-75         29-42         79-62         29-77         79-49         30-11         85           86         80-81         29-14         80-63         29-77         80-55         30-12         80-42         30-47         86           87         81-75         29-76         81-62         30-11         81-49         30-47         81-36         30-82         82-29         31-18         88           89         83-63         30-44         83-50         30-80         83-36         31-17         83-22         31-18         88           90         84-57         30-78         84-44         31-15         84-30         31-52         84-16         31-89         90           91         85-51	5	80	75.18	27.36	75.06	27.69	74.93	l	74.81	28.34	80
83         77-99         28-39         77-87         28-73         77-74         20-07         77-62         29-41         83           84         78-93         28-73         78-81         29-07         78-68         29-42         78-55         29-76         84           85         79-87         29-07         79-75         29-42         79-62         29-77         79-94         30-11         85           86         80-81         29-47         80-65         29-77         80-55         30-12         80-42         30-47         86           87         81-75         29-76         81-62         30-14         81-36         30-82         87           88         82-90         30-10         82-56         30-46         82-43         30-82         82-29         31-18         88           89         83-63         30-44         83-50         30-80         83-36         31-17         83-23         31-53         89           90         84-57         30-78         84-44         31-15         84-30         31-52         84-16         31-89         90           91         85-51         31-12         85-38         31-50         85-24	$\rangle$	81		27.70				28.37			
84         78-93         22-73         78-81         29-07         78-76         29-42         79-62         29-77         79-49         30-11         85           86         80-81         29-41         80-88         29-77         80-62         29-77         79-49         30-11         85           87         81-75         29-76         81-62         30-11         81-49         30-47         81-36         30-82         87           88         82-69         30-10         82-56         30-46         82-43         30-82         82-29         31-18         88           89         83-63         30-44         83-50         30-80         83-36         31-17         83-23         31-53         89           90         84-57         30-78         84-44         31-15         83-30         31-17         83-23         31-53         89           91         85-51         31-12         85-38         31-50         85-24         31-87         85-10         32-24         91           92         84-45         30-78         84-44         31-48         86-17         32-22         86-03         32-59         92           93         87-33	>	82	77.05			28.38					
85         79.87         29.07         79.75         29.42         79.62         29.77         79.49         30.11         85           86         30.81         29.41         80.68         29.77         80.55         30.12         80.42         30.47         86           87         81.75         29.76         81.62         30.11         81.49         30.47         81.30         30.82         87           88         82.69         30.10         82.56         30.46         82.43         30.82         82.29         31.18         88           89         38.63         30.44         83.50         30.80         33.63         31.75         89.31         31.53         89           90         84.57         30.78         84.44         31.15         84.30         31.52         84.16         31.89         90           91         85.51         31.12         85.38         31.50         85.24         31.87         85.10         32.24         91           92         86.45         31.47         86.31         31.84         86.17         32.22         86.03         32.59         92           93         87.39         31.81         87.25	$\rangle$		77.99			20.15					
86         80-81         29-41         80-68         29-77         80-55         30-12         80-42         30-47         86           87         81-75         29-76         81-62         30-41         81-99         30-82         87           88         82-69         30-10         82-56         30-46         82-43         30-82         82-29         31-18         88           89         83-63         30-44         83-50         30-80         83-36         31-17         82-23         31-53         89           90         84-57         30-78         84-44         31-15         84-30         31-52         82-23         31-53         89           91         85-51         31-12         85-38         31-50         85-24         31-87         85-10         32-24         91           92         86-45         31-47         86-31         31-84         86-17         32-22         86-03         32-59         92           93         87-39         31-81         87-25         32-19         87-11         32-57         86-97         32-95         93           94         88-33         32-215         88-19         32-24         88-98	$\rangle$										
87         81.75         29.76         81.62         30.11         81.49         30.47         81.836         30.82         87           88         82.69         30.10         82.56         30.46         82.43         30.82         82.29         31.18         88           89         83.63         30.44         83.50         30.80         83.36         31.17         82.33         31.53         89           90         84.57         30.78         84.44         31.15         84.30         31.52         84.16         31.89         90           91         85.51         31.42         85.38         31.50         85.24         31.87         85.10         32.24         91           92         86.45         31.47         86.31         31.84         86.17         32.22         86.03         32.59         92           93         87.39         31.81         87.25         32.19         87.11         32.57         86.97         32.95         93           94         88.33         32.15         88.19         32.54         88.89         32.92         87.90         33.30         94           95         89.27         32.49         89.13	$\rangle$		80.81	29.41	80.68				80.42	30.47	86
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	. ?	87	81.75	29.76	81.62	30.11	81.49	30.47	81.36	30.82	87
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	γ.	88			82.56	30.46	82.43	30.82	82.29	31.18	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7					30.80		31.17			90
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5		85.51	31.12					85.10		
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95 89-27 32-49 89-13 32-88 88-98 33-27 88-84 33-66 95 96 90-21 32-83 90-07 33-23 89-92 33-62 89-77 34-01 96 97 91-15 33-18 91-00 33-57 90-86 33-97 90-71 34-37 97 98 92-09 33-52 91-94 33-92 91-79 34-32 91-64 34-72 98 99 93-03 33-86 92-88 34-27 92-73 34-67 92-58 35-07 99 100 93-97 34-20 93-82 34-61 93-67 35-02 93-51 35-43 100	(		88.33	32:15	88-19	32.54	88.05	32.92	87.90	33.30	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5			32.49	89.13	32.88	88.98	33.27	88.84		.95
97         91-15         33-18         91-00         33-57         90-86         33-97         90-71         34-37         97           98         92-90         33-52         91-94         33-92         91-79         34-32         91-64         34-72         98           99         93-03         33-86         92-88         34-27         92-73         34-67         92-58         35-07         99           100         93-97         34-20         93-82         34-61         93-67         35-02         93-51         35-43         100	5	96	90.21	32.83	90.07	33.23	89.92	33.62	89.77	34.01	
99 93·03 33·86 92·88 34·27 92·73 34·67 92·58 35·07 99 100 93·97 34·20 93·82 34·61 93·67 35·02 93·51 35·43 100	5		91.15	33.18						34.37	
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\[ \frac{1}{2} \]	5	100	93.97	34.20	93.82	34.61	93.67	35.02		35.43	
Dep.   Lat. Dep.   Lat. Dep.   Lat.   3	δ.				ļ			ļ	ļ	·	<u> </u>
	ζ	Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	ı Lat.	рер.	ı Lat.	Distance
$\left\langle \begin{array}{c c} \overline{2} & 70 \text{ Deg.} & 69\% \text{ Deg.} & 69\% \text{ Deg.} & 69\% \text{ Deg.} & 5\% \end{array} \right $	5	sta.	70	Dec	693/	Dec.	6912	Deg.	691	Dec.	Sta
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}	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.;	8 {
	1 2 3 4 5 6 7 8 9	0.93 1.87 2.80 3.73 4.67 5.60 6.54 7.47 8.40 9.34	0·36 0·72 1·08 1·43 1·79 2·15 2·51 2·87 3·23 3·58	0.93 1.86 2.80 3.73 4.63 5.59 6.52 7.46 8.39 9.32	0·36 0·72 1·99 1·45 1·81 2·17 2·54 2·90 3·26 3·62	0.93 1.86 2.79 3.72 4.65 5.58 6.51 7.44 8.37 9.30	0·37 0·73 1·10 1·47 1·83 2·20 2·57 2·93 3·30 3·67	0.93 1.86 2.79 3.72 4.64 5.57 6.50 7.43 8.36 9.29	0·37 0·74 1·11 1·48 1·85 2·22 2·59 2·96 3·34 3·71	1 2 3 4 5 6 7 8 9 10 4
· · · · · · · · · · · · · · · · · · ·	11 12 13 14 15 16 17 18 19 20	10·27 11·20 12·14 13·07 14·00 14·94 15·87 16·80 17·74 18·67	3.94 4.30 4.66 5.02 5.38 5.73 6.09 6.45 6.81 7.17	10·25 11·18 12·12 13·05 13·98 14·91 15·84 16·78 17·71 18·64	3·99 4·35 4·71 5·07 5·44 5·80 6·16 6·52 6·89 7·25	10·23 11·17 12·10 13·03 13·96 14·89 15·82 16·75 17·68 18·61	4·03 4·40 4·76 5·13 5·50 5·86 6·23 6·60 6·96 7·33	10·22 11·15 12·07 13·00 13·93 14·86 15·79 16·72 17·65 18·58	4·08 4·45 4·82 5·19 5·56 5·93 6·30 6·67 7·04 7·41	11 \ 12 \ 13 \ 14 \ 15 \ 16 \ 17 \ 18 \ 19 \ 20 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
***************************************	21 22 23 24 25 26 27 28 29 30	19·61 20·54 21·47 22·41 23·34 24·27 25·21 26·14 27·07 28·01	7.53 7.88 8.24 8.60 8.96 9.32 9.68 10.03 10.39 10.75	19·57 20·50 21·44 22·37 23·30 24·23 25·16 26·10 27·03 27·96	7·61 7·97 8·34 8·70 9·06 9·42 9·79 10·15 10·51 10·87	19·54 20·47 21·40 22·33 23·26 24·19 25·12 26·05 26·98 27·91	7·70 8·06 8·43 8·80 9·16 9·53 9·90 10·26 10·63 11·00	19·50 20·43 21·36 22·29 23·22 24·15 25·08 26·01 26·94 27·86	7·78 8·15 8·52 8·89 9·63 10·01 10·38 10·75 11·12	21
~~~~~	31 32 33 34 35 36 37 38 39	28.94 29.87 30.81 31.74 32.68 33.61 34.54 35.48 36.41 37.34	11·11 11·47 11·83 12·18 12·54 12·90 13·26 13·62 13·98 14·33	28·89 29·82 30·76 31·69 32·62 33·55 34·48 35·42 36·35 37·28	11·24 11·60 11·96 12·32 12·69 13·05 13·41 13·77 14·14 14·50	28·84 29·77 30·70 31·63 32·56 33·50 34·43 35·36 36·29 37·22	11·36 11·73 12·09 12·46 12·83 13·19 13·56 13·93 14·29 14·66	28·79 29·72 30·65 31·58 32·51 33·44 34·37 35·29 36·22 37·15	11·49 11·86 12·23 12·60 12·97 13·34 13·71 14·08 14·45 14·82	31 32 33 34 35 36 37 38 39 40
	41 42 43 44 45 46 47 48 49	38·28 39·21 40·14 41·08 42·01 42·94 43·88 44·81 45·75 46·68	14·69 15·05 15·41 15·77 16·13 16·48 16·84 17·20 17·56 17·92	38·21 39·14 40·08 41·01 41·94 42·87 43·30 44·74 45·67 46·60	14·86 15·22 15·58 15·95 16·31 16·67 17·03 17·40 17·76 18·12	38·15 39·08 40·01 40·94 41·87 42·80 43·73 44·66 45·59 46·52	15·03 15·39 15·76 16·13 16·49 16·86 17·23 17·59 17·96 18·33	38·08 39·01 39·94 40·37 41·80 42·73 43·65 44·58 45·51 46·44	15·19 15·56 15·93 16·80 16·68 17·05 17·42 17·79 18·16 18·53	41 42 43 44 45 46 47 48 49 50
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Distance.	21 1	Deg.	211/4	Deg.	21½	Deg.	213/4	Deg.	Distance,
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	1се,
51	47·61	18·28	47·53	18·48	47·45	18·69	47·37	18·90	51
52	48·55	18·64	48·46	18·85	48·38	19·06	48·30	19·27	52
53	49·48	18·99	49·40	19·21	49·31	19·42	49·23	19·64	53
54	50·41	19·35	50·33	19·57	50·24	19·79	50·16	20·01	54
55	51·35	19·71	51·26	19·93	51·17	20·16	51·08	20·38	55
56	52·28	20·07	52·19	20·30	52·10	20·52	52·01	20·75	56
57	53·21	20·43	53·12	20·66	53·03	20·89	52·94	21·12	57
58	54·15	20·79	54·06	21·02	53·96	21·26	53·87	21·49	58
59	55·08	21·14	54·99	21·38	54·89	21·62	54·80	21·86	59
60	56·01	21·50	55·92	21·75	55·83	21·99	55·73	22·23	60
61	56·95	21·86	56·85	22·11	56·76	22·36	56.66	22·60	61
62	57·88	22·22	57·78	22·47	57·69	22·72	57.59	22·97	62
63	58·82	22·58	58·72	22·83	58·62	23·09	58.52	23·35	63
64	59·75	22·94	59·65	23·20	59·55	23·46	59.44	23·72	64
65	60·68	23·29	60·58	23·56	60·48	23·82	60.37	24·09	65
66	61·62	23·65	61·51	23·92	61·41	24·19	61.30	24·46	66
67	62·55	24·01	62·44	24·28	62·34	24·56	62.23	24·83	67
68	63·48	24·37	63·38	24·65	63·27	24·92	63.16	25·20	68
69	64·42	24·73	64·31	25·01	64·20	25·29	64.09	25·57	69
70	65·35	25·09	65·24	25·37	65·13	25·66	65.02	25·94	70
71	66·28	25·44	66·17	25·73	66.06	26·02	65.95	26·31	71
72	67·22	25·80	67·10	26·10	66.99	26·39	66.87	26·68	72
73	68·15	26·16	68·04	26·46	67.92	26·75	67.80	27·05	73
74	69·08	26·52	68·97	26·82	68.85	27·12	68.73	27·42	74
75	70·02	26·88	69·90	27·18	69.78	27·49	69.66	27·79	75
76	70·95	27·24	70·83	27·55	70.71	27·85	70.59	28·16	76
77	71·89	27·59	71·76	27·91	71.64	28·22	71.52	28·53	77
78	72·82	27·95	72·70	28·27	72.57	28·59	72.45	28·90	78
79	73·75	28·31	73·63	28·63	73.50	28·95	73.38	29·27	79
80	74·69	28·67	74·56	29·00	74.43	29·32	74.30	29·64	80
81 82 83 84 85 86 87 88 89	75·62 76·55 77·49 78·42 79·85 80·29 81·22 82·16 83·09 84·02	29·03 29·39 29·74 30·10 30·46 30·82 31·18 31·54 31·89 32·25	75·49 76·42 77·36 78·29 79·22 80·15 81·08 82·02 82·95 83·88	29·36 29·72 30·08 30·44 30·81 31·17 31·53 31·89 32·26 32·62	75·36 76·29 77·22 78·16 79·09 80·02 80·95 81·88 82·81 83·74	29·69 30·05 30·42 30·79 31·15 31·52 31·89 32·25 32·62 32·99	75·23 76·16 77·09 78·02 78·95 79·88 80·81 81·74 82·66 83·59	30·02 30·39 30·76 31·13 31·50 31·87 32·24 32·61 32·98 33·35	81 82 83 84 85 86 87 88 89 90
91	84·96	32·61	84·81	32·98	84·67	33·35	84·52	33·72	91
92	85·89	32·97	85·74	33·34	85·60	33·72	85·45	34·09	92
93	86·82	33·33	86·68	33·71	86·53	34·08	86·38	34·46	93
94	87·76	33·69	87·61	34·07	87·46	34·45	87·31	34·83	94
95	88·69	34·04	88·54	34·43	88·39	34·82	88·24	35·20	95
96	89·62	34·40	89·47	34·79	89·32	35·18	89·17	35·57	96
97	90·56	34·76	90·40	35·16	90·25	35·55	90·09	35·94	97
98	91·49	35·12	91·34	35·52	91·18	35·92	91·02	36·31	98
99	92·42	35·48	92·27	35·88	92·11	36·28	91·95	36·69	99
100	93·36	35·84	93·20	36·24	93·04	36·65	92·88	37·06	100
Distance.	Dep. 69	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.

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}	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ree.
	1 2 3 4 5 6 7 8 9	0·93 1·85 2·78 3·71 4·64 5·56 6·49 7·42 8·34 9.27	0·37 0·75 1·12 1·50 1·87 2·25 2·62 3·00 3·37 3·75	0.93 1.85 2.78 3.70 4.63 5.48 7.40 8.33 9.26	0·38 0·76 1·14 1·51 1·89 2·27 2·65 3·03 3·41 3·79	0.92 1.85 2.77 3.70 4.62 5.54 6.47 7.39 8.31 9.24	0·38 0·77 1·15 1·53 1·91 2·30 2·68 3·06 3·44 3·83	0.92 1.84 2.77 3.69 4.61 5.53 6.46 7.38 8.30 9.22	0·39 0·77 1·16 1·55 1·93 2·32 2·71 3·09 3·48 3·87	1 2 3 4 5 6 7 8 9
\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	11 12 13 14 15 16 17 18 19 20	10·20 11·13 12·05 12·98 13·91 14·83 15·76 16·69 17·62 18·54	4·12 4·50 4·87 5·24 5·62 5·99 6·37 6·74 7·12 7·49	10·18 11·11 12·03 12·96 13·88 14·81 15·73 16·66 17·59 18·51	4·17 4·54 4·92 5·30 5·68 6·06 6·44 6·82 7·19 7·57	10·16 11·09 12·01 12·93 13·86 14·78 15·71 16·63 17·55 18·48	4·21 4·59 4·97 5·36 5·74 6·12 6·51 6·89 7·27 7·65	10·14 11·07 11·99 12·91 13·83 14·76 15·68 16·60 17·52 18·44	4·25 4·64 5·03 5·41 5·80 6·19 6·57 6·96 7·35 7·73	11 12 13 14 15 16 17 18 19 20
	21 22 23 24 25 26 27 28 29 30	19·47 20·40 21·33 22·25 23·18 24·11 25·03 25·96 26·89 27·82	7·87 8·24 8·62 8·99 9·37 9·74 10·11 10·49 10·86 11·24	19·44 20·36 21·29 22·21 23·14 24·06 24·99 25·92 26·84 27·77	7.95 8.33 8.71 9.09 9.47 9.84 10.22 10.60 10.98 11.36	19·40 20·33 21·25 22·17 23·10 24·02 24·94 25·87 26·79 27·72	8·04 8·42 8·80 9·18 9·57 9·95 10·33 10·72 11·10 11·48	19·37 20·29· 21·21 22·13 23·05 23·98 24·90 25·82 26·74 27·67	8·12 8·51 8·89 9·28 9·67 10·05 10·44 10·83 11·21 11·60	21
***************************************	31 32 33 34 35 36 37 38 39 40	28·74 29·67 30·60 31·52 32·45 33·38 34·31 35·23 36·16 37·09	11.61 11.99 12.36 12.74 13.11 13.49 13.86 14.24 14.61 14.98	28·69 29·62 30·54 31·47 32·39 33·32 34·24 35·17 36·10 37·02	11·74 12·12 12·50 12·87 13·25 13·63 14·01 14·39 14·77 15·15	28·64 29·56 30·49 31·41 32·34 33·26 34·18 35·11 36·03 36·96	11·86 12·25 12·63 13·01 13·39 13·78 14·16 14·54 14·92 15·31	28·59 29·51 30·43 31·35 32·28 33·20 34·12 35·04 35·97 36·89	11.99 12.37 12.76 13.15 13.53 13.92 14.31 14.70 15.08 15.47	31 32 33 34 35 36 37 38 39 40
-	41 42 43 44 45 46 47 48 49 50	38·91 38·94 39·87 40·80 41·72 42·65 43·58 44·50 45·43 46·36 Dep.	15·36 15·73 16·11 16·48 16·86 17·23 17·61 17·98 18·36 18·73	37·95 38·87 39·80 40·72 41·65 42·57 43·50 44·43 45·35 46·28 Dep.	15·52 15·90 16·28 16·66 17·04 17·42 17·80 18·18 18·55 18·93	37.88 38.80 39.73 40.65 41.57 42.50 43.42 44.35 45.27 46.19 Dep.	15·69 16·07 16·46 16·84 17·22 17·60 17·99 18·37 18·75 19·13	37·81 38·73 39·65 40·58 41·50 42·42 43·34 44·27 45·19 46·11 Dep.	15·86 16·24 16·63 17·02 17·40 17·79 18·18 18·56 18·95 19·34 Lat.	41 42 43 44 45 46 47 48 49 50
}	Distance		Deg.		Deg.	1	Deg.	l	Deg.	Distance

$\sim\sim$	$\sim\sim$	$\sim\sim$	~~~	$\sim\sim$	$\sim\sim$	$\sim\sim$	$\sim\sim$	$\sim\sim$	$\sim$	٠,
Distance	22	Deg.	221/4	Deg.	221/2	Deg.	223/4	Deg.	Distanec.	}
) ree	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	sec.	{
$\begin{cases} -51 \\ 52 \end{cases}$	47·29 48·21	19·10 19·48	47·20 48·13	19·31 19·69	47·12 48·04	19·52 19·90	47·03 47·95	19·72 20·11	51 52	-
53	49.14	19.85	49.05	20.07	48.97	20.28	48.88	20.50	53	(
( 54	50.07	20.23	49.98	20.45	49.89	20.66	49.80	20.88	54	₹
55	51.00	20.60	50.90	20.83	50.81	21.05	50.72	21.27	55	(
56	51.92 52.85	20·98 21·35	51.83 52.76	21·20 21·58	51.74 52.66	21·43 21·81	51.64 52.57	21.66 22.04	56	7
57 58	53.78	21.73	53.68	21.96	53.59	22.20	53.49	22.43	57 58	7
59	54.70	22.10	54.61	22.34	54.51	22.58	54.41	22.82	59	(
60	55.63	22.48	55.53	22.72	55.43	22.96	55.33	23.20	60	ζ
61	56.56	22.85	56.47	23.10	56.36	23.34	56.25	23.59	61	{
62	57.49	23.23	57.38	23.48	57.28	23.73	57.18	23.98	62	?
63	58·41 59·34	23·60 23·97	58·31 59·23	$23.85 \\ 24.23$	58·20 59·13	24·11 24·49	58·10 59·02	24·36 24·75	63	?
64 65	60.27	24.35	60.16	24.61	60.05	24.87	59.94	25.14	64 65	?
66	61.19	24.72	61.09	24.99	60.98	25.26	60.87	25.52	66	?
( 67	62.12	25.10	62.01	25.37	61.90	25.64	61.79	25.91	67	>
68	63.05	25.47	62.94	25.75	62.82	26.02	62.71	26.30	68	)
69	63.98	25.85	63.86	26.13	63.75	26.41	63.63	26.68	69 70	$\rangle$
70	64.90	26.22	64.79	26.51	64.67	26.79	64.55	27.07	70	ζ
71	65.83	26.60	65.71	26.88	65.60	27.17	65.48	27.46	71	ζ
72	66.76	26.97	66.64	27·26 27·64	66·52 67·44	27.55	66·40 67·32	27·84 28·23	72	ς
5 73	67.68 68.61	27·35 27·72	67.56 68.49	28.02	68:37	27·94 28·32	68.24	28.62	73	ς
74 75	69.54	28.10	69.42	28.40	69.29	28.70	69.17	29.00	74 75	ς
76	70.47	28.47	70.34	28.78	70.21	29 08	70.09	29.39	76	ζ
77	71.39	28.84	71.27	29.16	71.14	29.47	71.01	29.78	77	Κ
78	72.32	29.22	72.19	29.53	72.06	29.85	71.93	30.16	77 78	ς
79	73.25	29.59	73.12	29.91	72.99	30.23	72.85	30.55	79	ζ
80	74 17	29.97	74.04	30.29	73.91	30.61	73.78	30.94	80	5
( 81	75.10	30.34	74.97	30.67	74.83	31.00	74.70	31.32	81	)
82	76.03	30.72	75.89	31.05	75.76	31.38	75.62	31.71	82	)
83	76.96	31.09	76.82	31.43	76.68	31.76	76.54	32.10	83	
84	77.88	31.47	77.75	31.81	77.61	32.15	77·46 78·39	32.48	84	->
85	78·81 79·74	31·84 32·22	78·67 79·60	32·19 32·56	78·53 79·45	32·53 32·91	79.31	32·87 33·26	85 86	$\rightarrow$
87	80.66	32.59	80.52	32.94	80.38	33.29	80.23	33.64	87	)
88	81.59	32.97	81.45	33.32	81.30	33.68	81.15	34.03	88	->
89	82.52	33.34	82.37	33.70	82.23	34.06	82.08	34.42	89	- >
\$ 90	83.45	33.71	83.30	34.08	83.15	34.44	83.00	34.80	90	>
91	84.37	34.09	84.22	34.46	84.07	34.82	83.92	35.19	91	3
92	85.30	34.46	85.15	34.84	85.00	35.21	84.84	35.58	92	(
93	86.23	34.84	86.08	35.21	85.92	35.59	85.76	35.96	93	(
5 94	87 16	35.21	87.00	35.59	86.84	35·97 36·35	86·69 87·61	36.35 36.74	94	(
95 96	88.08	35·59 35·96	87·93 88·85	35·97 36·35	87·77 88·69	36.74	88.53	37.12	96	(
90	89.94	36.34	89.78	36.73	89.62	37.12	89.45	37.51	97	(
98	90.86	36.71	90.70	37.11	90.54	37.50	90.38	37.90	98	(
99	91.79	37.09	91.63	37.49	91.46	37.89	91.30	38.28	99	(
5.100	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	100	(
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Distance.	68	Deg.	673/4	Deg.	671/9	Deg.	671/4	Deg.	Distance	(

{	$\left. \left. \left. \right\rangle \right. \right. $ Distance.	23	Deg.	231/4	Deg.	231/2	Deg.	233/4	Deg.	Distance
{	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
· · · · · · · · · · · · · · · · · · ·	1 2 3 4 5 6 7 8 9	0·92 1·84 2·76 3·68 4·60 5·52 6·44 7·36 8·28 9·20	0·39 0·78 1·17 1·56 1·95 2·34 2·74 3·13 3·52 3·91	0·92 1·84 2·76 3·68 4·59 5·51 6·43 7·35 8·27 9·19	0·39 0·79 1·18 1·58 1·97 2·37 2·76 3·16 3·55 3·95	0.92. 1.83 2.75 3.67 4.59 5.50 6.42 7.34 8.25 9.17	0·40 0·80 1·20 1·59 1·99 2·39 2·79 3·19 3·59 3·99	0.92 1.83 2.75 8.66 4.58 5.49 6.41 7.32 8.24 9.15	0·40 0·81 1·21 1·61 2·01 2·42 2·82 3·22 3·62 4·03	1 2 3 4 5 6 7 8 9 10 2
· · · · · · · · · · · · · · · · · · ·	11 12 13 14 15 16 17 18 19 20	10·13 11·05 11·97 12·89 13·81 14·73 15·65 16·57 17·49 18·41	4·30 4·69 5·08 5·47 5·86 6·25 6·64 7·03 7·42 7·81	10·11 11·03 11·94 12·86 13·78 14·70 15·62 16·54 17·46 18·38	4·34 4·74 5·13 5·53 5·92 6·32 6·71 7·11 7·50 7·89	10·09 11·00 11·92 12·84 13·76 14·67 15·59 16·51 17·42 18·34	4·39 4·78 5·18 5·58 5·98 6·38 6·78 7·18 7·58 7·97	$\begin{array}{c} 10.07 \\ 10.98 \\ 11.90 \\ 12.81 \\ 13.73 \\ 14.64 \\ 15.56 \\ 16.48 \\ 17.39 \\ 18.31 \end{array}$	4·43 4·83 5·24 5·64 6·04 6·44 6·85 7·25 7·65 8·05	11 12 13 14 15 16 17 18 19 20 4
***************************************	21 22 23 24 25 26 27 28 29 30	19·33 20·25 21·17 22·09 23·01 23·93 24·85 25·77 26·69 27·62	8·21 8·60 8·99 9·38 9·77 10·16 10·55 10·94 11·33 11·72	19·29 20·21 21·13 22·05 22·97 23·89 24·81 25·73 26·64 27·56	8·29 8·68 9·08 9·47 9·87 10·26 10·66 11·05 11·45 11·84	19·26 20·18 21·09 22·01 22·93 23·84 24·76 25·68 26·59 27·51	8·37 8·77 9·17 9·57 9·97 10·37 10·77 11·16 11·56 11·96	$\begin{array}{c} 19 \cdot 22 \\ 20 \cdot 14 \\ 21 \cdot 05 \\ 21 \cdot 97 \\ 22 \cdot 88 \\ 23 \cdot 80 \\ 24 \cdot 71 \\ 25 \cdot 63 \\ 26 \cdot 54 \\ 27 \cdot 46 \end{array}$	8:46 8:86 9:26 9:67 10:07 10:47 10:87 11:28 11:68 12:08	21 22 23 24 25 26 27 28 29 30 30
~~~~~	31 32 33 34 35 36 37 38 39 40	28·54 29·46 30·38 31·30 32·22 33·14 34·06 34·98 35·90 36·82	12·11 12·50 12·89 13·28 13·68 14·07 14·46 14·85 15·24 15·63	28·48 29·40 30·32 31·24 32·16 33·08 34·00 34·91 35·83 36·75	12·24 12·63 13·03 13·42 13·42 14·21 14·61 15·00 15·39 15·79	28·43 29·35 30·26 31·18 32·10 33·01 33·93 34·85 35·77 36·68	12·36 12·76 13·16 13·56 13·56 14·35 14·75 15·15 15·55 15·95	28·37 29·29 30·21 31·12 32·04 32·95 33·87 34·78 35·70 36·61	12·49 12·89 13·29 13·69 14·10 14·50 14·90 15·30 15·71 16.11	31 32 33 34 35 36 37 38 39 40
	41 42 43 44 45 46 47 48 49 50	37·74 38·66 39·58 40·50 41·42 42·34 43·26 44·18 45·10 46·03	16.02 $16.41$ $16.80$ $17.19$ $17.58$ $17.97$ $18.36$ $18.76$ $19.15$	37·67 38·59 39·51 40·43 41·35 42·26 43·18 44·10 45·02 45·94	16·18 16·58 16·97 17·37 17·76 18·16 18·55 18·95 19·34 19·74	37·60 38·52 39·43 40·35 41·27 42·18 43·10 44·02 44·94 45·85	16:35 16:75 17:15 17:54 17:94 18:34 18:74 19:14 19:54 19:94	37·53 38·44 39·36 40·27 41·19 42·10 43·02 43·93 44·85 45·77	16·51 16·92 17·32 17·72 18·12 18·53 18·93 19·33 19·73 20·14	41 42 43 44 45 46 47 48 49 50
~	Distance.	67	Deg.	Dep. 663/4	Deg.	Dep. 66½	Lat.	Dep. 661/4	Lat.	Distance.

Distance	23	Deg.	231/4	Deg.	23½	Deg.	233/4	Deg.	Distance
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51	46·95	19·93	46·86	20·13	46·77	20·34	46.68	20·54	51
52	47·87	20·32	47·78	20·53	47·69	20·73	47.60	20·94	52
53	48·79	20·71	48·70	20·92	48·60	21·13	48.51	21·35	53
54	49·71	21·10	49·61	21·32	49·52	21·53	49.43	21·75	54
55	50·63	21·49	50·53	21·71	50·44	21·93	50.34	22·15	55
56	51·55	21·88	51·45	22·11	51·36	22·93	51.26	22·55	56
57	52·47	22·27	52·37	22·50	52·27	22·73	52.17	22·96	57
58	53·39	22·66	53·29	22·90	53·19	23·13	53.09	23·36	58
59	54·31	23·05	54·21	23·29	54·11	23·53	54.00	23·76	59
60	55·23	23·44	55·13	23·68	55·02	23·92	54.92	24·16	60
61	56·15	23·83	56·05	24·08	55.94	24·32	55·83	24·57	61
62	57·07	24·23	56·97	24·47	56.86	24·72	56·75	24·97	62
63	57·99	24·62	57·88	24·87	57.77	25·12	57·66	25·37	63
64	58·91	25·01	58·80	25·26	58.69	25·52	58·58	25·78	64
65	59·83	25·40	59·72	25·66	59.61	25·92	59·50	26·18	65
66	60·75	25·79	60·64	26·05	60.53	26·32	60·41	26·58	66
67	61·67	26·18	61·56	26·45	61.44	26·72	61·33	26·98	67
68	62·59	26·57	62·48	26·84	62.36	27·11	62·24	27·39	68
69	63·51	26·96	63·40	27·24	63.28	27·51	63·16	27·79	69
70	64·44	27·35	64·32	27·63	64.19	27·91	64·07	28·19	70
71	65:36	27·74	65·23	28·03	65·11	28·31	64·99	28·59	71
72	66:28	28·13	66·15	28·42	66·03	28·71	65·90	29·00	72
73	67:20	28·52	67·07	28·82	66·95	29·11	66·82	29·40	73
74	68:12	28·91	67·99	29·21	67·86	29·51	67·73	29·80	74
75	69:04	29·30	68·91	29·61	68·78	29·91	68·65	30·21	75
76	69:96	29·70	69·83	30·00	69·70	30·30	69·56	30·61	76
77	70:88	30·09	70·75	30·40	70·61	30·70	70·48	31·01	77
78	71:80	30·48	71·67	30·79	71·53	31·10	71·39	31·41	78
79	72:72	30·87	72·58	31·18	72·45	31·50	72·31	31·82	79
80	73:64	31·26	73·50	31·58	73·36	31·90	73·22	32·22	80
81	74·56	31·65	74·42	31·97	74·28	32·30	74·14	32·62	81 82 83 84 85 86 87 88 89 90 8
82	75·48	32·04	75·34	32·37	75·20	32·70	75·06	33·03	
83	76·40	32·43	76·26	32·76	76·12	33·10	75·97	33·43	
84	77·32	32·82	77·18	33·16	77·03	33·49	76·89	33·83	
85	78·24	33·21	78·10	33·55	77·95	33·89	77·80	34·23	
86	79·16	33·60	79·02	33·95	78·87	34·29	78·72	34·64	
87	80·08	23·99	79·93	34·34	79·78	34·69	79·63	35·04	
88	81·00	34·38	S0·85	34·74	80·70	35·09	80·55	35·44	
89	81·92	34·78	81·77	35·13	81·62	35·49	81·46	35·84	
90	82·85	35·17	82·69	35·53	82·54	35·89	82:38	36·25	
91 92 93 94 95 96 97 98 99 100	83·77 84·69 85·61 86·53 87·45 88·37 89·29 90·21 91·13 92·05	35·56 35·95 36·34 36·73 37·12 37·51 37·90 38·29 38·68 39·07	83·61 84·53 85·45 86·37 87·29 88·20 89·12 90·04 90·96 91·88	35·92 36·32 36·71 37·11 37·50 37·90 38·29 38·68 39·08 39·47	83·45 84·37 85·29 86·20 87·12 88·04 88·95 89·87 90·79 91·71	36·29 36·68 37·08 37·48 37·88 38·28 38·68 39·48 39·48	83·29 84·21 85·12 86·04 86·95 87·87 88·79 89·70 90·62 91·53	36·65 37·05 37·46 37·86 38·26 38·66 39·07 39·47 39·47 40·27	91 92 93 94 95 96 97 98 99 100
Distance.	Dep. 67	Lat.	Dep. 663/4	Lat.	Dep. 66½	Lat.	Dep. 661/4	Lat. Deg.	Distance.

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{	$\langle$ Distance	24 I	Deg.	241/4	Deg.	24½	Deg.	243/4	Deg.	$\left. \left\{ \begin{array}{l} \text{Distance.} \end{array} \right. \right.$	}
3	ace.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ice.	}
	1 2 3 4 5 6 7 8 9	0·91 1·83 2·74 3·65 4·57 5·48 6·39 7·31 8·22 9·14	0·41 0·81 1·22 1·63 2·03 2·44 2·85 3·25 3·66 4·07	0·91 1·82 2·74 3·65 4·56 5·47 6·38 7·29 8·21 9·12	0·41 0·82 1·23 1·64 2·05 2·46 2·87 3·29 3·70 4·11	0·91 1·82 2·73 3·64 4·55 5·46 6·37 7·28 8·19 9·10	0·41 0·83 1·24 1·66 2·07 2·49 2·90 3·32 3·73 4·15	0·91 1·82 2·72 3·63 4·54 5·45 6·36 7·27 8·17 9·08	0·42 0·84 1·26 1·67 2·09 2·51 2·93 3·35 3·77 4·19	1 2 3 4 5 6 7 8 9	
	11 12 13 14 15 16 17 18 19 20	10·05 10·96 11·88 12·79 13·70 14·62 15·53 16·44 17·36 18·27	4·47 4·88 5·29 5·69 6·10 6·51 6·92 7·32 7·73 8·13	10·03 10·94 11·85 12·76 13·68 14·59 15·50 16·41 17·32 18·24	4·52 4·93 5·34 5·75 6·16 6·57 6·98 7·39 7·80 8·21	10·01 10·92 11·83 12·74 13·65 14·56 15·47 16·38 17·29 18·20	4·56 4·98 5·39 5·81 6·22 6·64 7·05 7·46 7·88 8·29	9·99 10·90 11·81 12·71 13·62 14·53 15·44 16·35 17·25 18·16	4·61 5·02 5·44 5·86 6·28 6·70 7·12 7·54 7·95 8·37	11 12 13 14 15 16 17 18 19 20	
:	21 22 23 24 25 26 27 28 29 30	19·18 20·10 21·01 21·93 22·84 23·75 24·67 25·58 26·49 27·41	8·54 8·95 9·35 9·76 10·17 10·58 10·98 11·39 11·80 12·20	19·15 20·06 20·97 21·88 22·79 23·71 24·62 25·53 26·44 27·35	8.63 9.04 9.45 9.86 10.27 10.68 11.09 11.50 11.91 12.32	19·11 20·02 20·93 21·84 22·75 23·66 24·57 25·48 26·89 27·80	8·71: 9·12 9·54 9·95 10·37 10·78 11·20 11·61 12·03 12·44	19·07 19·98 20·89 21·80 22·70 23·61 24·52 25·43 26·34 27·24	$\begin{array}{c} 8.79 \\ 9.21 \\ 9.63 \\ 10.05 \\ 10.47 \\ 10.89 \\ 11.30 \\ 11.72 \\ 12.14 \\ 12.56 \end{array}$	21 22 23 24 25 26 27 28 29 30	
~~~~~	31 32 33 34 35 36 37 38 39 40	28·32 29·23 30·15 31·06 31·97 32·89 33·80 34·71 35·63 36·54	12·61 13·02 13·42 13·83 14·24 14·64 15·05 15·46 15·86 16·27	28·26 29·18 30·09 31·00 31·91 32·82 33·74 34·65 35·56 36·47	12·73 13·14 13·55 13·96 14·38 14·79 15·20 15·61 16·02 16·43	28·21 29·12 30·03 30·94 31·85 32·76 33·67 34·58 35·49 36·40	12·86 13·27 13·68 14·10 14·51 14·93 15·34 15·76 16·17 16·59	28·15 29·06 29·97 30·88 31·78 32·69 33·60 34·51 35·42 36·33	12-98 13-40 13-82 14-23 14-65 15-07 15-49 15-91 16-33 16-75	31 32 33 34 35 36 37 38 39 40	
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~~~	Distance'		Deg.	<u> </u>	Deg.	651	2 Deg.	1	4 Deg.	Distance	}

Distance	24 1	Deg.	241/4	Deg.	24½	Deg.	243/4	Deg.	$\left. \left. \left. \right\rangle \right\rangle \right\rangle $ Distance
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ē. {
51 52 53 54 55 56 57 58 59 60	46·59 47·50 48·42 49·33 50·24 51·16 52·07 52·99 53·90 54·81	20·74 21·15 21·56 21·96 22·37 22·78 23·18 23·59 24·00 24·40	46·50 47·41 48·32 49·24 50·15 51·06 51·97 52·88 53·79 54·71	20·95 21·36 21·77 22·18 22·59 23·00 23·41 23·82 24·23 24·64	46·41 47·32 48·23 49·14 50·05 50·96 51·87 52·78 53·69 54·60	21·15 21·56 21·98 22·39 22·81 23·22 23·64 24·05 24·47 24·88	46·32 47·22 48·13 49·04 49·95 50·86 51·76 52·67 53·58 54·49	21·35 21·77 22·19 22·61 23·03 23·44 23·86 24·28 24·70 25·12	51
61 62 63 64 65 66 67 68 69 70	55·73 56·64 57·55 58·47 59·38 60·29 61·21 62·12 63·03 63·95	24·81 25·22 25·62 26·03 26·44 26·84 27·25 27·66 28·06 28·47	55·62 56·53 57·44 58·35 59·26 60·18 61·09 62·00 62·91 63·82	25·05 25·46 25·88 26·29 26·70 27·11 27·52 27·93 28·34 28·75	55·51 56·42 57·33 58·24 59·15 60·06 60·97 61·88 62·79 63·70	25·30 25·71 26·13 26·54 26·96 27·37 27·78 28·20 28·61 29·03	55·40 56·30 57·21 58·12 59·03 59·94 60·85 61·75 62·66 63·57	25·54 25·96 26·38 26·79 27·21 27·63 28·05 28·47 28·89 29·31	61 62 63 64 65 66 67 68 69 70
71   72   73   74   75   76   77   78   79   80	64:86 65:78 66:69 67:60 68:52 69:43 70:34 71:26 72:17 73:08	28·88 29·28 29·69 30·10 30·51 30·91 31·32 31·73 32·13 32·54	64·74 65·65 66·56 67·47 68·38 69·29 70·21 71·12 72·03 72·94	29·16 29·57 29·98 30·39 30·80 31·21 31·63 32·04 32·45 32·86	64·61 65·52 66·43 67·34 68·25 69·16 70·07 70·98 71·89 72·80	29·44 29·86 30·27 30·69 31·10 31·52 31·93 32·35 32·76 33·18	64·48 65·39 66·29 67·20 68·11 69·02 69·93 70·84 71·74 72·65	29·72 30·14 30·56 30·98 31·40 31·82 32·24 32·66 33·07 33·49	71 72 73 74 75 76 77 78 79 80
81 82 83 84 85 85 86 87 88 89 90	74·00 74·91 75·82 76·74 77·65 78·56 79·48 80·39 81·31 82·22	32·95 33:35 33·76 34·17 34·57 34·98 35·39 35·79 36·20 36·61	73·85 74·76 75·68 76·59 77·50 78·41 79·32 80·24 81·15 82·06	33·27 33·68 34·09 34·50 34·91 35·32 35·73 36·14 36·55 36·96	73·71 74·62 75·53 76·44 77·35 78·26 79·17 80·08 80·99 81·90	33·59 34·00 34·42 34·83 35·25 35·66 36·08 36·49 36·91 37·32	73·56 74·47 75·38 76·28 77·19 78·10 79·01 79·92 80·82 81·73	33.91 34.33 34.75 35.17 35.59 36.00 36.42 36.84 37.26 37.68	81 82 83 84 85 86 87 88 89 90
91 92 93 94 95 96 97 98 99 100	83·13 84·05 84·96 85·87 86·79 87·70 88·61 89·53 90·44 91·35	37·01 37·42 37·83 38·23 38·64 39·05 59·45 39·86 40·27 40·67	82:97 83:88 84:79 85:71 86:62 87:53 88:44 89:35 90:26 91:18	37·38 37·79 38·20 38·61 39·02 39·43 39·84 40·25 40·66 41·07	82:81 83:72 84:63 85:54 86:45 87:36 88:27 89:18 90:09 91:00	37·74 38·15 38·57 38·98 39·40 39·81 40·23 40·64 41·05 41·47 Lat.	82·64 83·55 84·46 85·37 86·27 87·18 88·09 89·90 89·91 90·81 Dep.	38·10 38·52 38·94 39·35 39·77 40·19 40·61 41·03 41·45 41·87	91 92 93 94 95 96 97 98 99 100
Distance	Dep. 66	Deg.	Dep. 653/	Lat.	65 <sup>1</sup> / <sub>2</sub>	Z Deg.	1	Deg.	Distance

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0-91 0-42 0-90 0-43 0-90 0-43 0-90 0-43 1 1-81 0-85 1-81 0-85 1-81 0-86 1-80 0-87 2 2-72 1-27 1-72 2-71 1-28 2-71 1-29 2-70 1-30 3 3-63 1-69 3-62 1-71 3-61 1-72 3-60 1-74 4 4-53 2-11 4-52 2-13 4-51 2-15 4-50 2-17 5 5-544 2-54 5-43 2-56 5-42 2-58 5-49 2-61 6-6 6-34 2-96 6-33 2-99 6-32 3-01 6-30 3-04 7 7-25 3-38 7-24 3-41 7-22 3-44 7-21 3-48 8 5-16 3-80 8-14 3-84 8-12 3-87 8-11 3-91 9 9-06 4-23 9-04 4-27 9-03 4-31 9-01 4-34 10 9-97 4-65 9-95 4-69 9-93 4-74 9-91 4-78 11 10-88 5-07 10-85 5-12 10-83 5-17 10-81 5-21 12-11 11-78 5-49 11-76 5-55 11-73 5-60 11-71 5-65 13 12-60 5-92 12-66 5-97 12-64 6-03 12-61 6-08 14 13-59 6-34 13-57 6-40 13-54 6-46 13-51 6-52 15 14-50 6-76 14-47 6-83 14-44 6-89 14-41 6-95 16 14-50 6-76 14-47 6-83 14-44 6-89 14-41 6-95 16 15-41 7-18 15-38 7-25 15-34 7-32 15-31 7-39 17 16-31 7-61 16-28 7-63 16-25 7-75 16-21 7-82 18 17-22 8-03 17-13 8-10 17-15 8-18 17-11 8-25 19 19-03 8-87 18-99 8-96 18-95 9-04 18-91 9-12 21 19-94 9-30 19-90 9-38 19-86 9-47 19-82 9-56 22 20-85 9-72 20-80 9-81 20-76 9-90 20-72 9-99 23 21-75 10-14 21-71 10-24 21-66 10-33 21-62 10-43 24 22-66 10-57 22-61 10-66 22-56 10-76 25-52 10-86 25 23-719 12-68 27-13 12-80 27-78 13-35 9-22 13-30 30 28-10 13-10 28-04 13-52 27-98 13-35 27-92 13-47 31 28-90 13-50 28-04 13-52 27-98 13-35 28-92 13-90 32 28-90 13-50 28-04 13-62 22 27-98 13-35 28-92 13-90 32 28-90 13-50 28-04 13-62 22 27-98 13-35 28-92 13-90 33 28-90 13-50 28-04 13-62 28-88 13-78 28-82 13-90 38 28-90 13-50 28-04 13-62 28-88 13-78 28-82 13-90 38 28-90 13-50 28-04 13-62 28-88 13-78 28-82 13-90 38 28-90 13-50 28-04 13-62 28-88 13-78 28-82 13-90 38 28-90 13-50 28-04 13-62 28-88 13-78 28-82 13-90 38	34 35 36 37 38 39 40 41 42 43 44 44 44 44 44 44 44 44 45 46 47 48 49 50 60 60 60 60 60 60 60 60 60 60 60 60 60	31 32 33	21 22 23 24 25 26 27 28 29 30	11 12 13 14 15 16 17 18 19 20	$\begin{bmatrix} 2\\3\\4 \end{bmatrix}$	ance.
0-42	30·81 31·72 32·63 38·53 34·44 35·35 36·25 37·16 38·96 38·96 38·97 40·78 41·69 42·60 44·41 45·32 Dep.		19·94 20·85 21·75 22·66 23·56 24·47 25·38	10·88 11·78 12·69 13·59 14·50 15·41 16·31 17·22	1·81 2·72 3·63 4·53 5·44 6·34 7·25 8·16	
0-90	14-37 14-79 15-21 15-64 16-06 16-48 16-90 17-33 17-75 18-10 19-02 19-44 19-82 20-21 20-71 21-13	13.52	9·30 9·72 10·14 10·57 10·99 11·41 11·83	5·07 5·49 5·92 6·34 6·76 7·18 7·61 8·03	0.85 1.27 1.69 2.11 2.54 2.96 3.38 3.80	
0-43	29 85 30 75 8 31 66 32 56 33 46 34 37 36 18 37 08 37 99 38 89 40 70 41 60 42 51 43 41 44 32 45 22 Dep.	28.94	19·90 20·80 21·71 22·61 23·52 24·42 25·32	10.85 11.76 12.66 13.57 14.47 15.38 16.28 17.18	1.81 2.71 3.62 4.52 5.43 6.33 7.24 8.14	
0-90 0-43 0-90 0-43 1 1-81 0-86 1-80 0-87 2 2-71 1-29 2-70 1-30 3 3-61 1-72 3-60 1-74 4 4-51 2-15 4-50 2-17 5 5-42 2-58 5-49 2-61 6 6-32 3-01 6-30 3-04 7 7-22 3-44 7-21 3-48 8 8-12 3-87 8-11 3-91 9 9-03 4-31 9-01 4-34 10 9-93 4-74 9-91 4-78 11 10-83 5-17 10-81 5-21 12 11-73 5-00 11-71 5-65 13 12-64 6-03 12-61 6-08 14 13-54 6-46 13-51 6-52 15 14-44 6-89 14-41 6-95 16 15-34 7-32 15-31 7-39 17 16-25 7-75 16-21 7-82 18 17-15 8-18 17-11 8-25 19 18-95 9-04 18-91 9-12 21 19-86 9-47 19-82 9-56 22 20-76 9-90 20-72 9-99 23 18-95 9-04 18-91 9-12 21 19-86 9-47 19-82 9-56 22 20-76 9-90 20-72 9-99 23 21-66 10-33 21-62 10-43 24 22-56 10-76 22-52 10-86 25 23-47 11-19 23-42 11-30 26 24-37 11-62 24-32 11-73 27 25-27 12-05 25-22 12-16 28 24-78 11-62 24-32 11-73 27 25-27 12-05 25-22 12-16 29 27-98 12-92 27-02 13-03 30 27-98 13-35 27-92 13-47 31 28-88 13-78 28-88 13-90 32	14·08 14·93 15·36 15·78 16·21 16·64 17·06 17·49 17·92 18·34 18·77 19·20 19·62 20·05 20·48 20·90 21·33	13.65	9·38 9·81 10·24 10·66 11·09 11·52 11·94 12·37	5·12 5·55 5·97 6·40 6·83 7·25 7·68 8·10	0·85 1·28 1·71 2·13 2·56 2·99 3·41 3·84	
0-43	29·79 30·69 31·59 32·49 33·40 35·20 36·10 37·01 37·91 38·81 39·71 40·62 41·52 42·42 44·23 45·13 Dep.	28.88	19·86 20·76 21·66 22·56 23·47 24·37 25·27 26·17	10·83 11·73 12·64 13·54 14·44 15·34 16·25 17·15	1·81 2·71 3·61 4·51 5·42 6·32 7·22 8·12	
0-90 0-43 1 1-80 0-87 2 2-70 1-30 3 3-60 1-74 4 4-50 2-17 5 5-49 2-61 6 6-30 3-04 7 7-21 3-48 8 8-11 3-91 9 9-01 4-34 10 9-91 4-78 11 10-81 5-21 12 11-71 5-65 13 12-61 6-98 14 13-51 7-39 17 16-21 7-82 18 17-11 8-25 19 18-01 8-95 16 15-31 7-39 17 16-21 7-82 18 17-11 8-25 19 18-01 8-95 69 20 20-72 9-99 23 12-62 10-43 24 22-52 10-86 25 23-42 11-30 26 24-32 11-73 27 25-22 12-16 28 24-23 11-73 27 25-22 12-16 28 24-23 11-73 27 25-22 12-16 28 24-23 11-73 27 25-22 12-16 28 24-32 11-73 30 27-92 13-93 30	14-21 14-64 15-07 15-50 15-93 16-36 16-79 17-22 17-65 18-08 18-51 18-94 19-37 19-80 20-23 20-66 21-10 21-53	13.78	9.47 9.90 10.33 10.76 11.19 11.62 12.05 12.48	5·17 5-60 6·03 6·46 6·89 7·32 7·75 8·18	0·86 1·29 1·72 2·15 2·58 3·01 3·44 3·87	
0.43 1 0.87 2 1.30 3 1.74 4 2.17 5 2.61 6 3.04 7 3.48 8 3.91 9 4.34 10 4.78 11 5.21 12 5.66 13 6.08 14 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15 6.52 15	297 (2 30-62 31-52 32-43 33-33 34-23 35-13 36-03 37-83 38-73 39-63 40-53 41-43 42-33 44-13 45-03 Dep.	28.82	19·82 20·72 21·62 22·52 23·42 24·32 25·22 26·12	10·81 11·71 12·61 13·51 14·41 15·31 16·21 17·11	1·80 2·70 3·60 4·50 5·40 6·30 7·21 8·11	
1 2 3 4 5 6 7 8 9 10 11 12 3 14 4 15 6 17 18 19 20 21 22 23 24 25 29 30 20 20 20 20 20 20 20 20 20 20 20 20 20	14:34 14:71 15:64 16:07 16:51 16:94 17:38 17:81 18:25 18:68 19:12 19:55 19:98 20:42 20:85 21:29 21:72	13.90	9.56 9.99 10.43 10.86 11.30 11.73 12.16 12.60	5·21 5·65 6·08 6·52 6·95 7·39 7·82 8·25	0·87 1·30 1·74 2·17 2·61 3·04 3·48 3·91	
	0345 637 839 40 4142 444 445 445 45 45 45 45 45 45 45 45 45	32	22 23 24 25 26 27 28 29	12 13 14 15 16 17 18 19	9	Distance.

Distance	25 1	Deg.	$25\frac{1}{4}$	Deg.	$25\frac{1}{2}$	Deg.	253/4	Deg.	Distance
\$ 8	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ice.
$\begin{array}{c} 51 \\ 52 \end{array}$	46·22 47·13	21·55 21·98	46·13 47·03	21·75 22·18	46.03 46.93	21·96 22·39	45·94 46·84	22·16 22·59	51 52
> 53	48.03	22.40	47.94	22.61	47.84	22.82	47.74	23.03	53
54	48.94	22.82	48.84	23.03	48.74	23.25	48.64	23.46	54
55	49.85	23.24	49.74	23.46	49.64	23.68	49.54	23.89	55
56	50.75	23.67 $24.09$	50.65	$23.89 \\ 24.31$	50.54	24·11 24·54	50·44 51·34	24·33 24·76	56
57	51.66 52.57	$\frac{24.09}{24.51}$	51·55 52·46	24.74	51·45 . 52·35	24.97	52.24	25.20	57 ( 58 (
$\begin{cases} 58 \\ 59 \end{cases}$	53.47	24.93	53.36	25.17	53.25	25:40	53.14	25.63	59 (
60	54.38	25.36	54.27	25.59	54.16	25:83	54.04	26.07	60
61	55.28	25.78	55.17	26 02	55.06	26.26	54.94	26.50	61
62	56.19	26.20	56.08	26.45	55.96	26.69	55.84	26.94	62
63	57.10	26.62	56.98	26.87	56.86	27:12	56.74	27:37	63 (
64	58.00	27.05	57·89 58·79	27·30 27·73	57.77	27·55 27·98	57.64 58.55	27.80	64 (
65	58·91 59·82	27·47 27·89	59.69	28.15	58·67 59·57	28.41	59.45	28·24 28·67	65 ( 66 /
67	60.72	28.32	60.60	28.58	60.47	28.84	60.35	29.11	67
68	61.63	28.74	61.50	29.01	61.38	29.27	61.25	29.54	68
69	62.54	29.16	62.41	29.43	62.28	29.71	62.15	29.98	69
5 70	63.44	29.58	63.31	29.86	63.18	30.14	63.05	30.41	70
71	64.35	30.01	64.22	30.29	64.08	30.57	63.95	30.85	71
72	65.25	30.43	65.12	30.71	64.99	31.00	64.85	31.28	72
73	66.16	30.85	66.03	31.14	65.89	31.43	65.75	31.71	$\frac{73}{74}$
$\begin{cases} 74 \\ 75 \end{cases}$	67·07 67·97	31·27 31·70	66·93 67·83	31·57 31·99	66.79	31·86 32·29	66·65 67·55	32·15 32·58	75
ζ 76 I	68.88	32.12	68.74	32.42	68.60	32.72	68.45	33.02	76
77	69.79	32.54	69.64	32.85	69.50	33.15	69.35	33.45	77
78	70.69	32.96	70.55	33.27	70.40	33.58	70.25	33.89	78
( 79	71.60	33.39	71.45	33.70	71.30	34.01	71.16	34.32	79 ,
3 80	72.50	33 81	72.36	34.13	72.21	34.44	72.06	34.76	80
81	73.41	34.23	73.26	34.55	73.11	34.87	72.96	35.19	81 82
82	74.32	34.65	74.17	34.98	74.01	35.30	73.86	35.62	83
83	75.22	35.08	75.07	35.41	74.91	35·73 36·16	$74.76 \\ 75.66$	36.06	84
84	76·13 77·04	35·50 35·92	75·97 76·88	35·83 36·26	75·82 76·72	36.29	78.56	36·49 36·93	85
86	77.9±	36.35	77.78	36.68	77.62	37.02	77.46	37.36	86
87	78.85	36.77	78.69	37.11	78.52	37.45	78.36	37.80	87
88	79.76	37.19	79.59	37.54	79.48	37.88	79.26	38.23	88
89	80.66	37.61	80.50	37.96	80.33	38.32	80.16	38.67	89
90	81.57	38.04	81.40	38-39	81.23	38.75	81.06	39.10	90
91	82.47	38.46	82.31	38.82	82.14	39.18	81.96	39.53	91
92	83.38	38.88	83.21	39.24	83.04	39.61	82.86	39.97	92
2. 93	84.29	39.30	84.11	39.67	83.94	40.04	83.76	40.40	93
94	85.19	39.73	85.02	40.10	84.84	40.47	84.67	40.84	94
95	86.10	40.15	85.92	40.52	85.75	40.90	85.57	41.27	95 96
96	87.01	40.57	86·83 87·73	40.95 41.38	86·65 87·55	41.33	86·47 87·37	41·71 42·14	96
98	87·91 88·82	40.99 41.42	88.64	41.80	88.45	42.19	88.27	42.14	98
99	89.72	41.84	89.54	42.23	89.36	42.62	89.17	43.01	99
100	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	100
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Distance.	26	Deg.	261/4	Deg.	261/2	Deg.	263/4	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.;	nce.
1 2 3 4 5 6 7 8 9 10	0·90 1·80 2·70 3·60 4·49 5·30 6·29 7·19 8·09	0.44 0.88 1.32 1.75 2.19 2.63 3.07 3.51 3.95 4.38	0.90 1.79 2.69 3.59 4.48 5.38 6.28 7.17 8.07 8.97	0·44 0·88 1·33 1·77 2·21 2·65 3·10 3·54 3·98 4·42	0·89 1·79 2·68 3·58 4·47 5·37 6·26 7·16 8·05 8·95	0·45 0·89 1·34 1·78 2·23 2·68 3·12 3·57 4·02 4·46	0·89 1·79 2·68 3·57 4·46 5·36 6·25 7·14 8·04 8·93	0·45 0·90 1·35 1·80 2·25 2·70 3·15 3·60 4·05 4·50	1 2 3 4 5 6 7 8 9 10 }
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	9·89 10·79 11·68 12·58 13·48 14·38 15·28 16·18 17·08	4·82 5·26 5·70 6·14 6·58 7·01 7·45 7·89 8·33 8·77	9·87 10·76 11·66 12·56 13·45 14·35 15·25 16·14 17·04 17·94	4·87 5·31 5·75 6·19 6·63 7·08 7·52 7·96 8·40 8·85	9·84 10·74 11·63 12·53 13·42 14·32 15·21 16·11 17·00 17·90	4·91 5·35 5·80 6·25 6·69 7·14 7·59 8·03 8·48 8·92	9·82 10·72 11·61 12·50 13·39 14·29 15·18 16·07 16·97 17·86	4.95 5.40 5.85 6.30 6.75 7.20 7.65 8.10 8.55 9.00	11
21 22 23 24 25 26 27 28 29 30	18·87 19·77 20·67 21·57 22·47 23·37 24·27 25·17 26·06 26·96		18·83 19·73 20·63 21·52 22·42 23·32 24·22 25·11 26·01 26·91	9·29 9·73 10·17 10·61 11·06 11·50 11·94 12·38 12·83 13·27	18·79 19·69 20·58 21·48 22·37 23·27 24·16 25·06 25·95 26·85	9·37 9·82 10·26 10·71 .11·15 11·60 12·05 12·49 12·94 13·39	18·75 19·65 20·54 21·43 22·32 23·22 24·11 25·00 25·90 26·79	9·45 9·90 10·35 10·80 11·25 11·70 12·15 12·60 13·05 13·50;	21
31 32 33 34 35 36 37 38 39 40	29·66 30·56 31·46 32·36 33·26 34·15 35·06	14·03 14·47 14·90 15·34 15·78 16·22 16·66 17·10	27·80 28·70 29·60 30·49 31·39 32·29 33·18 34·08 34·98 35·87	13·71 14·15 14·60 15·04 15·48 15·92 16·36 16·81 17·25 17·69	27·74 28·64 29·53 30·43 31·32 32·22 33·11 34·01 34·90 35·80	13·83 14·28 14·72 15·17 15·62 16·06 16·51 16·96 17·40 17·85	27.68 28.58 29.47 30.36 31.25 32.15 33.04 33.93 34.83 35.72	13.95 14.40 14.85 15.30 15.75 16.20 16.65 17.10 17.55 18.00	81 32 33 34 35 36 37 38 39 40
41 42 43 44 44 44 45 45 45 45	2 37·78 38·63 40·44 36 41·3 7 42·2 8 43·1 9 44·0	5 18·41 18·85 19·29 19·73 4 20·17 4 20·60 4 21·04 4 21·48	36·77 37·67 38·57 39·46 40·36 41·26 42·15 43·05 43·95 44·84	18·13 18·58 19·02 19·46 19·90 20·35 20·79 21·23 21·67 22·11	36·69 37·59 38·48 39·38 40·27 41·17 42·06 42·96 43·85 44·75	18·29 18·74 19·19 19·63 20·08 20·53 20·97 21·42 21·86 22·31	36·61 37·51 38·40 39·29 40·18 41·08 41·97 42·86 43·76 44·65	18·45] 18·90 19·35 19·80 20·25 20·70 21·15 21·60 22·05 22·50	41 42 43 44 45 46 47 48 49 50
Distance	Dep	Lat. 4 Deg.	Dep. 633	Lat.	Dep. 631	Lat.	Dep. 63½	Lat.	Distance.

Distance.	26 ]	Oeg.	261/4	Deg.	$26\frac{1}{2}$	Deg.	26¾	Deg.	Distance	$\frac{1}{2}$
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.	3
51	45·84	22·36	45·74	22·56	45·64	22·76	45·54	22·96	51	
52	46·74	22·80	46·64	23·00	46·54	23·20	46·43	23·41	52	
53	47·64	23·23	47·53	23·44	47·43	23·65	47·33	23·86	53	
54	48·53	23·67	48·43	23·88	48·33	24·09	48·22	24·31	54	
55	49·43	24·11	49·33	24·33	49·22	24·54·	49·11	24·76	55	
56	50·33	24·55	50·22	24·77	50·12	24·99	50·01	25·21	56	
57	51·23	24·99	51·12	25·21	51·01	25·43	50·00	25·66	57	
58	52·13	25·43	52·02	25·65	51·91	25·88	51·79	26·11	58	
59	53·03	25·86	52·92	26·09	52·80	26·33	52·69	26·56	59	
60	53·93	26·30	53·81	26·54	53·70	26·77	53·58	27·01	60	
61	54·83	26·74	54·71	26·98	54·59	27·22	54·47	27·46	61	~~~~~~
62	55·73	27·18	55·61	27·42	55·49	27·66	55·36	27·91	62	
63	56·62	27·62	56·50	27·86	56·38	28·11	56·26	28·36	63	
64	57·52	28·06	57·40	28·31	57·28	28·56	57·15	28·81	64	
65	58·42	28·49	58·30	28·75	58·17	29·00	58·04	29·26	65	
66	59·32	28·93	59·19	29·19	59·07	29·45	58·94	29·71	66	
67	60·22	29·37	60·09	29·63	59·96	29·90	59·83	30·16	67	
68	61·12	29·81	60·99	30·08	60·86	30·34	60·72	30·61	68	
69	62·02	30·25	61·88	30·52	61·75	30·79	61·62	31·06	69	
70	62·92	30·69	62·78	30·96	62·65	31·23	62·51	31·51	70	
71	63·81	31·12	63·68	31·40	63·54	31·68	63·40	31·96	71	••••••
72	64·71	31·56	64·57	31·84	64·44	32·13	64·29	32·41	72	
73	65·61	32·00	65·47	32·29	65·33	32·57	65·19	32·86	73	
74	66·51	32·44	66·37	32·73	66·23	33·02	66·08	33·31	74	
75	67·41	32·88	67·27	33·17	67·12	33·46	66·97	33·76	75	
76	68·31	33·32	68·16	33·61	68·01	33·91	67·87	34·21	76	
77	69·21	33·75	69·06	34·06	68·91	34·36	68·76	34·66	77	
78	70·11	34·19	69·96	34·50	69·80	34·80	69·65	35·11	78	
79	71·00	34·63	70·85	34·94	70·70	35·25	70·55	35·56	79	
80	71·90	35·07	71·75	35·38	71·59	35·70	71·44	36·01	80	
81 82 83 84 85 86 87 88 89 90	72·80 73·70 74·60 75·50 76·40 77·80 78·20 79·09 79·99 80·89	35·51 35·95 36·38 36·82 37·26 37·70 38·14 38·58 39·01 39·45	72.65 73.54 74.44 75.84 76.23 77.13 78.03 78.92 79.82 80.72	35·83 36·27 36·71 37·15 37·59 38·04 38·48 38·92 39·36 39·81	72·49 73·38 74·28 75·17 76·07 76·96 77·86 78·75 79·65 80·54	36·14 36·59 37·03 37·48 37·93 38·37 38·82 39·27 39·71 40·16	72·33 73·22 74·12 75·01 75·90 76·80 77·69 78·58 79·48 80·37	\$6.46 \$6.91 \$7.36 \$7.81 \$8.26 \$8.71 \$9.16 \$9.61 \$40.06 \$40.51	81 82 83 84 85 86 87 88 89	
91	81·79	39·89	81·62	40·25	81·44	40·60	81·26	40.96	91	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
92	82·69	40·33	82·51	40·69	82·33	41·05	82·15	41.41	92	
93	83·59	40·77	83·41	41·13	83·23	41·50	83·05	41.86	93	
94	84·49	41·21	84·31	41·58	84·12	41·94	83·94	42.31	94	
95	85·39	41·65	85·20	42·02	85·02	42·39	84·83	42.76	95	
96	86·28	42·08	86·10	42·46	85·91	42·83	85·73	43.21	96	
97	87·18	42·52	87·00	42·90	86·81	43·28	86·62	43.66	97	
98	88·08	42·96	87·89	43·34	87·70	43·73	87·51	44.11	98	
99	88·98	43·40	88·79	43·79	88·60	44·17	88·40	44.56	99	
100	89·88	43·84	89·69	44·23	89·49	44·62	89·30	45.01	100	
Distance.	Dep. 64 1	Lat.	Dep. 633/4	Lat. Deg.	Dep. 63½	Lat.	Dep. 631/4	Lat. Deg.	Distance.	

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61 62 63 64 65 66 67 68 69 70	53·35 54·23 55·10 55·98 56·85 57·72 58·60 59·47 60·35 61·22	29·57 30·06 30·54 31·03 31·51 32·00 32·48 32·97 33·45 33·94	53·22 54·97 55·84 56·71 57·58 58·46 ·59·33 60·20 61·07	29·81 30·29 30·78 31·27 31·76 32·25 32·74 33·23 33·71 34·20	53·09 53·96 54·83 55·70 56·57 57·44 58·31 59·18 60·05 60·92	30·04 30·53 31·02 31·52 32·01 32·50 32·99 33·48 33·98 34·47	52.96 53.83 54.70 55.56 56.43 57.30 58.17 59.04 59.91 60.77	30·27 30·77 31·26 31·76 32·25 32·75 33·25 33·74 34·24 34·74	61 62 63 64 65 66 67 68 69 70
71 72 73 74 75 76 77 78 79 80	62·10 62·97 63·85 64·72 65·60 66·47 67·35 68·22 69·09 69·97	34·42 34·91 35·39 35·88 36·36 36·85 37·33 37·82 38·30 38·78	61.95 62.82 63.69 64.56 65.44 66.31 67.18 68.05 68.93 69.80	34·69 35·18 35·67 36·16 36·65 37·14 37·62 38·11 38·60 39·09	61·80 62·67 63·54 64·41 65·28 66·15 67·02 67·89 68·76 69·63	34·96 35·45 35·95 36·44 36·93 37·42 37·92 38·41 38·90 39·39	61·64 62·51 63·38 64·25 65·11 65·98 66·85 67·72 68·59 69·46	35·23 35·73 36·22 36·72 37·22 37·71 38·21 38·70 39·20 39·70	71 72 73 74 75 76 77 78 79 80
81 82 83 84 85 86 87 88 39 90	67·35   37·33 68·22   37·82 69·09   38·30		79.67 71.54 72.42 73.29 74.16 75.03 75.91 76.78 77.65 78.52	39·58 40·07 40·56 41.04 41·53 42·02 42·51 43·00 43·49 43·98	70·50 71·37 72·24 73·11 73·98 74·85 75·72 76·59 77·46 78·33	39·89 40·38 40·87 41·36 41·86 42·35 42·84 43·33 43·83 44·32	70·32 71·19 72·06 72·93 73·80 74·67 75·53 76·40 77·27 78·14	40·19 40·69 41·19 41.68 42·18 42·67 43·17 43·67 44·16 44·66	81 82 83 84 85 86 87 88 89 90
91 92 93 94 95 96 97 98 99 100	79·59 80·46 81·34 82·21 83·09 83·96 84·84 85·71 86·59 87·46	44·12 44·60 45·09 45·57 46·06 46·54 47·03 47·51 48·00 48·48	79·40 80·27 81·14 82·01 82·89 83·76 84·63 85·50 86·38 87·25	44·46 44·95 45·44 45·93 46·42 46·91 47·40 47·88 48·37 48·86	79·20 80·07 80·94 81·81 82·68 83·55 84·42 85·20 86·17 87·04	44·81 45·30 45·80 46·29 46·78 47·27 47·77 48·26 48·75 49·24	79·01 79·87 80·74 81·61 82·48 83·35 84·22 85·08 85·95 86·82	45·16 45·65 46·15 46·64 47·14 47·64 48·13 48·63 49·13 49·62	91 92 93 94 95 96 97 98 99 100
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1 2 3 4 5 6	0.87 1.73 2.60 3.46	0.50 1.00 1.50 2.00	0.86 1.73 2.59 3.46	0·50 1·01 1·51 2·02	0.86 1.72 2.58 3.45	0.51 1.02 1.52 2.03	0.86 1.72 2.58 3.44	0.51 1.02 1.53 2.05	$\begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix}$
\$ 6 7 8 9 10	4·33 5·20 6·06 6·93 7·79 8·66	2·50 3·00 3·50 4·00 4·50 5·00	4·32 5·18 6·05 6·91 7·77 8·64	2·52 3·02 3·53 4·03 4·53 5·04	4·31 5·17 6·03 6·89 7·75 8·62	2·54 3·05 3·55 4·06 4·57 5·08	4·30 5·16 6·02 6·88 7·73 8·59	2·56 3·07 3·58 4·09 4·60 5·11	$\begin{bmatrix} 5 & 6 & 7 & 8 & 9 & 10 & 10 & 10 & 10 & 10 & 10 & 10 $
11 12 13 14 15 16 17 18 19 20	9·53 10·39 11·26 12·12 12·99 13·86 14·72 15·59 16·45 17·32	5·50 6·00 6·50 7·00 7·50 8·00 8·50 9·00 9·50	9·50 10·37 11·23 12·09 12·96 13·82 14·69 15·55 16·41 17·28	5·54 6·05 6·55 7·05 7·56 8·06 8·56 9·07 9·57	9·48 10·34 11·20 12·06 12·92 13·79 14·65 15·51 16·37 17·23	5.58 6.09 6.60 7.11 7.61 8.12 8.63 9.14 9.64 10.15	9·45 10·31 11·17 12·03 12·89 13·75 14·61 15·47 16·33 17·19	5·62 6·14 6·65 7·16 7·67 8·18 8·69 9·20 9·71 10·23	11 12 13 14 15 16 17 18 19 20
21 22 23 24 25 26 27 28 29 30	18·19 19·05 19·92 20·78 21·65 22·52 23·38 24·25 25·11 25·98	10·50 11·00 11·50 12·00 12·50 13·00 13·50 14·00 14·50 15·00	18·14 19·00 19·87 20·73 21·60 22·46 23·32 24·19 25·05 25·92	10.58 11.08 11.59 12.09 12.59 13.10 13.60 14.11 14.61 15.11	18·09 18·96 19·82 20·68 21·54 22·40 23·26 24·13 24·99 25·85	10·66 11·17 11·67 12·18 12·69 13·20 13·70 14·21 14·72 15·23	18·05 18·91 19·77 20·63 21·49 22·34 26·20 24·06 24·92 25·78	10·74 11·25 11·76 12·27 12·78 13·29 13·80 14·32 14·83 15·34	21 22 23 24 25 26 27 28 29 30 30
31 32 33 34 35 36 37 38 39 40	26·85 27·71 28·58 29·44 30·31 31·18 32·04 32·91 33·77 34·64	15·50 16·00 16·50 17·00 17·50 18·00 18·50 19·00 19·50 20·00	26·78 27·64 28·51 29·37 30·23 31·10 31·96 32·83 33·69 34·55	15·62 16·12 16·62 17·13 17·63 18·14 18·64 19·14 19·65 20·15	26·71 27·57 28·43 29·30 30·16 31·02 31·88 32·74 33·60 34·47	15·73 16·24 16·75 17·26 17·76 18·27 18·78 19·29 19·79 20·30	26·64 27·50 28·36 29·22 30·08 30·94 31·80 32·66 33·52 34·38	15·85 16·36 16·87 17·38 17·90 18·41 18·92 19·43 19·94 20·45	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	35·51 36·37 37·24 38·11 38·97 39·84 40·70 41·57 42·44 43·30	20·50 21·00 21·50 22·00 22·50 23·00 23·50 24·00 24·50 25·00	35·42 36·28 37·14 38·01 38·87 39·74 40·60 41·46 42·33 43·19	20·65 21·16 21·66 22·17 22·67 23·17 23·68 24·18 24·68 25·19	35·33 36·19 37·05 37·91 38·77 39·63 40·50 41·36 42·22 43·08	20·81 21·32 21·82 22·33 22·84 23·35 23·85 24·36 24·87 25·38	35·24 36·10 36·95 37·81 38·67 39·53 40·39 41·25 42·11 42·97	20·96 21·47 21·99 22·50 23·01 23·52 24·03 24·54 25·05 25·56	41 42 43 44 45 46 47 48 49 50
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51	44.17	25.50	44.06	25.69	43.94	25.88	43.83	26.08	51	ζ
52 53	45.03	26.00	44.92	26.20	44.80	26.39	44.69	26.59	52	(
( 53	45.90	26.50	45.78	26.70	45.67	26.90	45.55	27.10	53	?
54	46.77	27.00	46.65	27.20	46.53	27.41	46.41	27.61	54	?
55 56	47·63 48·50	27·50 28·00	47·51 48·37	$27.71 \\ 28.21$	47·39 48·25	27·91 28·42	47·27 48·13	28·12 28·63	- 55 56	?
57	49.36	28.50	49.24	28.72	49.11	28.93	48.99	29.14	56 57	)
58	50.23	29.00	50:10	29.22	49.97	29.44	49.85	29.65	58	)
2 59	51.10	29.50	50.97	29.72	50.84	29.94	50.70	30.17	59	)
60	51.96	30.00	51.83	30.23	51.70	30.45	51.56	30.68	60	{
61	52.83	30.50	52.69	30.73	52.56	30.96	52.42	31.19	61	ζ
62	53.69	31.00	53.56	31.23	53.42	31.47	53.28	31.70	62	5
63	54.56	31.50	54.42	31.74	54.28	31.97	54.14	32.21	63	5
64	55.43	32.00	55.29	32·24 32·75	55.14	32.48	55.00	32.72	64 65	(
65	56·29 57·16	32·50 33·00	56·15 57·01	33.75	56.01	32·99 33·50	55·86 56·72	33.23	66	(
67	58.02	33.20	57.88	33.75	56·87 57·73	34.01	57.58	33·75 34·26	67	(
68	58.89	34.00	58.74	34.26	58.59	34.51	58.44	34.77	68	(
69	59.76	34.50	59.60	34.76	59.45	35.02	59.30	35.28	69	(
5 70	60.62	35.00	60.47	35.26	60.31	85.53	60.16	35.79	70	ζ
71	61.49	35.50	61.33	35.77	61.18	36.04	61.02	36.30	71	{
72	62·35 63·22	36.00	62.20	36.27	62.04	36.54	61.88	36.81	72	2
73	63.22	36.50	63.06	36.78	62.90	37.05	62.74	37.32	73	?
74	64.09	37.00	63.92	37.28	63.76	37.56	63.60	37.84	74	)
$\begin{cases} 75 \\ 76 \end{cases}$	64 95 65 82	37.50	64.79	37·78 38·29	64·62 65·48	38.07	64·46 65·31	38.35	75 76	)
76	66.68	38·00 38·50	65·65 66·52	38.79	66.35	38.57	66.17	38.86	77	)
78	67.55	39.00	67.38	39.29	67.21	39·08 39·59	67.03	39·37 39·88	78	)
79	68.42	39.50	68.24	39.80	68.07	40.10	67.89	40.39	79	)
80	69.28	40.00	69.11	40.30	68.93	40.60	68.75	40.90	80	>
81	70.15	40.50	69.97	40.81	69.79	41.11	69-61	41.41	81	?
82	71.01	41.00	70.83	41.31	70.65	41.62	70.47	41.93	82	7
83	71.88	41.50	71.70	41.81	71.52	42.13	71.33	42.44	83	?
( 84	72.75	42.00	72.56	42.32	72.38	42.63	72.19	42.95	84	)
85	73.61	42.50	73.43	42.82	73.24	43.14	73.05	43.46	85	
86	74.48	43.00	74.29	43.32	74.10	43.65	73 91	43.97	86	Σ
87	75.31	43.50	75.15	43.88	74.96	44.16	74.77	44.48	87	5
) 88	76.21	44.00	76.02	44.33	75.82	44.66	75.63	44.99	88	5
89	77.08	44.50	76.88	44.84	76.68	45.17	76.49	45.51	89 90	5
90	77.94	45.00	77.75	45.34	77.55	45.68	77.35	46.02	90	>
( 91	78.81	45.50	78.61	45.84	78.41	46.19	78.21	46.53	91	7
92	79.67	46.00	79.47	46.35	79.27	46.69	79.07	47.04	92	?
93	80.54	46.50	80.34	46.85	80.13	47.20	79.92	47.55	93	>
94	81.41	47.00	81.20	47.35	80.99	47.71	80.78	48.06	94	)
95	82.27	47.50	82.06	47.86	81.85	48.22	81.64	48.57	95	)
96	83.14 48.00		82.93	48.36	82.72	48.72	82.50	49.08	96 97	>
\ 97 98	84·00 84·87	48·50 49·00	83·79 84·66	48.87	83·58 84·44	49·23 49·74	83·36 84·22	49.60	98	5
99	85.74	49.50	85.52	49.87	85.30	50.25	84.22	50·11 50·62	99	5
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21 22 23 24 25 26 27 28 29 30	18·00 18·86 19·71 20·57 21·43 22·29 23·14 24·00 24·86 25·71	18·00 10·82 18·86 11·33 19·71 11·85 20·57 12·36 21·43 12·88 22·29 13·39 23·14 13·91 24·00 14·42		10·89 11·41 11·93 12·45 12·97 13·49 14·01 14·53 15·04 15·56	17·91 18·76 19·61 20·46 21·32 22·17 23·02 23·87 24·73 25·58	10·97 11·49 12·02 12·54 13·06 13·58 14·11 14·63 15·15 15·67	17·86 18·71 19·56 20·41 21·26 22·11 22·96 23·81 24·66 25·51	11·05 11·58 12·10 12·63 13·16 13·68 14·21 14·73 15·26 15·79	21 22 23 24 25 26 27 28 29 30 2
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41 42 43 44 45 46 47 48 49 50	35·14 36·00 36·86 37·72 38·57 39·43 40·29 41·14 42·00 42·86	21·12 21·63 22·15 22·66 23·18 23·69 24·21 24·72 25·24 25·75	35·05 35·91 36·76 37·62 38·47 39·33 40·18 41·04 41·89 42·75	21·27 21·79 22·31 22·83 23·34 23·86 24·38 24·90 25·42 25·94	34·96 35·81 36·66 37·52 38·37 39·22 40·07 40·93 41·78 42·63	21·42 21·94 22·47 22·99 23·51 24·03 24·56 25·08 25·60 26·12	34·86 35·71 36·57 37·42 38·27 39·12 39·97 40·82 41·67 42·52	21.57 22.10 22.63 23.15 23.68 24.21 24.73 25.26 25.78 26.31	41 42 43 44 45 46 47 48 49 50
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51 52 53 54 55 56 57 58 59 60	43·72 44·57 45·43 46·29 47·14 48·00 48·86 49·72 50·57 51·43	26·27 26·78 27·30 27·81 28·33 28·84 29·36 29·87 30·39 30·90	43·60 44·46 45·31 46·17 47·02 47·88 48·73 49·58 50·44 51·29	26·46 26·98 27·49 28·01 28·53 29·05 29·57 50·09 30·61 31·13	43·48 44·34 45·19 46·04 46·90 47·75 48·60 49·45 50·31 51·16	26·65 27·17 27·69 28·21 28·74 29·26 29·78 30·30 30·83 31·35	43:37 44:22 45:07 45:92 46:77 47:62 48:47 49:32 50:17 51:02	26·84 27·36 27·89 28·42 28·94 29·47 29·99 30·52 31·05 31·57	51 52 53 54 55 56 57 58 59 60	
61 62 63 64 65 66 67 68 69 70	52·29 53·14 54·00 54·86 55·72 56·57 57·43 58·29 59·14 60·00	31·42 31·93 32·45 32·96 33·48 33·99 34·51 35·02 35·54 36·05	52·15 53·00 53·86 54·71 55·57 56·42 57·28 58·13 58·99 59·84	31.65 32.16 32.68 33.20 33.72 34.24 34.76 35.28 35.80 36.31	52.01 52.86 53.72 54.57 55.42 56.27 57.13 57.98 58.83 59.68	31·87 32·39 32·92 33·44 33·96 34·48 35·01 35·53 36·05 36·57	51·87 52·72 53·57 54·42 55·27 56·12 56·98 57·82 58·67 59·52	32·10 32·63 33·15 33·68 34·20 34·73 35·26 35·78 36·31 36·83	61 62 63 64 65 66 67 68 69 70	~~~~~
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51	42·28	28·52	42·16	28·70	42·03	28·89	41·90	29·07	51
52	43·11	29·08	42·98	29·27	42·85	29·45	42·73	29·64	52
53	43·94	29·64	43·81	29·83	43·68	30·02	43·55	30·21	53
54	44·77	30·20	44·64	30·39	44·50	30·59	44·37	30·78	54
55	45·60	30·76	45·46	30·95	45·33	31·15	45·19	31·35	55
56	46·43	31·31	46·29	31·52	46·15	31·72	46·01	31·92	56
57	47·26	31·87	47·12	32·08	46·98	32·29	46·83	32·49	57
58	48·08	32·43	47·94	32·64	47·80·	32·85	47·66	33·06	58
59	48·91	32·99	48·77	33·21	48·62	33·42	48·48	33·63	59
60	49·74	33·55	49·60	33·77	49·45	33·98	49·30	34·20	60
61	50·57	34·11	50·42	34·33	50·27	34·55	50·12	34·77	61
62	51·40	34·67	51·25	34·89	51·10	35·12	50·94	35·34	62
63	52·23	35·23	52·08	35·46	51·92	35·68	51·76	35·91	63
64	53·06	35·79	52·90	36·02	52·74	36·25	52·59	36·48	64
65	53·89	36·35	53·73	36·58	53·57	36·82	53·41	37·05	65
66	54·72	36·91	54·55	37·15	54·39	37·38	54·23	37·62	66
67	55·55	37·46	55·38	37·71	55·22	37·95	55·05	38·19	67
68	56·37	38·03	56·21	38·27	56·04	38·52	55·87	38·76	68
69	57·20	38·58	57·03	38·83	56·86	39·08	56·69	39·33	69
70	58·03	39·14	57·86	39·40	57·69	39·65	57·52	39·90	70
71 72 73 74 75 76 77 78 79 80	58.86 59.69 60.52 61.35 62.18 63.01 63.84 64.66 65.49 66.32	39·70 40·26 40·82 41·38 41·94 42·50 43·62 44·18 44·74	58·69 59·51 60·34 61·17 61·99 62·82 63·65 64·47 65·30 66·13	39·96 40·52 41·08 41·65 42·21 42·77 43·34 43·90 44·46 45·02	58·51 59·34 60·16 60·99 61·81 62·63 63·46 64·28 65·11 65·93	40·21 40·78 41·35 41·91 42·48 43·05 43·61 44·18 44·75 45·31	58·34 59·16 59·98 60·80 61·62 62·45 63·27 64·09 64·91 65·73	40·47 41·04 41·61 42·18 42·75 43·32 43·89 44·46 45·03 45·60	71 72 73 74 75 76 77 78 79 80
81	67:15	45·29	66.95	45·59	66·75	45·88	66·55	46·17	81
82	67:98	45·85	67.78	46·15	67·58	46·45	67·37	46·74	82
83	68:81	46·41	68.61	46·71	68·40	47·01	68·20	47·31	83
84	69:64	46·97	69.43	47·28	69·23	47·58	69·02	47·88	84
85	70:47	47·53	70.26	47·84	70·05	48·14	69·84	48·45	85
86	71:30	48·09	71.09	48·40	70·87	48·71	70·66	49·02	86
87	72:13	48·65	71.91	48·96	71·70	49·28	71·48	49·59	87
88	72:96	49·21	72.74	49·53	72·52	49·84	72·30	50·16	88
89	73:78	49·77	73.57	50·09	73·35	50·41	73·13	50·73	89
90	74:61	50·33	74.39	50·65	74·17	50·98	73·95	51·30	90
91	75·44	50·89	75·22	51·22	75·00	51·54	74·77	51·87	91
92	76·27	51·45	76·05	51·78	75·82	52·11	75·59	52·44	92
93	77·10	52·00	76·87	52·34	76·64	52·68	76·41	53·01	93
94	77·93	52·56	77·70	52·90	77·47	53·24	77·23	53·58	94
95	78·76	53·12	78·53	53·47	78·29	53·81	78·06	54·15	95
96	79·59	53·68	79·35	54·03	79·12	54·37	78·88	54·72	96
97	80·42	54·24	80·18	54·59	79·94	54·94	79·70	55·29	97
98	81·25	54·80	81·01	55·15	80·76	55·51	80·52	55·86	98
99	82·07	55·36	81·83	55·72	81·59	56·07	81·34	56·43	99
100	82·90	55·92	82·66	56·28	82·41	56·64	82·16	57·00	100
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•	11 12 13 14 15 16 17 18 19 20	9·01 9·83 10·65 11·47 12·29 13·11 13·93 14·74 15·56 16·38	6.31 6.88 7.46 8.03 8.60 9.18 9.75 10.32 10.90 11.47	8.98 9.80 10.62 11.43 12.25 13.07 13.88 14.70 15.52 16.33	6·35 6·93 7·50 8·08 8·66 9·23 9·81 10·39 10·97 11·54	8.96 9.77 10.58 11.40 12.21 13.03 13.84 14.65 15.47 16.28	6·39 6·97 7·55 8·13 8·71 9·29 9·87 10·45 11·03 11·61	8·93 9·74 10·55 11·36 12·17 12·99 13·80 14·61 15·42 16·23	6·43 7·01 7·60 8·18 8·76 9·35 9·93 10·52 11·10 11·68	11
*******	21 22 23 24 25 26 27 28 29 30	17·20 18·02 18·84 19·66 20·48 21·30 22·12 22·94 23·76 24·57	12·05 12·62 13·19 13·77 14·34 14·91 15·49 16·06 16·63 17·21	17·15 17·97 18·78 19·60 20·42 21·23 22·05 22·87 23·68 24·50	12·12 12·70 13·27 13·85 14·43 15·01 15·58 16·16 16·74 17·31	17·10 17·01 18·72 19·54 20·35 21·17 21·98 22·80 23·61 24·42	12·19 12·78 13·36 13·94 14·52 15·10 15·68 16·26 16·84 17·42	17·04 17·85 18·67 19·48 20·29 21·10 21·91 22·72 23·54 24·35	12:27 12:85 13:44 14:02 14:61 15:19 15:77 16:36 16:94 17:53	21 22 23 24 25 26 27 28 29 30 2
· · · · · · · · · · · · · · · · · · ·	31 32 33 34 35 36 37 38 39 40	25·39 26·21 27·03 27·85 28·67 29·49 30·31 31·13 31·95 32·77	17·78 18·35 18·93 19·50 20·08 20·65 21·22 21·80 22·37 22·94	25·32 26·13 26·95 27·77 28·58 29·40 30·22 31·03 31·85 32·67	17·89 18·47 19·05 19·62 20·20 20·78 21·35 21·93 22·51 23·09	25·24 26·05 26·87 27·68 28·49 29·31 30·12 30·94 31·75 32·56	18·00 18·58 19·16 19·74 20·32 20·91 21·49 22·07 22·65 23·23	25·16 25·97 26·78 27·59 28·41 29·22 80·03 80·84 31·65 32·46	18·11 18·70 19·28 19·86 20·45 21·03 21·62 22·20 22·79 23·37	31 32 33 34 35 36 37 38 39 40
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nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	41·78	29·25	41·65	29·43	41·52	29·62	41·39	29·80	51
52	42·60	29·83	42·47	30·01	42·33	30·20	42·20	30·38	52
53	43·42	30·40	43·28	30·59	43·15	30·78	43·01	30·97	53
54	44·23	30·97	44·10	31·17	43·96	31·36	43·82	31·55	54
55	45·05	31·55	44·92	31·74	44·78	31·94	44·64	32·13	55
56	45·87	32·12	45·73	32·32	45·59	32·52	45·45	32·72	56
57	46·69	32·69	46·55	32·90	46·40	33·10	46·26	33·30	57
58	47·51	33·27	47·37	33·47	47·22	33·68	47·07	33·89	58
59	48·33	38·84	48·18	34·05	48·03	34·26	47·88	34·47	59
60	49·15	34·41	49·00	34·63	48·85	34·84	48·69	35·05	60
61	49·97	34·99	49·82	35·21	49·66	35·42	49·51	35·64	61 62 63 64 65 66 67 68 69 70 5
62	50·79	35·56	50·63	35·78	50·48	36·00	50·32	36·22	
63	51·61	36·14	51·45	36·36	51·29	36·58	51·13	36·81	
64	52·43	36·71	52·27	36·94	52·10	37·16	51·94	37·39	
65	53·24	37·28	53·08	37·51	52·92	37·75	52·75	37·98	
66	54·06	37·86	53·90	38·09	53·73	38·33	53·56	38·56	
67	54·88	38·43	54·71	38·67	54·55	38·91	54·38	39·14	
68	55·70	39·00	55·53	39·25	55·36	39·49	55·19	39·73	
69	56·52	39·58	56·35	39·82	56·17	40·07	56·00	40·31	
70	57·34	40·15	57·16	40·40	56·99	40·65	56·81	40·90	
71	58·16	40·72	57.98	40·98	57·80	41·23	57·62	41·48	71
72	58·98	41·30	58.80	41·55	58·62	41·81	58·43	42·07	72
73	59·80	41·87	59.61	42·13	59·43	42·39	59·24	42·65	73
74	60·62	42·44	60.43	42·71	60·24	42·97	60·06	43·23	74
75	61·44	43·02	61.25	43·29	61·06	43·55	60·87	43·82	75
76	62·26	43·59	62.06	43·86	61·87	44·13	61·68	44·40	76
77	63·07	44·17	62.88	44·44	62·69	44·71	62·49	44·99	77
78	63·89	44·74	63.70	45·02	63·50	45·29	63·30	45·57	78
79	64·71	45·31	64.51	45·59	64·32	45·88	64·11	46·16	79
80	65·53	45·89	65.33	46·17	65·13	46·46	64·93	46·74	80
81	66:35	46·46	66·15	46·75	65·94	47·04	65·74	47·32	81 82 83 84 85 86 87 88 89 90 90
82	67:17	47·03	66·96	47·33	66·76	47·62	66·55	47·91	
83	67:99	47·61	67·78	47·90	67·57	48·20	67·36	48·49	
84	68:81	48·18	68·60	48·48	68·39	48·78	68·17	49·08	
85	69:63	48·75	69·41	49·06	69·20	49·36	68·98	49·66	
86	70:45	49·33	70·23	49·63	70·01	49·94	69·80	50·25	
87	71:27	49·90	71·05	50·21	70·83	50·52	70·61	50·83	
88	72:09	50·47	71·86	50·79	71·64	51·10	71·42	51·41	
89	72:90	51·05	72·68	51·37	72·46	51·68	72·23	52·00	
90	73:72	51·62	73·50	51·94	73·27	52·26	73·04	52·58	
91	74·54	52·20	74·31	52·52	74·08	52:84	73·85	53·17	91
92	75·36	52·77	75·13	53·10	74·90	53:42	74·66	53·75	92
93	76·18	53·34	75·95	53·67	75·71	54:01	75·48	54·34	93
94	77·00	53·92	76·76	54·25	76·53	54:59	76·29	54·92	94
95	77·82	54·49	77·58	54·83	77·34	55:17	77·10	55·50	95
96	78·64	55·06	78·40	55·41	78·16	55:75	77·91	56·09	96
97	79·46	55·64	79·21	55·98	78·97	56:33	78·72	56·67	97
98	80·28	56·21	80·03	56·56	79·78	56:91	79·53	57·26	98
99	81·10	56·78	80·85	57·14	80·60	57:49	80·35	57·84	99
100	81·92	57·36	81·66	57·71	81·41	58:07	81·16	58·42	100
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1 2 3 4 5 6 7 8 9	0·81 1·62 2·43 3·24 4·05 4·85 5·66 6·47 7·28 8·09	0·59 1·18 1·76 2·35 2·94 3·53 4·11 4·70 5·29 5·88	0·81 1·61 2·42 3·23 4·03 4·84 5·65 6·45 7·26 8·06	0·59 1·18 1·77 2·37 2·96 3·55 4·14 4·73 5·32 5·91	0·80 1·61 2·41 3·22 4·02 4·82 5·63 6·43 7·23 8·04	0·59 1·19 1·78 2·38 2·97 3·57 4·16 4·76 5·35 5·95	0·80 1·60 2·40 3·20 4·01 4·81 5·61 6·41 7·21 8·01	0·60 1·20 1·79 2·39 2·99 8·59 4·19 4·79 5·38 5·98	1 2 3 4 5 6 7 8 9	
11	8·90	6·47	8·87	6·50	8·84	6·54	8·81	6·58	11	~~~~~
12	9·71	7·05	9·68	7·10	9·65	7·14	9·61	7·18	12	
13	10·52	7·64	10·48	7·69	10·45	7·73	10·42	7·78	13	
14	11·33	8·23	11·29	8·28	11·25	8·33	11·22	8·38	14	
15	12·14	8·82	12·10	8·87	12·06	8·92	12·02	8·97	15	
16	12·94	9·40	12·90	9·46	12·86	9·52	12·82	9·57	16	
17	13·75	9·99	13·71	10·05	13·67	10·11	13·62	10·17	17	
18	14·56	10·58	14·52	10·64	14·47	10·71	14·42	10·77	18	
19	15·37	11·17	15·32	11·23	15·27	11·30	15·22	11·37	19	
20	16·18	11·76	16·13	11·83	16·08	11·90	16·03	11·97	20	
21	16·99	12·34	16·94	12:42	16·88	12·49	16·83	12·56	21	
22	17·80	12·93	17·74	13:01	17·68	13·09	17·63	13·16	22	
23	18·61	13·52	18·55	13:60	18·49	13·68	18·43	13·76	23	
24	19·42	14·11	19·35	14:19	19·29	14·28	19·23	14·36	24	
25	20·23	14·69	20·16	14:78	20·10	14·87	20·03	14·96	25	
26	21·03	15·28	20·97	15:37	20·90	15·47	20·83	15·56	26	
27	21·84	15·87	21·77	15:97	21·70	16·06	21·63	16·15	27	
28	22·65	16·46	22·58	16:56	22·51	16·65	22·44	16·75	28	
29	23·46	17·05	23·39	17:15	23·31	17·25	23·24	17·35	29	
30	24·27	17·63	24·19	17:74	24·12	17·84	24·04	17·95	30	
31	25·08	18·22	25·00	18·33	24·92	18·44	24·84	18·55	31	
32	25·89	18·81	25·81	18·92	25·72	19·03	25·64	19·15	32	
33	26·70	19·40	26·61	19·51	26·53	19·63	26·44	19·74	33	
34	27·51	19·98	27·42	20·10	27·33	20·22	27·24	20·34	34	
35	28·32	20·57	28·23	20·70	28·13	20·82	28·04	20·94	35	
36	29·12	21·16	20·03	21·29	28·94	21·41	28·85	21·54	36	
37	29·93	21·75	29·84	21·88	29·74	22·01	29·65	22·14	37	
38	30·74	22·34	30·64	22·47	30·55	22·60	30·45	22·74	38	
39	31·55	22·92	31·45	23·06	31·35	23·20	31·25	23·33	39	
40	32·36	23·51	32·26	23·65	32·15	23.79	32·05	23·93	40	
41	33·17	24·10	33·06	24·24	32·96	24·39	32·85	24·53	41	
42	33·98	24·69	33·87	24·83	33·76	24·98	33·65	25·13	42	
43	34·79	25·27	34·68	25·43	34·57	25·58	34·45	25·73	43	
44	35·60	25·86	35·48	26·02	35·37	26·17	35·26	26·93	44	
45	36·41	26·45	36·29	26·61	36·17	26·77	36.06	26·92	45	
46	37·21	27·04	37·10	27·20	36·98	27·36	36·86	27·52	46	
47	38·02	27·63	37·90	27·79	37·78	27·96	37·66	28·12	47	
48	38·83	28·21	38·71	28·38	28·59	28·55	38·46	28·72	48	
49	39·64	28·80	39·52	28·97	39·39	29·15	39·26	29·32	49	
50	40·45	29·39	40·32	29·57	40·19	29·74	40·06	29·92	50	
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nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	дсе.
51 52 53 54 55 55 56 57 58 59 60	41.26 42.07 42.88 43.69 44.50 45.30 46.11 46.92 47.73 48.54	29·98 30·56 31·15 31·74 32·33 32·92 33·50 34·09 34·68 35·27	41·13 41·94 42·74 43·55 44·35 45·16 45·97 46·77 47·58 48·39	30·16 30·75 31·34 31·93 32·52 33·11 33·70 34·89 35·48	41·00 41·80 42·60 43·41 44·21 45·02 45·82 46·62 47·43 48·23	30·34 30·93 31·53 32·12 32·72 33·31 33·90 34·50 35·69	40·86 41·67 42·47 43·27 44·07 44·87 45·67 46·47 47·27 48·08	30·51 31·11 31·71 32·31 32·91 33·51 34·10 34·70 35·30 35·90	51 52 53 54 55 56 57 58 59 60
61 62 63 64 65 66 67 68 69 70	49·35 50·16 50·97 51·78 52·59 53·40 54·20 55·01 55·82 56·63	35·85 36·44 37·03 37·62 38·21 38·79 39·38 39·97 40·56 41·14	49·19 50·00 50·81 51·61 52·42 53·23 54·03 54·84 55·64 56·45	36·07 36·66 37·25 37·84 38·44 39·03 39·62 40·21 40·80 41·39	49·04 49·84 50·64 51·45 52·25 53·05 53·86 54·66 55·47 56·27	36·28 36·88 37·47 38·07 38·66 39·26 39·85 40·45 41·04 41·64	48.88 49.68 50.48 51.28 52.08 52.88 53.68 54.49 55.29 56.09	36·50 37·10 37·69 38·29 38·89 39·49 40·09 40·69 41·28 41·88	61 62 63 64 65 66 67 68 69 70
71 72 73 74 75 76 77 78 79 80	57·44 58·25 59·06 59·87 60·68 61·49 62·29 63·10 63·91 64·72	41·73 42·32 42·91 43·50 44·08 44·67 45·26 45·85 46·43 47·02	57·26 58·06 58·87 59·68 60·48 61·29 62·10 62·90 63·71 64·52	41.98 42.57 43.17 43.76 44.35 44.94 45.53 46.12 46.71 47.30	57.07 57.88 58.68 59.49 60.29 61.09 61.90 62.70 63.50 64.31	42·23 42·83 43·42 41·02 44·61 45·21 45·80 46·40 46·99 47·59	56·89 57·69 58·49 59·29 60·09 60·90 61·70 62·50 63·30 64·10	42·48 43·08 43·68 44·28 44·87 45·47 46·07 46·67 47·27 47·87	71 72 73 74 75 76 77 78 79 80
81 82 83 84 85 86 86 87 88 89 90	65·53 66·34 67·15 67·96 68·77 69·58 70·38 71·19 72·00 72·81	47·61 48·20 48·79 49·37 49·96 50·55 51·14 51·73 52·31 52·90	65·32 66·13 66·93 67·74 68·55 69·35 70·16 70·97 71·77 72·58	47·90 48·49 49·67 50·26 50·85 51·44 52·04 52·63 53·22	65·11 65·92 66·72 67·52 68·33 69·13 69·94 70·74 71·54 72·35	48·18 48·78 49·37 49·97 50·56 51·15 51·75 52·34 52·94 53·53	64·90 65·70 66·50 67·31 68·11 68·91 69·71 70·51 71·31 72·11	48·46 49·06 49·66 50·26 50·86 51·46 52·05 52·65 53·25 53·85	81 82 83 84 85 86 87 88 89 90
91 92 93 94 95 96 97 98 99 100	73·62 74·43 75·24 76·05 76·86 77·67 78·47 79.28 80·09 80·90	53·49 54·08 54·66 55·25 55·84 56·43 57·02 57·60 58·19 58·78	73·39 74·19 75·00 75·81 76·61 77·42 78·23 79·03 79·84 80·64	53·81. 54·40 54·99 55·58 56·17 56·77 57·36 57·95 58·54 59·13	73·15 73·95 74·76 75·56 76·37 77·17 77·97 78·78 79·58 80·39	54·13 54·72 55·32 55·91 56·51 57·10 57·70 58·29 58·89 59·48	72·91 73·72 74·52 75·32 76·12 76·92 77·72 78·52 79·32 80·13	54·45 55·05 55·64 56·24 56·84 57·44 58·64 58·64 59·23 59·83	91 92 93 94 95 96 97 98 99
Distance.	Dep. 54	Lat.	Dep. 533/4	Lat.	Dep. 53½	Lat.	Dep. 531/4	Lat.	Distance.

{	Distance	37 I	Oeg.	~~~ 37¼	Deg.	37½	Deg.	373/4	Deg.	$\left. \left\{ \begin{array}{l}$
}	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	[Fe. ]
}-	$\frac{1}{2}$	0.80 1.60	0.60 1.20	0.80 1.59	0·61 1·21	0·79 1·59	0·61 1·22	0.79 1.58	0·61 1·22	1 2 3 4 5 6 7 8
>	2 3 4 5 6 7 8	2.40	1.81	2.39	1.82	2.38	1.83	2.37	1.84	3 >
7	4	3·19 3·99	$\frac{2.41}{3.01}$	3·18 3·98	2·42 3·03	3·17 3·97	2·43 3·04	3·16 3·95	2·45 3·06	4 >
(	6	4.79	3.61	4.78	3.63	4.76	3.05	4.74	3.67	6 7
(	7	5.59	4.21	5.57	4.24	5.22	1.26	5.53	4.29	7 7
(	8	6.39	4.81	6.37	4.84	6.35	4.87	6.33	4.90	8 (
5	9 10	7·19 7·99	5·42 6·02	7·16 7·96	5·45 6·05	7·14 7·93	5·48 6·09	7·12 7·91	5·51 6·12	$\begin{vmatrix} 9 \\ 10 \end{vmatrix}$
}	11	8.78	6.62	8.76	6.66	8.73	6.70	8.70	6.73	11
ζ.	12	9.58	7.22	9.55	7.26	9.52	7.31	9.49	7.35	1 12 (
5	13	10.38	7.82 8.43	10°35 11°14	7·87 8·47	10·31 11·11	7·91 8·52	10·28 11·07	7.96	13 (
5	14	11·18 11·98	9.03	11.14	9.08	11.90	9.13	11.86	8·57 9·18	$\begin{vmatrix} 14 \\ 15 \end{vmatrix}$
5	$\frac{15}{16}$	12.78	9.63	12.74	9.68	12.69	9.74	12.65	9.80	.16
>	17	13.58	10.23	13.53	10.29	13.49	10.35	13.44	10.41	17
$\rangle$	18	14.38	10.83	14·33 15·12	10.90 11.50	14·28 15·07	10.96 11.57	14.23	11.02	18
>	19 20	15·17 15·97	$11.43 \\ 12.04$	15.12	12.11	15.87	12.18	15.02 15.81	11·63 12·24	$\begin{vmatrix} 19 \\ 20 \end{vmatrix}$
3		16.77	12.64	16.72	12.71	16.66	12.78	16 60	12.86	21
5	$\frac{21}{22}$	17.57	13.24	17.51	13.32	17.45	13.39	17:40	13.47	$\frac{21}{22}$
>	23	17·57 18·37	13.84	17·51 18·31	13.92	18.25	14.00	18.19	14.08	23
$\rangle$	$^{24}$	19.17	14.44	19.10	14.53	19·04 19·83	$14.61 \\ 15.22$	18.98	14.69	24
>	25	19·97 20·76	15.05 15.65	19·90 20·70	15·13 15·74	20.63	15.83	19·77 20·56	15·31 15·92	$\begin{bmatrix} 25 \\ 26 \end{bmatrix}$
>	$\frac{26}{27}$	21.56	16.25	21.49	16.34	21.42	16.44	21.35	16.53	27
>	28	22.36	16.85	22.29	16.95	22 21	17.05	22.14	17.14	28 2
>	29 30	23.16	17.45	23.08	17.55	23·01 23·80	17.65 18.26	22·93 23·72	17.75	$\left \begin{array}{c} \overline{29} \\ 30 \end{array}\right>$
3	30	23.96	18.05	23.88	18.16		-	ļ.	18.37	30 3
5	31	24.76	18.66	24·68 25·47	18·76 19·37	24·59 25·39	18.87 19.48	24.51	18.98	31 5
	32	25·56 26·35	19·26 19·86	26.27	19.97	26.18	20.09	25·30 26·09	19·59 20·20	32 8
	$\frac{33}{34}$	27.15	20.46	27.06	20.58	26.97	20.70	26.88	20.82	$\begin{vmatrix} 33 \\ 34 \end{vmatrix}$
	35	27.95	21.06	27.86	21.19	27.77	21.31	27.67	21.43	35
$\rangle$	36	28.75	21.67	28.66	21.79	28.56	21.92	28.46	22.04	36
$\rangle$	37	29.55	22.27	29·45 30·25	22·40 23·00	29·35 30·15	22·52 23·13	29.26	22.65	37.
7	38	30·35 31·15	22·87 23·47	31.04	25.61	30.94	23.74	30 05 30 84	23.26	38 8
ζ.	$\frac{39}{40}$	31.95	24 07	31.84	24.21	31.73	24.35	31.63	24.49	40 2
5	41	32.74	24 67	32.64	24.82	32.53	24.96	32.42	25.10	41 5
$\rangle$	42	33.54	25.28	33.43	25.42	33.32	25.57	33.21	25.71	42
7	43	34.34	25.88	34.23	26·03 26·63	34·11 34·91	26.18	34.00	26.33	43
7	44	35·14 35·94	26·48 27·08	35·02 35·82	27.24	35.70	26·79 27·39	34·79 35·58	26·94 27·55	44 45
7	$\frac{45}{46}$	36.74	27.68	36.62	27.84	36.49	28.00	36.37	28 16	46
7	47	37.54	28.29	37.41	28.45	37.29	28.61	37.16	28.77	47
7	48	38.33	28 89	38.21	29.05	38.08	29.22	37.95	29.39	48 2
(	49	39.13	29.49	39.00	29·66 30·26	38·87 39·67	29·83 30·44	38·74 39·53	30.00	49
ζ.	50	39.93	30.09					ļ		50
{	ce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	. ee .
{	Distance	53	Deg.	523/4	Deg.	521/2	Deg.	521/4	í Deg.	Distance
(	$\sim$	$\sim$	~~~	~~ٿ	~~~	<u>"</u> ~~~	~~~	<b>"</b> ~~~	~~~	لمتما

Distance	37 ]	Deg.	371/4	Deg.	37½	Deg.	373/4	Deg.	$\left\langle \begin{array}{c} \\ \\ \\ \end{array} \right\rangle$ Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	F. {
51	40·73	30·69	40·60	30·87	40·46	31.05	40·33	31·22	51
52	41·53	31·29	41·39	31·48	41·25	31.66	41·12	31·84	52
53	42·33	31·90	42·19	32·08	42·05	32.26	41·91	32·45	53
54	43·13	32·30	42·98	32·69	42·84	32.87	42·70	33·06	54
55	43·92	33·10	43·78	33·29	43·63	33.48	43·49	33·67	55
56	44·72	33·70	44·58	33·90	44·43	34.09	44·28	34·28	56
57	45·52	34·30	45·37	34·50	45·22	34.70	45·07	34·90	57
58	46·32	34·91	46·17	35·11	46·01	35.31	45·86	35·51	58
59	47·12	35.51	46·96	35·71	46·81	35.92	46·65	36·12	59
60	47·92	36·11	47·76	36·32	47·60	36.53	47·44	36·73	60
61	48·72	36·71	48-56	36·92	48·39	37·13	48·23	37·35	61 62 63 64 65 66 67 68 69 70
62	49·52	37·31	49-35	37·53	49·19	37·74	49·02	37·96	
63	50·31	37·91	50-15	38·13	49·98	38·35	49·81	38·57	
64	51·11	38·52	50-94	38·74	50·77	38·96	50·60	39·18	
65	51·91	39·12	51-74	39·34	51·57	39·57	51·39	39·79	
66	52·71	39·72	52-54	39·95	52·36	40·18	52·19	40·41	
67	53·51	40·32	53-33	40·55	53·15	40·79	52·98	41·02	
68	54·31	40·92	54-13	41·16	53·95	41·40	53·77	41·63	
69	55·11	41·53	54-92	41·77	54·74	42·00	54·56	42·24	
70	55·90	42·13	55-72	42·87	55·53	42·61	55·35	42·86	
71 72 73 74 75 76 77 78 79 80	56·70 57·50 58·30 59·10 59·90 60·70 61·49 62·29 63·09 63·89	42·73 43·33 43·93 44·53 45·14 45·74 46·94 47·54 48·15	56·52 57·31 58·11 58·90 59·70 60·50 61·29 62·09 62·88 63·68	42.98 43.58 44.19 44.79 45.40 46.00 46.61 47.21 47.82 48.42	56·33 57·12 57·91 58·71 59·50 60·29 61·09 61·88 62·67 63·47	43·22 43·83 44·41 45·05 45·66 46·27 46·87 47·48 48·09 48·70	56·14 56·93 57·72 58·51 59·30 60·09 60·88 61·67 62·46 63·26	43·47 44·08 44·69 45·30 45·92 46·53 47·14 47·75 48·37 48·98	71 72 73 74 75 76 77 78 79 80
81	64·69	48·75	64·48	49·03	64·26	49·31	64·05	49·59	81
82	65·49	49·35	65·27	49·63	65·05	49·92	64·84	50·20	82
83	66·29	49·95	66·07	50·24	65·85	50·53	65·63	50·81	83
84	67·09	50·55	66·86	50·84	66·64	51·14	66·42	51·43	84
85	67·38	51·15	67·66	51·45	67·43	51·74	67·21	52·04	85
86	68·68	51·76	68·46	52·66	68·23	52·35	68·00	52·65	86
87	69·48	52·36	69·25	52·66	69·02	52·96	68·79	53·26	87
88	70·28	52·96	70·05	53·27	69·82	53·57	69·58	53·88	88
89	71·08	53·56	70·84	53·87	70·61	54·18	70·37	54·49	89
90	71·88	54·16	71·64	54·48	71·40	54·79	71·16	55·10	90
91	72.68	54·77	72·44	55.08	72·20	55·40	71.95	55·71	91
92	73.47	55·37	73·23	55.69	72·99	56·01	72.74	56·32	92
93	74.27	55·97	74·03	56.29	73·78	56·61	73.53	56·94	93
94	75.07	56·57	74·82	56.90	74·58	57·22	74.32	57·55	94
95	75.87	57·17	75·62	57.50	75·87	57·83	75.12	58·16	95
96	76.67	57·77	76·42	58.11	76·16	58·44	75.91	58·77	96
97	77.47	58·38	77·21	58.71	76·96	59·05	76.70	59·39	97
98	78.27	58·98	78·01	59.32	77·75	59·66	77.49	60·00	98
99	79.06	59·58	78·80	59.92	78·54	60·27	78.28	60·61	99
100	79.86	60·18	79·60	60.53	79·34	60·88	79.07	61·22	100
Distance.	Dep. 53	Lat. Deg.	Dep. 523/4	Lat.	Dep. 52½	Lat.	Dep. 521/4	Lat.	Distance.

1         0.79         0.62         0.79         0.62         0.78         0.62         0.78         0.63         1           2         1.58         1.23         1.57         1.24         1.57         1.24         1.56         1.25         2         2           3         2.36         1.85         2.36         1.86         2.35         1.87         2.24         1.86         3.33         3.10         3.12         2.93         3.12         2.93         3.12         2.93         3.12         2.250         4         4         3.15         2.46         3.74         2.84         3.13         2.49         3.12         2.250         4         5         3.94         3.06         3.93         3.10         3.11         3.12         2.90         4         6         6.67         7.94         5.06         6.66         6.66         6.66         6.75         6.66         6.75         6.66         6.75         6.66         6.66         7.85         6.61         7.85         6.61         7.85         6.69         7.74         5.60         7.02         5.63         9         7.02         5.63         9         1.02         1.02         1.02         1.02         1	Distance	38 1	Deg.	381/4	Deg.	$38\frac{1}{2}$	Deg.	383/4	Deg.	Distance.
2         1.58         1.23         1.57         1.24         1.57         1.24         1.56         1.25         2         3         3         1.85         236         1.86         235         1.87         2:34         1.88         3         3         4         316         2:46         314         2:48         313         2:49         312         2:30         4         4         5         3:94         3:08         3:93         3:10         3:41         3:11         3:90         3:13         5         6         4.73         3:60         4:71         3:71         4:70         3:74         4:68         3:76         6         6         6         4:73         3:60         4:93         5:46         4:38         5:76         6	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
19	2 3 4 5 6 7 8 9	1.58 2.36 3.15 3.94 4.73 5.52 6.30 7.09	1·23 1·85 2·46 3·08 3·69 4·31 4·93 5·54	1.57 2.36 3.14 3.93 4.71 5.50 6.28 7.07	1·24 1·86 2·48 3·10 3·71 4·33 4·95 5·57	1·57 2·35 3·13 3·91 4·70 5·48 6·26 7·04	1·24 1·87 2·49 3·11 3·74 4·36 4·98 5·60	1.56 2.34 3.12 3.90 4.68 5.46 6.24 7.02	1·25 1·88 2·50 3·13 3·76 4·38 5·01 5·63	2 3 4 6 5 6 7 8 9 9
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12 13 14 15 16 17 18 19	9.46 10.24 11.03 11.82 12.61 13.40 14.18 14.97	7·39 8·00 8·62 9·23 9·85 10·47 11·08 11·70	9·42 10·21 10·99 11·78 12·57 13·35 14·14 14·92	7·43 8·05 8·67 9·29 9·91 10·52 11·14 11·76	9·39 10·17 10·96 11·74 12·52 13·30 14·09 14·87	7·47 8·09 8·72 9·34 9·96 10·58 11·21 11·83	9·36 10·14 10·92 11·70 12·48 13·26 14·04 14·82	7·51 8·14 8·76 9·39 10·01 10·64 11·27 11·89	12 13 14 15 16 17 18 19
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	22 23 24 25 26 27 28 29	17:84 18:12 18:91 19:70 20:49 21:28 22:06 22:85	13:54 14:16 14:78 15:39 16:01 16:62 17:24 17:85	17·28 18·06 18·85 19·63 20·42 21·20 21·99 22·77	13·62 14·24 14·86 15·48 16·10 16·72 17·33 17·95	17·22 18·00 18·78 19·57 20·35 21·13 21·91 22·70	13·70 14·32 14·94 15·56 16·19 16·81 17·43 18·05	17·16 17·94 18·72 19·50 20·28 21·06 21·84 22·62	13·77 14·40 15·02 15·65 16·27 16·90 17·53 18·15	21 22 23 24 25 26 27 28 29
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	32 33 34 35 36 37 38 39	25·22 26·00 26·79 27·58 28·37 29·16 29·94 30·73	19·70 20·32 20·93 21·55 22·16 22·78 23·40 24·01	25·13 25·92 26·70 27·49 28·27 29·06 29·84 30·63	19·81 20·43 21·05 21·67 22·29 22·91 23·53 24·14	25·04 25·83 26·61 27·39 28·17 28·96 29·74 30·52	19·92 20·54 21·17 21·79 22·41 23·03 23·66 24·28	24·96 25·74 26·52 27·30 28·08 28·86 29·64 30·42	20·03 20·66 21·28 21·91 22·53 23·16 23·79 24·41	32 33 34 35 36 37 38 39
Dep. Lat. Dep. Lat. Dep. Lat. S	42 43 44 45 46 47 48 49	33·10 33·88 34·67 35·46 36·25 37·04 37·82 38·61	25·86 26·47 27·09 27·70 28·32 28·94 29·55 30·17	32·98 33·77 34·55 35·34 36·12 36·51 37·79 38·48	26·00 26·62 27·24 27·86 28·48 29·10 29·72 30·34	32·87 33·65 34·43 35·22 36·00 36·78 37·57 38·35	26·15 26·77 27·39 28·01 28·64 29·26 29·88 30·50	32·76 33·53 34·31 35·09 35·87 36·65 37·43 38·21	26·29 26·91 27·54 28·17 28·79 29·42 30·04 30·67	42 43 44 45 46 47 48 49
$\frac{12}{2}$ 52 Deg. 513/4 Deg. 511/2 Deg. 511/4 Deg. $\frac{12}{2}$	Distance.			-	·	<u> </u>		1		Distance.

Distance	38	Deg.	381/4	Deg.	381/2	~~~ ≨ Peg.	383/4	Deg.	\ Distance.	3
} nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.	}
51 52 53 54 55 56 57 58 59 60	40·19 40·98 41·76 42·55 43·34 44·13 44·92 45·70 46·49 47·28	31·40 32·63 33·25 33·86 34·48 35·09 35·71 36·32 36·94	40·05 40·84 41·62 42·41 43·19 43·98 44·76 45·55 46·33 47·12	31·57 32·19 32·81 33·43 34·05 34·67 35·29 35·91 36·53 37·15	39·91 40·70 41·48 42·26 43·04 43·83 44·61 45·39 46·17 46·96	31·75 32·37 32·99 33·62 34·24 34·86 35·48 36·11 36·73 37·35	39·77 40·55 41·33 42·11 42·89 43·67 44·45 45·23 46·01 46·79	31·92 32·55 33·17 33·80 34·43 35·05 35·68 36·30 36·93 37·56	51 52 53 54 55 56 57 58 59 60	· · · · · · · · · · · · · · · · · · ·
61	48.07	37·56	47.90	37·76	47·74	37·97	47·57	38·18	61	
62	48.86	38·17	48.69	38·38	48·52	38·60	48·35	38·81	62	
63	49.64	38·79	49.47	39·00	49·30	39·22	49·13	39·43	63	
64	50.43	39·40	50.26	39·62	50·09	39·84	49·91	40·06	64	
65	51.22	40·02	51.05	40·24	50·87	40·46	50·69	40·68	65	
66	52.01	40·63	51.83	40·86	51·65	41·09	51·47	41·31	66	
67	52.80	41·25	52.62	41·48	52·43	41·71	52·25	41·94	67	
68	53.58	41·86	53.40	42·10	53·22	42·33	53·03	42·56	68	
69	54.37	42·48	.54.19	42·72	54·00	42·95	53·81	43·19	69	
70	55.16	43·10	54.97	43·34	54·78	43·58	54·59	43·81	70	
71	55.95	43·71	55·76	43.96	55·57	44·20	55·37	44·44	71	~~~~~
72	56.74	44·33	56·54	44.57	56·35	44·82	56·15	45·07	72	
73	57.52	44·94	57·33	45.19	57·13	45·44	56·93	45·69	73	
74	58.31	45·56	58·11	45.81	57·91	46·07	57·71	46·32	74	
75	59.10	46·17	58·90	46.43	58·70	46·69	58·49	46·94	75	
76	59.89	46·79	59·68	47.05	59·48	47·31	59·27	47·57	76	
77	60.68	47·41	60·47	47.67	60·26	47·93	60·05	48·20	77	
78	61.46	48·02	61·25	48.29	61·04	48·56	60·83	48·82	78	
79	62.25	48·64	62·04	48.91	61·83	49·18	61·61	49·45	79	
80	63.04	49·25	62·83	49.53	62·61	49·80	62·39	50·07	80	
81	63·83	49.87	63·61	50·15	63·39	50·42	63·17	50·70	81	
82	64·62	50.48	64·40	50·77	64·17	51·05	63·95	51·33	82	
83	65·40	51.10	65·18	51·38	64·96	51·67	64·73	51·95	83	
84	66·19	51.72	65·97	52·00	65·74	52·29	65·51	52·58	84	
85	66·98	52.33	66·75	52·62	66·52	52·91	66·29	53·20	85	
86	67·77	52.95	67·54	53·24	67·30	53·54	67·07	53·83	86	
87	68·56	53.56	68·32	53·86	68·09	54·16	67·85	54·46	87	
88	69·34	54.18	69·11	54·48	68·87	54·78	68·63	55·08	88	
89	70·13	54.79	69·89	55·10	69·65	55·40	69·41	55·71	89	
90	70·92	55.41	70·68	55·72	70·43	56·03	70·19	56·33	90	
91	71·71	56.03	71·46	56·34	71·22	56.65	70.97	56.96	91	
92	72·50	56.64	72·25	56·96	72·00	57.27	71.75	57.58	92	
93	73·28	57.26	73·03	57·58	72·78	57.89	72.53	58.21	93	
94	74·07	57.87	73·82	58·19	73·57	58.52	73.31	53.84	94	
95	74·86	58.49	74·61	58·81	74·35	59.14	74.09	59.46	95	
96	75·65	59.10	75·39	59·43	75·13	59.76	74.87	60.09	96	
97	76·44	59.72	76·18	60·05	75·91	60.38	75.65	60.71	97	
98	77·22	60.33	76·96	60·67	76·70	61.01	76.43	61.34	98	
99	78·01	60.95	77·75	61·29	77·48	61.63	77.21	61.97	99	
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ζ	56	155	2851		502		666		778		817		792		695		518		
- (	57 58		5728 8598		788		$952 \\ 0.237$		07.058 $342$		24100 $384$		11 07 £ 357		976 $58257$		798 5 078		3 (
ς.	59	156	$\frac{8998}{1472}$		$\frac{3075}{361}$		10 237 523		627		384 667		639		538 538		357 357		
- 5	60	130	431	5	648		809		911		951		921		819	0	637	4 0	5 (
-5	1	8	10	8	300		79°		780		770		76°		75°	1	$74^{\circ}$	/	ζ
(	~ ~	ما		```	~~	<i>۔</i> ہہ۔	~~	یار	~ ~	~ `~	~ ~	<i>ر</i> ار		$\dot{\sim}$	~~~	Ċ.	$\sim$	<u>ٺ</u> ۔	Ν

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1	16°	17°	18°	190	200	21°	220	230	7
9 0		292 3717					374 6066		60 (
$\left\langle \begin{array}{c} 1 \\ 2 \end{array} \right $	9170 276 1965	6499 9280	2936 5702	8432 3261182	2935 5668	6395 9110	8763 375 1459	9989	59 } 58 }
3	4761	·293 2061	8468	3932		359 1825	4156	5343	57
(4	7556		·310 1234	6681	•343 1133	4540	6852	8019	56
5	277 0352	7623	3999	9430	3865	7254		*392 0695	55 5
$\begin{pmatrix} 6 \\ 7 \end{pmatrix}$	5941	·294 0403 3183	6764 9529	·327 2179 4928	6597 9329	360 2682	·376 2243 4938	3371 6047	54 5
8	8736		·311 2294	7676	344 2060	5395	7632	8722	.52
9	278 1530	8743	5058	$\cdot 3280424$	4791	8108	377 0327	393 1397	51 )
10	4324	295 1522	7822	3172	7521	·361 0821	3021	4071	50 }
) 11	7118	4302	312 0586	5919 8666	345 0252	3534	5714	6745	49
$\begin{cases} 12 \\ 13 \end{cases}$	9911	7081 9859	3349 6119	329 1413	2982 5712	6246 8958	8408 378 1101	9419	48 \
(14	5497	296 2638	8875	4160	8441		3794	4766	46
( 15	8290		313 1638		346 1171	4380	6486	7439	45 <
( 16	280 1085	8194	4400	9653 -330 2398	3900 6628		9178 $3791870$	·395 0111 2783	$\frac{44}{43}$
\ \frac{17}{18}	8875 6667	297 0971 3749	9925		9357	363 2512		5455	42
19	9459		314 2686		347 2085	5222	7253	8127	41 )
20	281 2251	9303	5448	331 0634	4812	7932	9944	396 0798	40
21	5042				7540		380 2634	3468	39 )
22	7833		315 0969				5324 8014	6139	38
$\begin{cases} 23 \\ 24 \end{cases}$	282 0624 3415	7632 ·299 0408		332 1611	2994 5720		381 0704	8809 397 1479	36
25	6205								35 (
26	8995								34 (
$\begin{cases} 27 \\ 28 \end{cases}$	283 1785			9841 333 2584	3898 6624		8770 382 1459		33 )
28	4575 7364					366 2306		4823	31
30	284 0158	1	1	1		1	i .	1 1	30
31	2942				4798	7719	9522		29 \
32	5731					367 0425			28
$\begin{cases} 33 \\ 34 \end{cases}$	8520 285 1308		318 1321		351 0246				$\begin{vmatrix} 27 \\ 26 \end{vmatrix}$
35		302 0926							25
36	6884	3699	9598	4516		368 1246		3490	24 )
37	9671		319 2350		352 1139				$\begin{vmatrix} 23 \\ 22 \end{vmatrix}$
38	286 2458 5246							8821 401 1486	$\begin{vmatrix} 22\\21 \end{vmatrix}$
/	1				1		1	1	20
5 40 41	8032				9300	369 2061 4763			19
42	360							9478	18 (
43	6391	3102	888			370 0170			j 17 🕻
(44	9177	5875			354 019			4804	16 (
2 45 46	288 196 474								15 7
47	753							1 2791	13)
( 48	289 031	8 695	3 322 265	7379	355 107	0 367	8 515	6 5453	12 5
49	310	972	3 541	1	,-	1	1		1 /
50	588							8 404 0775	
51	867					6 372 178			
52									
54							8 389 124		
> 55	980	5 633	4 324 192	653	1 357 009	7 373 257			
> 56									
57			$\begin{vmatrix} 9 & 742 \\ 6 & 325 & 018 \end{vmatrix}$			1 797 8 374 067			
59					8 358 096				
2 60	371	7 309 017	0 568	2 342 020	1 367	9 606	6 731	1 7366	0 (
~ { /	73°	72°	710	700	690	680	670	660	1/3
2	~~~	~~~	$\dot{\sim}$	$\dot{\sim}$	٠~~	$\dot{\sim}\sim$	$\dot{\sim}\sim$	$\dot{\sim}\sim$	<u> </u>

				NAT. S	SINE.				95
(~	$\widetilde{24^{\circ}}$	$\widetilde{25^{\circ}}$	$\sim_{26^{\circ}}$	$\phantom{aaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaa$		29°		$\sim 31^{\circ}$	73
5 0		·422 6183 8819	438 3711	·453 9905 ·454 2497	469 4716	·484 8096 ·485 0640	•500 0000 2519	515 0381 2874)	60 \ 59
$\begin{cases} \frac{1}{2} \end{cases}$	407 0024 2681	423 1455	8940	5088	9852	3184	5037	5367	58
( 3	5337		439 1553		470 2419	5727	7556	7859	57
$\begin{pmatrix} 4 \\ 5 \end{pmatrix}$	7993 ·408 0649	6725 9360	4166 6779	·455 0269 2859	4986 7553	·486 0812	·501 0073	2842	56 ) 55 \
6		$\cdot 4241994$	9392	5449	471 0119	3354	5107	5333	54 \
5 7	5960		440 2004	8038	2685		7624 502 0140	7824	53 (
8 9	8615 •409 1269	7262 9895	$\frac{4515}{7227}$	·456 0627 3216	5250 7815	487 0977	2655	2804	$\begin{array}{c} 52 \\ 51 \end{array} \}$
10	3923		9838	- 1	472 0380		5170	5293	50
(11	6577	5161	·441 2448	8392	2944	6057	7685	7782	49 (
$\begin{pmatrix} 12 \\ 13 \end{pmatrix}$	9230	7793	5059 7668	·457 0979 3566	5508	8597 488 1136	·503 0199 2713	·518 0270 2758	48 }
13	4536		·442 0278		4730634			5246	46
) 15	7189	5687	2887		3197	6212	7740	7733	45
$\begin{cases} 16 \\ 17 \end{cases}$	9841	8318 427 0949	5496 8104	·458 1325 3910	5759 8321	8750 -489 1288	·504 0252 2765	519 0219 2705	$\frac{44}{43}$
18	5144		·443 0712		474 0882	3825	5276	5191	42 (
( 19	. 7795	1 1		9080	3443			7676	41 (
5 20	412 0445	8838		459 1665	6004		·505 0298 2809		40 S
$\begin{cases} 21 \\ 22 \end{cases}$	5745	·428 1467 4095	8534 •444 1140		•475 1124	·490 1433 3968	5319	2646 5130	38
23	8395	6723	3746	9415	3683	6503	7828	7613	37
$\left\langle \begin{array}{c} 24\\ 25 \end{array} \right $	413 1044	9351 $4291979$	6352 8957	·460 1998 4580	6242	9038 491 1572	·506 0338 2846	$521\ 0096 \ 2579$	36
26	6342		445 1562		·476 1359	4105		5061	34
( 27	8990	7233	4167	9744	3917			7543	
$\begin{cases} 28 \\ 29 \end{cases}$	414 1638	9859 •430 2485	6771 9375	·461 2325 4906	6474 9031	9171 $4921704$	507 0370 2877	522 0024 2505	$\begin{vmatrix} 32 \\ 31 \end{vmatrix}$
30	6932		446 1978	1 1	·477 1588		1	ł	I \
31	9579	7736	4581	.4620066	4144	6767	7890	7466	29
32	415 2226 4872	·431 0361 2986	7184 9786		6700	9298 $4931829$	•508 0396	$9945$ $\cdot 523\ 2424$	
33	7517	5610	·447 2388		478 1810				26 5
35	416 0163				4364 6919		7910 509 0414	7381 9859	
36	5453	·432 0857 3481	$7591$ $\cdot 448\ 0192$			2 494 1948		524 2336	
38	8097	6103	2792	8115	479 2026	4476	5421	4818	22 2
39	417 0741	1		464 0692	4579	1	1	1	1 (
40	3385 6028		7992 ·449 0591		713	9532 3 <b>495</b> 2060	510 0426	9760 525 2241	
42	8671		3190		480 223				
3	418 1313			465 0996					
44 45	* 3956 6597		8387 •450 0984		7337 988	9039	511 0431	9665 •526 2130	
46	9233	7072	3582	8719	·481 2438	4690	5431	4618	14 (
47	419 1880			-466 1293 3866	4987 7537		7930 512 0429		
48	4521 7161		8778 451 1372		482 0086	6 497 2264			
50	9801	1	1		l .	1	1		1
) 51	·420 2441	436 0166	6568	467 1584	5189				
52			9158 452 175			9833 7 <b>498 2</b> 353	3 513 0420	9448 5-528 1914	
54			4347	9298	282	4877	5413	438	6 5
( 55	2996	437 0634	6941	468 1869	5370				
56	5634 8272		9538 453 2128			9920 2 499 2441	514 0404 2899	9325 9-529 1790	
58	422 0909	8482	4721	9578	3007	4961	l) 5393	4258	2)
59		438 1097		469 2147 4716			l 7887 0 ·515 0381		
60	6188 65°	8711 64°	9908 63°	620	610	600	290 0381	580	1 73
(	1000	\ \ \	1 000	0000	000	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	ممما	~~~	رکہ

96 NAT. SINE.

90				MAI.	INE.				
50	$\widetilde{32^{\circ}}$	$\widetilde{33}$	$\widetilde{34^{\circ}}$	$\widetilde{_{35}}$	$\widetilde{36^{\circ}}$	$\sim_{37}\sim_{1}$	$\sim_{38}\sim_{1}$	$\widetilde{39}$	$\sim$
0	529 9193	544 6390	559 1929	573 5764			615 6615	629 3204	60 ?
) 1	530 1659	8830	4340		588 0206	602.0473	8907	$\frac{5464}{7724}$	59 ) 58 )
$\left\langle \begin{array}{c} 2\\3 \end{array} \right $	412a 6591	545 1269 3707	6751 9162	574 0529 2911	$2558 \\ 4910$	2795 5117	616 1198 3489	9983	57
( 4	9057		560 1572	5292	7262	7439		630 2242	56 \
, 5	531 1521	8583	3981	7672	9613	9760	8069	4500	55
6.	3980 6450	546 1020 3456	6390 8798	575 0053 2432	4314	·603 2080 4400	617 0359 2648	6758 9015	$\frac{54}{53}$
5 8	8913		561 1206	4811	6663	6719		631 1272	52
9	5321376	8328	3614	7190	9012	9038	7224	3528	51 )
10		.547 0763	6021		590 1361	.604 1356	9511	5784	50 )
11	6301	3198		·576.1946 4323	3709	3674 5991	618 1798	8039 632 0293	49 )
$\begin{cases} 12 \\ 13 \end{cases}$	8763 -533 1224	8066	5620834 $3239$	6700	6057 8404	8308	6370	2547	47
(14	3685	-5480499	5645	9076	·591 0750	605 0624	8655	4800	46 (
(15	6145	2932	8049		3096	2940		7053	45
$\frac{16}{17}$	8605 534 1065	5365 7797	$563\ 0453\ 2857$	3827 6202	5442 7787	5255 7570	3224 5507	9306 633 1557	$\frac{44}{43}$
18	3523	549 0228	5260		·592 0132	9884	7790	3809	42 >
) 19	5982	2659	7663	578 0950	2476	606 2198	!	6059	41 >
20	8440		564 0066	3323	4819	4511	2355	8310	40
$\left\langle \begin{array}{c} 21 \\ 22 \end{array} \right $	·535 0898 3355	7520 9950	2467 4869	5696 8069	7163 9505	6824 9136	4636 6917	·634 0559 2808	39 }
23	5812		7270		·593 1847	607 1447	9198	5057	37 (
24	8268	4807	9670	2812	4189				36 (
$\begin{cases} 25 \\ 26 \end{cases}$	536 0724 3179	7236 9663	·565 2070 4469	5183 7553	6530 8871			9558 635 1800	$\begin{vmatrix} 35 \\ 34 \end{vmatrix}$
27	5634		6868		.594 1211				33
28	8089	4518	9267	·580 2292	3550	2998			32 >
29	537 0543	00	.566.1665	4661	5889	1		1	31 >
30	2996		4062 6459		8228 595 0566				30 >
32	5449 7902			581 1765	2904	609 2229			28
33	538 0354	6645	567 1252	4132	5241	4535	623 1974	7513	27 (
$\begin{cases} 34 \\ 35 \end{cases}$	2806 5257		3648 · 6043		7577 9913				$\begin{vmatrix} 26 \\ 25 \end{vmatrix}$
36	7708	3915	8437	582 1230	$\cdot 5962249$	610 1452	8796	4240	24 )
37	539 0158	6338	568 0832				624 1069		23 )
$\begin{cases} 38 \\ 39 \end{cases}$	2608 5058		3225 5619					8721 1.638 0961	$\begin{vmatrix} 22 \\ 21 \end{vmatrix}$
/		1	8011			1	1	1	20
$\begin{pmatrix} 40 \\ 41 \end{pmatrix}$	7507 9954	3603 6024	.569 0403			611 0666 2969	625 015		
42	540 240	8444	2795	5412	625	1 5270	242	7678	18 (
43	485		5187						
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	7298 9748		9968		598 0918 324				
46	541 219		570 2357		557	7 4478	626 150		14 /
47	4637								
48	708: 952								
50			571 191		1	ı		1	1 /
( 51									
( 52								2 641 0032	8 (
2 53 2 54									
55									
) 56	662	558 2279	622	843	885	4 744	2 415	7 8958	4)
57	906				601 117	973 3 ·615 202			
59									
( 60	639	0.5591929	576	785	815	0 661	629 320	4 7876	0 (
₹/	570	560	55°	540	53°	52°	51°	50°	1/3
h	~~~	^~~	~~	~~~	~~~	~~~	~~~	~~~	$\sim\sim$

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0	642 7876	656 0500 ·	000 7000			707 1069	-710 920S	791 9597	60 (
1	612 0104	2785	2469	681 9984 682 2111 4237	9676 9676	3124	·719 3398 5418	5521	59
2	2332	4980	5628	4937	695 0767	5180	7438	7503	58 }
3	4559	7174	7789			7236		9486	57
4	6785	9367	9948	-6460	4040	0.901	790 1476	.782 1467	56 )
5	9011	657 1560	670 2108	683 0613	7039	.708 1845	3494	3449	55
6	644 1236	3752	4266	2738 4861	9128	3398	5511	5429	54
7	3461	5944	6424	4861	696 1213	708 1345 3398 5451	7528	7409	53 (
8	5685	8135	8582	6984	330	7504	9544	9388	52 (
9	7909	658 0326		6984 9107	5399	9556	$\cdot 7211559$	.733 1367	51 (
10	645 0132	2516		684 1229		709 1607			50 (
ii	2355	4706	5053	9350	056	3657	5580	5299	49
12	4577	6895	2001	3350 5471	697 165	5707	5589 7602 9615 722 1628 3640	7200	48
13	6798	9083	9361	5471 7591 9711	272	7757	9615	0275	47
14		659 1271		0711	500	0806	1799 1698	734 1250	46
15	646 1240	3458	2888	·685 1830 3948	700	1.710 1854	3640	3225	45
16	3460	5645	5000	3048	008	3901	5651	5199	44
17	5679	7831	7973	8086	998 698 207 415	1 5045	7661	7173	43
18	7808	660 0017	679 0195	818/	415	7005	7661 9671	9146	42
19	647 0116	2202	9976	.686 0300	805	1 .711 0041	723 1681	735 1115	41
20									1
	2334		4427	2410	831	5 2086			
$\frac{1}{22}$	4551		6577		699 039				39 (
23	6767		8727	6647			7705		38 2
		661 0936			455	5 8218	9712		
24	648 1199			687 087			724 1719	7730 0971	36
$\frac{25}{26}$	3414	5300	5172			1 2303	3724		
	5628	7482	7319		1 700 078				34 5
$\begin{pmatrix} 27 \\ 28 \end{pmatrix}$	7842	9662	9466	7213	286		7734		33 (
$\frac{28}{29}$		662 1842		932	494	2 8420	9738	8842	32 (
	2268			688 143			725 1741		
( 30	4480			354	909	3 250			
} 31	6692				701 116				
32		663 0557		776	5 324	1 658	1 7747	6703	28 >
33	650 1114	2734	2333	987	531	4 861	9748	8666	27 )
34	3324	4910	4476	689 198	1 738	7 714 065	5 726 1748	1.738 0629	26 \
35	5533	7087	6618	408		9 269	1 3748		
36	7742	9262	8760	619	$5   \cdot 702158$	1 472	7 5747	4552	24 (
37		664 1437	677 0901	830 690 040	2 - 360	1 676	2 7745	6515	23 (
38	651 2158		3041	690 040	7 567	2 879	6 9743	8475	22 /
39	4366	i 5785	1 5181	251	2   774	1 715 083	2 7745 6 9745 0 727 1740 3 3736	739 0485	21 )
40	6572	7959	7320 9459 -678 1597	461	7 08	1 286	3 3736	2394	20
41		665 0131	9450	672	1.703 185	9 489	5 5732	4353	19
\$ 42	652 0984	2304	678 1597	882	1 396	7 692			
43	3189	4475	3784	691 092			9 972	8268	17 5
44	5394		5871	302	9 809	1-716 098	9 728 1710	3 740 022	16
(45	7598		8007	513	1 704 01	17 301	9l 3710	218	
7 46		666 0987	679 0149		2 22		9 570	4137	
247	653 2004	3156	2278	933	2 42			609	
348	4206		4419	692 143	2 63	12 910	6 968	6 804	12)
49	6408		6547		1 84	6 -717-119	4 729 167	7 741 000	
50	8609		1		01.705 04				
51					25	32 518			
52		0 667 1828 3994					3 764		
53	3010			$ \begin{array}{c c} 6 & 982 \\ 693 & 192 \end{array} $				5 780	
54	5209 7408				90 em	16.710 100	$\frac{3}{3}$ 730 $\frac{9}{162}$	3 975	
55		7 668 0490		0 401	4 706 07	76 328	27 261	0.742170	š   ž )
56			681 146						
57	4005		001 140	$9 \cdot 694 \cdot 030$					
58	619	698		ما ممد		53 93			
59	839		1 785 3 998	6 440	1 00	11 -710 12	77 781 155	3 950	9 1 5
60	-856 DED	0 669 1306	3 000	4 650	34 -707 10	68 110 19	77 ·781 155	7.743144	8 0 5
700	400	1009 1000	470	460	10110	110	190	190	ຶ  ັ⁄ ໄ
7'	1 490	48° ∼~~~	1 41	400		$44^{\circ}$	45	420	1')
\~	$\sim \sim$	~~~	~~~	~~~	~~~	~~~	~~~	$\sim\sim$	~~
	9			NAT.	COSINE		Hosted by	Goo	gle
									9,
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(	~1	$\sim_{\widetilde{48}^{\circ}}\sim_{\widetilde{1}}$	$\widetilde{49}^{\circ}$	$\sim \widetilde{50}^{\circ}$	$\widetilde{51}^{\circ}$	$\widehat{52^{\circ}}$	$\widetilde{53^{\circ}}$	$\sim_{54^{\circ}}$	$\tilde{r}$	ζ
<	0	743 1448	754 7096	766 0444	777 1460	788 0108	·798 6355	809 0170	60	ζ
(	1	3394	9004	2314	3290	1898	8105	1879	59	ζ
(	2	5340	755 0911	4183	5120	3688	9855	3588	58	ζ.
<	3 4	7285 9229	2818   4724	6051 7918	6949   8777	5477 7266	·799 1604   3352	5296 7004	57 56	ζ
(	5	744 1173	6630	9785	·778 0604	9054	5100	8710	55	ζ.
(	6	3115	8535	767 1652	2431	·789 0841	6847	·810 0416	54	(
(	7	5058	·756 0439	3517	4258	2627	8593	2122	53	(
(	8	6999	2342	5382	6084	4413	800 0338	3826	52	(
(	9	8941	4246	7246	7909	6198	2083	5530	51	(
	10	$\cdot 7450881$	6148	9110	9733	7983	3827	7234	50	(
	11	2821	8050	768 0973	779 1557	9767	5571	8936	49	(
	12	4760 6699	9951	2835 4697	3380 5202	·790 1550 3333	7314   9056	·811 0638   2339	48 47	ζ.
	$\frac{13}{14}$	8636	·757 1851 3751	6558	7024	5115	801 0797	4040	46	<
	15	·746 0574	5650	8418	8845	6896	2538	5740	45	ζ.
ζ.	16	2510	7548	·769 0278	·780 0665	8676	4278	7439	44	(
(	17	4116	9446	2137	. 2485	791 0456	6018	9137	43	(
(	18	6382	.758 1343	3996	4304	2235	7756	·812 0835	42	(
(	19	8317	3240	5853	6123	4014	9495	2532	41	(
(	20	·747 0251	5136	7710	7940	5792	·802 1232	4229	40	(
	$\frac{21}{22}$	2184 4117	7031 8926	9567 $7701423$	9757 •781 1574	7569 9345	2969 4705	5925 7620	39 38	5
	23	6049	·759 0820	3278	3390	·792 1121	6440	9314	37	ς
(	24	7981	2713	5132	5205	2896	8175	·813 1008	36	5
(	25	9912	4606	6986	7019	4671	9909	2701	35	ς.
(	26	7481842	6498	8840	8833	6445	$\cdot 8031642$	4393	34	5
(	27	3772	8389	771 0692	782 0646	8218	3375	6084	33	(
ζ.	28 29	5701 7629	·760 0280	2544	2459 4270	9990 793 1762	5107 6838	7775 9466	32 31	ς
ζ			2170	4395				1		5
ζ	30 31	9557 •749 1484	4060 5949	6246 8096	6082 7892	3533 5304	8569 804 0299	·814 1155 2844	30 29	5
ς	32	3411	7837	9945	9702	7074	2028	4532	28	5
-5	83	5337	9724	7721794	783 1511	8843	3756	6220	27	5
- 5	34	7262	761 1611	3642	3320	•794 0611	5484	.7906	26	)
>	35	9187	3497	5489	5127	2379	7211	9593 ·815 1278	25 24	)
>	36 37	·750 1111 3034	5383 7268	7336 9182	6935 8741	4146 5913	. 8938 -805 0664	2963	23	)
)	38	4957	9152	773 1027	784 0547	7678	2389	4647	22	>
5	39	6879	762 1036	2872	2352	9444	4113	6330	21	5
-5.	40	8800	2919	4716	4157	·795 1208	5837	8013	20	5
5	41	751 0721	4802	6559	5961	2972	7560	9695	19	5
- 5	42	2641	6683	8402	7764	4735	9283	·816 1376	18	١).
-5.	43	4561	8564	774 0244	9566	6497	-806 1005	3056	17	)
5	44	6480	$\cdot 7630445$	2086	785 1368	8259	2726	4736	16	5
- >	45	8398	2325	3926	3169	•796 0020	4446	6416 8094	15 14	5
>	$\frac{46}{47}$	752 0316 2233	4204 6082	5767 7606	4970 6770	1780 3540	6166 7885	9772	13	)
- >	48	4149	7960	9445	8569	5299	9603	817 1449	12	)
- >	$\frac{1}{49}$	6065	9838	775 1283	·786 0367	7058	807 1321	3125	11	
->	50	7980	764 1714	3121	2165	8815	3038	4801	10	
	51	9894	3590	4957	3963	797 0572	4754	6476	9	
)	52	753 1808	5465	6794	5759	2329	6470	8151	8	$\rangle$
$\rangle$	53	3721	7340	8629	7555	4084	8185	9824	7	$\rangle$
$\rangle$	54	5634	9214	776 0464	9350 •787 1145	5839	9899	·818 1497 3169	5	$\rangle$
$\rangle$	55 56	7546 9457	.765 1087 2960	2298 4132		7594 9347	3325	4841	4	)
$\rangle$	57	754 1368	4832	5965	4732		5037	6512	3	)
$\rangle$	58	3278	6704	7797	6524	2853	6749	8182	2	)
$\rangle$	59	5187	8574	9629	8316	4604		9852	1	
~	60	7096	766 0444	.777 1460				819 1520	0	7
?	/	410	40°	390	380	37°	360	. 35°	1 '	- )
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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
0   -819 1520   -829 0376   -838 6706   -848 0481   -857 1673   -866 0254   -874 61	
) 1   3189   2002   8290   2022   3171   1708   76	507   59 💚
	016 58
3 6523 5252 839 1455 5102 6164 4614 875 04	
	332 56
	239   55 \
	345   54 ( 351   53 )
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10 8170 6607 2513 5860 6619 4762 876 09	263   50 >
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( 15   6469   4696 841 0390   3522   4064   1988   7:	268 45 (
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\[ \begin{array}{c c c c c c c c c c c c c c c c c c c	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
	858 41
	254 40
	649   39 }
	043   38   437
	830   36
(25   3015   833 0822   6091   8793   8901   6386   878 1	222   35 (
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
	394 32
	783   31 }
	171   30 }
	$559   29 \rangle 946   28 \rangle$
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
(34 7847 5275 844 0161 2475 2191 9281 3	717 26 (
	102   25 (
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
	251 22
59 6062 3279 7952 854 0051 9549 6419 880 0	
	014 20
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
	$\frac{114}{152}$ $\frac{13}{17}$
(44   4260 836 1266 5726 7609 6889 3538 7	530 16 (
	907   15 (
\[ \begin{array}{c c c c c c c c c c c c c c c c c c c	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
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	409   11 \
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	527   8 \ 898   7
\$\langle 54 \cdot \cdot \cdot \cdot 2828 \cdot 0603  \tau 187 \cdot \cdot 847 \tau 219  \tau 2671  \tau 1514  \tau 7722 \cdot \cdot 882 \tau \tau 187  \tau 187 \	269 6
	638 5
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	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
59 8749 5121 8939 857 0174 8799 4786 8	110 1
60   829 0376   6706   848 0481   1673   866 0254   6197   9	476 0
\[ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	

	68° 927 1839 2928 4016	√ 60 }
\[ \begin{array}{c c c c c c c c c c c c c c c c c c c	2928	
		59 5
(3   3569   4024   1763   6762   9001   8455	5104	57
4 4933 5342 3035 7989 914 0181 9589	6191	56 }
$\left. \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7277 8363	55 }
7 9017 9291 6848 1665 3718 2986	9447	53
8   884 0377   892 0606   8117   2888   4895   4116   9	928 0531	52 (
9 1736 1920 9386 4111 6072 5246	1614	51
$\left\{ egin{array}{cccccccccccccccccccccccccccccccccccc$	2696 3778	50 \
(12   5810   5858   3188   7775   9597   8632	4858	48 /
(13 7166 7169 4453 8995 915 0770 9758	5938	47
\[ \begin{array}{c c c c c c c c c c c c c c c c c c c	7017 8096	$\frac{46}{45}$
) 16   885 1230   893 1098   8246   2649   4286   3134	9173	44 \
	929 0250	43
\[ \begin{array}{c c c c c c c c c c c c c c c c c c c	$1326 \\ 2401$	42 {
20 6639 6326 3292 7511 8963 7624	3475	40 (
21 7989 7632 4551 8725 916 0130 8745	4549	39 (
22     9339     8936     5810     9938     1297     9865       23     866 0688     894 0240     7068     909 1150     2462     923 0984	5622 6694	38 3
24 2036 1542 8325 2361 3627 2102	7765	36 )
25 3383 2844 9582 3572 4791 3220 26 4730 4146 902 0838 4781 5955 4336	8835	35
	9905	$\begin{vmatrix} 34 \\ 33 \end{vmatrix}$
(28) 7420 6746 3347 7199 8279 6567	2042	32 (
29 8765 8045 4600 8406 9440 7682	3109	31 3
30     887 0108     9344     5853     9613     917 0601     8795       31     1451     895 0641     7105     910 0819     1760     9908	$\frac{4176}{5241}$	$\begin{vmatrix} 30 \\ 29 \end{vmatrix}$
32 2793 1938 8356 2024 2919 924 1020	6306	28 >
33 4134 3234 9606 3228 4077 2131 34 5475 4529 903 0856 4432 5234 3242	7370 8434	$\begin{vmatrix} 27 \\ 26 \end{vmatrix}$
35 6815 5824 2105 5635 6391 4351	9496	25
36 8154 7118 3353 6837 7546 5460 37 9492 8411 4600 8038 8701 6568	·931 0553 1619	$\begin{vmatrix} 24 \\ 23 \end{vmatrix}$
38 888 0830 9703 5847 9238 9855 7676	2679	$\begin{vmatrix} 23 \\ 22 \end{vmatrix}$
39 2166 896 0994 7093 911 0438 918 1009 8782	3739	21 )
40         3503         2285         8338         1637         2161         9888	4797	20 (
\[ \begin{array}{c c c c c c c c c c c c c c c c c c c	5855 6912	19 }
) 43   7506   6153   2068   5229   5614   3201	7969	17 5
44 8839 7440 3310 6425 6763 4303	9024	16
45   889 0171   8727   4551   7620   7912   5405   6506   6506	·932 0079 1133	15
47 2834 1299 7032 912 0008 919 0207 7606	2186	13 (
48     4164     2584     8271     1201     1353     8706       49     5493     3868     9509     2393     2499     9805	3238 4290	12 /
49 5493 3868 9509 2393 2499 9805 50 6822 5151 905 0746 3584 3644 926 0902	5340	10
51 8149 6433 1983 4775 4788 2000	6390	9
52 9476 7715 3219 5965 5931 3096	7439	8
\[ \begin{array}{c c c c c c c c c c c c c c c c c c c	8488 9535	6
55 3453 1555 6922 9529 9356 6380	·933 0582	5 (
( 56   4777   . 2834   8154   913 0716   920 0496   7474	1628	4 (
6         57         6100         4112         9386         1902         1635         8566         8566         3087         2774         9658	2673 3718	3 (
59 8744 6665 1848 4271 3912 927 0748	4761	1 2
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	5804 21°	0
~ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	~~~	لــُــــــــــــــــــــــــــــــــــ

~	$\sim$	$\sim\sim\sim$	$\sim\sim\sim$	$\sim\sim\sim$	$\sim\sim\sim$	$\sim\sim\sim$	$\sim\sim\sim$	$\sim\sim\sim$	$\sim$
5	1	690	70°	710	720	73°	740	75°	1)
)	0	933 5804	939 6926	945 5186	951 0565	.956 3048	961 2617	965 9258	60
5	ĭ	6846	7921	6132	1464	3898	3418	966 0011	59
(	2	7388	8914	7078	2361	4747	4219	0762	58
1	2	8928	9907	8023	3258	5595	5019	1513	57
7	4	9968	•940 0899	8968	4154	6443	5818	2263	56
)			1891	9911	5050	7290		3012	55
5	5	934 1007				8136	6616		
(	6	2045	2881	946 0854	5944		7413	3761	54
(	.7	3082	3871	1795	6838	8981	8210	4508	53
7	8	4119	4860	2736	7731	9825	9005	5255	52
)	9	5154	5848	3677	8623	·957 0669	9800	6001	51.
5	10	6189	6335	4616	9514	1512	962 0594	6746	50
ζ.	îĭ	7223	7822	5ี้อี้อี้อี้	952 0404	2354	1387	7490	49
(	12	8257	8808	6493	1294	3195	2180	8234	48
7	13	9289	9793	7430	2183	4035	2972	8977	47
)	14	935 0321	941 0777	8366	3071	4875	3762	9718	46
)	15	1352	1760	9301	3958	5714	4552	967 0459	45
5		2382	2743	9301		$\frac{5714}{6552}$		1200	44
(	16	3412	3721		4844	7389	5342	1939	43
7	17			1170	5730	7589	6130		
7	18	4440	4705	2103	6615	8225	6917	2678	42
)	19	5468	5686	3035	7499	9060	7704	3415	41 >
5	20	6495	6665	8966	8382	9895	8490	4152	40 )
(	21	7521	7644	4897	9264	958 0729	9275	4888	39
(	$\overline{22}$	8547	8621	5827	.953 0146	1562	963 0060	5624	38.
?	23	9571	9598	6756	1027	2394	0843	6358	37 (
)	24	936 0595	.942 0575	7684	1907	3226	1626	7092	36
)	$\frac{25}{25}$	1618	1550	8612	2786	4056	2408	7825	35
ς	26	2641	2525		3664	4886	3189	8557	34
(				9538					33
1	27	3662	3498	948 0464	4542	5715	3969	9288	
)	28	4683	4471	1389	5418	6543	4748	.968 0018	$\begin{vmatrix} 32 \\ 21 \end{vmatrix}$
)	29	5703	5444	2313	6294	7371	5527	0748	31 }
5	30	6722	6415	3237	7170	8197	6305	1476	30 )
(	31	7740	7386	4159	8044	9023	7081	2204	29 \
7	32	8758	8355	5081	8917	9848	7858	2931	28 (
{	33	9774	9324	6002	9790	-959 0672	8633	3658	27
>	34	·937 0790	.943 0293	6922	954 0662	1496	9407	4383	26 7
)	35	1806	1260	7842	1533	2318	.964 0181	5108	25 /
5	36	2820	2227	8760	2403	3140	0954	5832	24
(	37	3833	3192	9678	3273	3961	1726	6555	23
(	38	4846	4157	949 0595	4141	4781	2497	7277	22
7	39	5858	5122	1511	5009	5600	3268	7998	21 (
)		1		t .	ş.	1		-	. /
5	40	6869	6085	2426	5876	6418	4037	8719	20
ς.	41	7880	7048	3341	6743	7236	4806	9438	19 \
(	42	8889	8010	4255	7608	8053	5574	·969 0157	18 (
7	43	9898	8971	5168	8473	8869	6341	0875	17 (
)	44	-938 0906	9931	6080	9336	9684	7108	1593	16 /
)	45	1913	•944 0890	6991	.955 0199	0499	7873	2309	15
ς	46	2920	1849	7902	1062	960 1312	8638	3025	14 )
(	47	3925	2807	8812	1923	2125	9402	3740	13 5
7	48	4930	3764	9721	2784	2937	965 0165	4453	12
)	49	5934	4720	950 0629	3643	3748	0927	5167	۱ii 〈
)						1		1	1 /
ς	50	6938	5675	1536	4502	4558	1689	5879	10 5
(	51	7940	6630	2443	5361	5368	2449	6591	9 5
1	.52	8942	7584	3348	6218	6177	3209	7301	8 (
)	53	9943	8537	4253	7074	6984	3968	8011	7 (
)	54	939 0943	9489	5157	7930	7792	4726	8720	6 2
5	55	1942	945 0441	6061	8785	8598	5484	9428	5
(	56	2940	1391	6963	9639	9403	6240	970 0135	4
7	57	3938	2341	7865	956 0492	961 0208	6996	0842	3 5
7	58	4935	3290	8766	1345	1012	7751	1548	2 3
)									1 i
5	59	5931	4238	9666	2197	1815	8505	2253	; )
(	60	6926	5186	951 0565	3048		9258	2957	1 ? 5
(	./	20°	190	18°	170	16°	15°	14°	1' \
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ζ ο	970 2957	974 3701	978 1476	981 6272	·9848 978	•9876 883	·9902 681	60 (
( 1	3660	4355	2080	6826 7380	582 -9849 086	·9877 338 792	·9903 085 489	59 ( 58 )
$\begin{pmatrix} 2\\3 \end{pmatrix}$	4363 5065	5008 5660	2684 3287	7935	589	9878 245	891	57
) 4	5766	6311	3889	8485	9850 091	697	·9904 293	56
) 5	6466	6962	4490	9037	593	9879 148	694	55
) 6	7165	7612	5090	9587	·9851 093 593	599 9880 048	·9905 095 494	54 \
\ \ \ \ 8	7863 8561	8261 \ 8909	5689   6288	·982 0137 0686	9852 092	497	893	52
) 9	9258	9556	6886	1234	590	945	9906 290	51
10	9953	975 0203	7483	1781	·9853 087	·9881 392	687	50 (
(11	971 0649	0849	8079	2327	583	838	9907 083	49 (
( 12	1343	1494	8674	2873	9854 079	·9882 284 728	478 873	$\frac{48}{47}$
3 13	2036 2729	2138   2781	9268 9862	3417 3961	574 •9855 068	9883 172	9908 266	46
15	3421	3423	979 0455	4504	561	615	659	45
5 16	4112	4065	1047	5046	•9856 053	·9884 057	9909 051	44 \
5 17	4802	4706	1638	5587	544 •9857 035	498 939	442 832	43 (
\ \begin{array}{c} 18 \\ 19 \end{array}	5491 6130	5345 5985	2228 2818	6128 6668	524	9885 378	9910 221	41
20	6867	6623	3406	7206	.9858 013	817	610	40
21	7554	7260	3994	7744	501	9886 255	997	39 (
22	8240	7897	4581	8282	988	692	9911 384	38
23		8533	5167	8818	·9859 475 960	9887 128 564	770 -9912 155	37 36
24		9168 9802	5752 5337	9358 9888	9860 445	998	540	35
26		·976 0435	6921	.983 0422	929	·9888 432	923	34 (
( 27		1067	7504	0955	9861 412	865	•9913 306	33 (
$\begin{cases} 28 \\ 29 \end{cases}$		1699 2330	8086 8667	1487 2019	894 9862 375	9889 297 728	688 •9914 069	32 ( 31 /
30		2960	9247	2549	856	9890 159	449	30
31		3589	9827	3079	9863 336	588	828	29
32	5056	4217	·980 0405	3608	815	9891 017	9915 206	28
38		4845	0983	4136	9864 293	445 872	584 961	27 26
34		5472 6098	1560 2136	4663 5189	9865 246	9892 298	9916 337	25
36		6723	2712	5715	722	723	712	24 .
( 3)		7347	3286	6239		9893 148	9917 086	23
38		7970	3860 4433	6763 7286		572 994	459 832	22
(		8593				9894 416		20
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		9215 9836	5005 5576	7808 8330	9868 087	838	574	19
3 4		977 0456	6147	8850		9895 258	944	18
) 4:		1075	6716	9370		677	9919 314	17
(4		1693 2311	7285 7853	9889				16 15
4		2928	8420	0924				14
$\frac{1}{4}$		3544	8986	1441	897	•9897 347	782	13
( 4		4159	9552	1956				12
2	1	1	981 0116	1	1	•9898 177		.11
5 5			0680 1243					10
	2 8439		1805					8
5	3 9100	7222	2366	452	678	826	959	7
	4 9760							6
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$							5 4
	7 1734	9658	4603					3 2
) 5	8 2390	978 0265	5160	706	3 972			2
	9 3046							1 0
1	00   3701 130   3701	1476	6272 11°	100	888	80 80	$\begin{array}{c c} & 462 \\ 7^{\circ} \end{array}$	1 %
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\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	·9925 462	·9945 219	·9961 947	960	0086 205	980 888	89° 9968 477 527 577 625 673 720 766 812 856 900	60 }
$\left\{ \begin{array}{c} 1\\2\\2 \end{array} \right]$	816	523	9962 200	843	447	9994 009	527	59 }
$\left\langle \begin{array}{c} 2\\3 \end{array} \right $	·9926 169	10046 197	452	9976 045	598	110	577	58 (
3 4	873	428	954	445	898	209	673	56
5	9927 224	729	9963 204	645	9987 046	405	720	55
6 7	573 692	9947 028	453   701	•0077 040	240	502	766	54
( 8	9928 271	625	948	237	486	693	856	52
9	618	921	•9964 195	433	631	788	900	51 (
10	965   -0020 310	9948 217	440	627	775	881	942	50 (
$\begin{array}{c c} 11 \\ 12 \end{array}$	655	807	929	9978 015	·9988 061	9995 066	9999 025	48
( 13	999	•9949 101	·9965 172	207	203	157	065	47
( 14	9930 342 685	898 685	414 655	589	344 484	247	106	46 )
16	·9931 026	976	895	779	623	424	181	44 (
7 17	367	9950 266	9966135	968	761	512	218	43
19	9932 045	844	612	343	9989 035	684	289	41
20	384	·9951 132	849	530	171	770	323	40 }
( 21	721	419	•9967 085	716	306	854	357	39 \
22	393	705 990	521 555	900 084	573	9996 020	389 421	38
24	728	.9952 274	789	267	706	101	452	36
25	•9934 062	557	•9968 022	450	837	182	482	35
20	727	9953 122	485	811	9990 098	341	539	33
28	•9935 058	403	715	991	227	419	567	32 2
5 29	389	683	945	•9981 170	355	497	593	31 (
30	9936 047	962	9969 173	348 525	609	649	619	29
32	375	517	628	701	734	724	668	28
33	9937 029	·9955 070	9970 080	9982 052	983	798 871	692	26
35	355	345	304	225	9991 106	943	736	25 4
36	679	620	528	398	228	9997 015	756	24
38	326	9956 165	972	742	470	156	795	22
39	648	437	9971 193	912	590	224	813	21
40	969	708	413	9983 082	709	292	831.	20 }
( 41	+9939 290	978	633	250	827	360	847	19 (
343	928	515	9972 069	585	•9992 060	492	878	17 5
244	9940 246	783	286	751	176	556	892	16 5
45	880	9958 049	717	917	404	683	905	14
47	•9941 195	- 580	931	245	517	745	928	13
( 48	510	844	9973 145	408	629	807	939	12 (
50	020	9959 107	560	721	851	927	958	10
2 51	448	631	780	891	960	986	966	9
2 52	760	892	990	9985 050	9993 069	9998 044	973	8
54	379	9900 152	408	367	284	1 157	985	6
55	688	669	615	524	390	213	989	5 6
> 56	996	926	822	680	495	267	993	4 (
2 58	609	438	238	989	5   70	1 374	998	2
2 59	914	693	437	9986 143	80	3 426	1.0000 000	1
5 %	60 80	1 50 <sup>9±</sup>	4004	3029	2090	10	00000	11
<i>ب</i>	<b>ئ</b> ىئىر	<u>`</u> ـــَـــــٰ	· N	IAT. COSI	NE.	Hosted by	577 625 673 720 812 856 890 942 8999 984 9999 984 9999 984 289 181 218 289 323 387 389 421 452 482 482 482 482 482 668 756 776 776 813 831 831 831 831 831 831 831 831 831	

ζ	~	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	1°	2°	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	4°	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	7°	$\widetilde{\prime}$
}	0 1	·000 0000 2909		·034 9208 ·035 2120	·052 4078	·069 9268 ·070 2191	·087 4887 7818		·1227846 ·1230798	60 59
(	2		018 0370	5033	9912		088 0749	6925		58
(	้	8727	3280	7945	053 2829	8038	3681		6705	57
(	4	·001 1630		·036 0858		•071 0961		$\cdot 1062808$		56 )
(	5	4544	9100	3771		3885			124 2612	55
(	6	7453			054 1581		089 2476	8692		54 (
(	7	002 0362	4920	9596 037 2500		9733 072 2657		107 1634 4576		53 (
(	8	3271	·020 0740		.055 0333	5581	090 1273	7519		52 ( 51 (
(								108 0462		(
(	10 11	9089 003 1998	3650	$8335$ $\cdot 0381248$	3251	073 1430	7138			50 ( 49 /
(	12	4907	9470		9087	4354	091 0071			48
(	13		021 2380		056 2005	7279				47
(	14	004 0725	5291	9988	4923	0.0740203	5938	$\cdot 1092234$	9205	46
(	15	3634		0392901	7841	3128	8871		127 2161	45
(	16	6542	0221111		.057 0759		092 1804			44
ζ	17	9451	4021	8728 040 1641	3678	8979	4738 7672	110 1060	8073 128 1030	43
(	18	*005 2360 5269			6596	075 1904	093 0606			42
ζ	19	I.	1				1	1		
(	$\frac{20}{21}$	006 1087	023. 2753	041 0383	058 2434	7755	6474	111 2844		40 39
(	22	3996			8271	·076 0680	9409		129 2858	38
ζ	23		024 1484	6210	059 1190	6532	094 2344			37
ζ	24	9814		9124	4109	9458		112 1680		36
(	25	007 2723	7305	042 2038	7029	9458 077 2384	8213	4623	130 1731	35
(	$^{26}$		0250216	4952	9948	5311	./•095 1148	7571		34
(	27	8541		7866	.060 2867	8237	4084	113 0517		33
(	28 29	008 1450		043 0781 3695	5787	·078 1164 4090	7019 9955		131 0607	32 31
(		4300						1		(
(	30 31		026 1859		·061 1626 4546	9944	096 2890	9356 114 2303		30 29
(	32	009 0178	4770	044 2438		079 2871	8768	5250	0.1322444	28
Ś	33		027 0592	5358	-0620386	5798	097 1699			27
-{	34	8905		8268	3306	8726	4638	115 114		
(	35	.010 1814		045 1183		080 1653			2 133 1324	
-5	36	4724		4097	9147 063 2067		098 0509			24 23
5	37 38		·028 2236 5148			7509 081 0437			$7246 \\ 1340207$	25
ζ	39	011 0542 3451		046 2842						22
3	40			1	7	,	3:099 2257		1	20
(	41	9270	·029 0970 3882		·064 0829	9221		8832 117 178		19
(	42	012 2179		047 1588		082 2150			135 2053	
ζ	$\tilde{43}$	5088					100 1071	7679		17
(	44	7998	030 2616	7419	065 2513	8007	4009	118 0628	7978	
-{	45	013 0907		048 0334		083 0936			3 136 0940	
5	46	3817	8439							14
5	47 48	6726			·066 1278 4199		101 282	9478 119 242		
-5	48	9635 014 2545		049 1997		084 2653			3 137 2793	
-5	50	1	082 0086		067 0043	1	102 164	1		1
3	51	8364						120 1279		9
5	52	015 1273		050 0746		085 1442			138 1685	
3	53	4183		3662	8809	4372	2 103 0460	7185	2; 4650	7
ς	5.1	7093	0331734	6578	068 1732	7302	3399	121 013	3 7615	6
-5	55	016 0002				086 0233			139 0580	
-5	56	2912		051 2411						
3	57	5821		5328 8244	·069 0499 3422	902a	104 2220	8988 122 194	6510	
-5	58 59	8731 017 1641		0521161		087 1956	0101 3 8101	489	L! 9476 3 •140 2442	
-5	60	4551					105 1042			
-5	1	890	880	870	860		840		820	1
(	<u></u>	٠٠٠٠		ئمتنہ	~~~		~~~		بحتب	4
					NAT.	COTAN.		Hosted by	G00	316

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? !	80	90	100	110		10	140	150	<u>/</u> \ \
\ 0 1	140 5408 8375	158 3844	1763270 $6269$	·194 3803 6822		$\cdot 2308682 \\ \cdot 2311746$	·249 3280 6370	267 9492	60 ) 59 \
5 2	$\cdot 141 1342$	9809	9209	9841	213 1647	4811	9460	5728	58 5
3		159 2791			4688		·250 2551		57
$\begin{cases} 4\\ 5 \end{cases}$	7276 142 0243	5774 8757	5270 8270	5881	2140772	·232 0941 4007	8734	·269 1967 .5087	56 ( 55 (
( 6		·160 1740		196 1922	3814	7073	251 1826	8207	54 /
7 7	. 6179	4724	4273	4943		·233 0140		270 1328	53
3 8	9147	7708	7274	7964 197 0986	9900 215 20.11		8012 $2521106$		52 > 51
10	5084	3677	3279	4008	5988		1	271 0694	50
) 11	8053	6662	6281	7031		234 2410	7294		49 >
12	144 1022			198 0053			253 0389		$\frac{48}{47}$
$\begin{cases} 13 \\ 14 \end{cases}$	6961	162 2632 5618		3076 6109	5122 8167	8548 235 1617	6580	272 0064 3188	46
( 15	9931	8603	8295	9124	217 1213	4687	9676	6313	45 (
( 16		163 1590			4259				$\frac{44}{43}$
$\begin{cases} 17 \\ 18 \end{cases}$	5872 8842		4303 7308		·218 0353	236 0829 3900		·273 2564 5690	42
19		164 0550			3400				41 5
20	4784		3319			.237 0044		274 1945	40,
$\begin{cases} 21 \\ 22 \end{cases}$	7756 •147 0727		6324	$7274$ $\cdot 2010300$	9496				$\begin{vmatrix} 39 \\ 38 \end{vmatrix}$
23		165 2501	183 2337	3327	5593		·256 1363 4469	275 1330	37
( 24	6672	5489	5343	6354		·238 2336			36 (
$\begin{cases} 25 \\ 26 \end{cases}$	9644		8350	9381 ·202 2409	·220 1692 4742		257 0664	$7589$ $\cdot 2760719$	35 34
27	5590					239 1560			33
28	8562			8465	$\cdot 221\ 0844$	4635	9970		32
29		167 0436			3895			277 0113	31 >
30	4510 7484		3390 6399		6947 9999				30 >
32	150 0458			204 0582		6942	259 2384		28 (
$\begin{cases} 33 \\ 34 \end{cases}$	3433 6408	168 2398 5390				·241 0019 3097			27 26
35	9388				223 2211		260 1699		
36			187 1449	205 2705	5265	925	4808	$5 \cdot 279 2050$	24 )
37	5333 8303				$^{\circ}2241374$	242 233	791 261 101		
39				3 206 1801				3 -280 1459	
\$ 40	4265			1		243 157		1	20 \
5 41	723	6338	6507	7867	225 0541	465	3 262 034:	7735	19 (
$\begin{cases} 42 \\ 43 \end{cases}$	153 0213	5  9331 2  171 2325		207 0900 3934				1 281 0873 4012	
44	6170					244 0819 1 3905			
2 45	914			208 0009	226 276	698	1 263 278	282 0292	15 /
$\begin{cases} 46 \\ 47 \end{cases}$	154 212		190 1573 458			245 003			
48	808				227 194		3.·264 211		
49				7 209 2145				6 283 2857	
50						3 .246 240			
51									
53		8 ·174 228				1 ·247 166			
( 51	595	8 5279	569	6 7331	229 030	6 475	0.266079	4 8575	6 2
\ 55 56		9 8277 9 <b>175</b> 1278	871	3 ·211 0369 1 3407		$783$ $9 \cdot 248 \cdot 092$		9 ·285 1720 5 4866	
57	490						oj 702 3 •267 014		
58	788	1 727	776	6 9486	230 255	5 · 710	2 325	$7 \cdot 2861159$	2 5
\ \ \ 60				4 ·212 252 3 556		$ \begin{vmatrix} 8 \cdot 249 & 019 \\ 2 & 328 \end{vmatrix} $			
- { >	810	800	790	780	7700	760	750		1 %
1		1000			<u></u>		0000		( , , )

_	$\sim$	~~~	~~~	~~~	^~~	~~~	~~~	~~~	~~~	~
ς.	1	16°	170	180	19°	20°	210	220	230	13
5	0		305 7307				383 8640		424 4748	60 5
5	$\frac{1}{2}$	·287 0602 3751	306 0488 3670	5630	6030 9785	364 2997 6292	584 1978	3646 7031	8182 425 1610	59 58
5	3	6900	6852		·345 3040	958:		405 0417	5051	57
>	4		307 0034		6296		385 1996	3804	8487	58
>	5	3201	3218		9553	6182	5337	7191	·426 1924	55 >
>	6	6352	6402		346 2810	948(		406 0579	5361	54
>	7 8	9503	9586	327 1724 4944	6068 9327	366 2779 6079	386 2021 5364	3968 7358	8800 427 2239	53 S
?	9	5808	5957		-347 2586	9379		407 0748	5680	51
?	10	8961	1	328 1387	5846		387 2053	4139	9121	50 (
	11	290 2114		4610	9107	5981	5398	7531	·428 2563	49 2
	12	5269	5517		·348 2368	9284		·408 0924	6005	48 (
<	13	8423				368 2587	388 2091	4318 7713	9449 •429 2894	47
<	$\frac{14}{15}$	4734	310 1893 5083		8893 349 2156		5439 8787	·409 1108	6339	46 \
<	16	7890				369 2500		4504	9785	44 (
5	17	292 1047			8685		5486		430 3232	43 <
5	18	4205						410 1299	6680	42
í	19	7363		i	5216	1 '		4697	$^{431}$ $^{0129}$	41 \
5	$\frac{20}{21}$	293 0521						8097 411 1497	3579 7030	40 \ 39
)	22	3680 6839		332 0097	·351 1750 5018	371 234			432 0481	38
1	$\overline{23}$	9998			8287			8300		37
)	$^{24}$	294 3160				8967		4121703	7386	36
?	25	6321						5106		35
,	$\frac{26}{27}$	9488				5 5590 8 8908		8510 413 1915		$\frac{34}{33}$
7	28	5808			353 4640	373 2217		5321		$\frac{32}{32}$
7	29	8971	9790	334 2719	7915	5532		8728	4665	31 2
(	30	296 2135				8847		414 2136		30 2
′	31	5299							435 1583	29 (
ζ.	32 33	8464 -297 1630						8953 •415 2363		$\begin{vmatrix} 28 \\ 27 \end{vmatrix}$
3	34	4796				375 2116				26
5	35	7962		336 2134	756					25 \
	36 37	298 1129				8753 8 876 2073				$\begin{vmatrix} 24 \\ 23 \end{vmatrix}$
$\rangle$	38	4297 746								$\left \begin{array}{c} 25\\ 22 \end{array}\right>$
$\rangle$	39		1 318 179							21
)	40	380	1	- 54			8 397 2746	6257	438 2756	20
2	41	697								19
- 7	42	300 014	4 319 140	7 481						18
(	43	331					398 2858			17
- 2	44	648	$\begin{array}{c c} 6 & 781 \\ 8 \cdot 320 \ 102 \end{array}$		9  708 3 -359 036					16 \
Ò	46	301 283					8 399 2968			14
(	47	600		0 340 103	2 693	6 531		420 019	7051	13 (
(	48	917								12 (
(	49	302 235	1		1	1	3 400 3089	1		11 \
(	50	552		7 .341 077						10 (
(	51	870 303 187			9 361 008 7 337		$ \begin{vmatrix} 9841 \\ 41.401 \\ 3218 \end{vmatrix} $			
(	53									
(	54	823	2 991	2 376	5 994	9 862	9 997	416	5.4431390	65
(	55						2 402 335			55
(	$\frac{56}{57}$									
	58	776								
	59							9 424 131		
	60 (	730	7 919	7 327	6 970	2 864	0 404 026	2 474	S ·445 2287	0 >
	′	73°	72°	710	70°	690	680	670	660	11)
	<i>`</i> ~	~~~	~~~	$\sim$	~~~	~~~	~~~	~~~	~~~	$\sim\sim$

ď	$\sim$	$\sim \sim \sim \sim \sim$	$\sim \sim $	~~~~	$\sim \sim $	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~~~~	$\sim_{30}$	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	$\sim$
?	6	.445.9997	466 3077							60 2
7	1	5778	6618	488 0927	8919	-5320826	6894	7382	601 2566	59
<	$\hat{2}$		467 0161		·510 2585		555 0698		6527	58 (
(	3	446 2747	3705	8133	6252		4504 8311		·602 0490 4454	57
(	4	6236	·468 0796	489 1737	·511 3588	·533 2029	.556 2119		8419	56 ) 55 )
ζ	5 6	·447 3216	4342	8949	7259	9503			603 2386	54
5	7	6708	7890		512 0930	$\cdot 534\ 3242$		·580 0684	6354	53 🐧
5	8	$\cdot 448\ 0200$		6166	4602		557 3551		604 0323	52 (
5	9	3693	4988	9775		535 0723		8462	4294	51 4
5	10	7187			513 1950		·558 1179 4994		8266 605 2240	50 5
>	$\frac{11}{12}$	·449 0682 4178	470 2090	6997 $4920610$	5625	·536 1953	8811	.582 0139	6215	49 (
7	13	7675	9196		514 2980	5699	-559 2629		606 0192	47
7	$\tilde{14}$		$\cdot 4712751$	7838	6658	9446	6449	7930		46
?	15	4672	6306		515 0338	537 3194	560 0269	583 1828	8149	45
?	16 17	8171	9863 •472 3420	5071 8689		6943 538 0694			·607 2130 6112	44 \
7	18	5173			516 1385		-561 1738			42
(	19		473 0538	\$ 5928					4080	41 2
(	20	$.452\ 2179$	4098	9549	8755	-539 1952		.585 1335	8067	40 (
(	21	5683	7659	495 3171	$\cdot 5172441$		562 3219	5241	609 2054	39 (
(	22		474 1222	6794				9148	6043 610 0034	38 (
3	23 24	·453 2694 6201		496 0418	518 3508					37 )
3	25		475 1914	7669		-541 0740				35 \
5	26	·454 3218	5481		·519 0891	4501	. 564 2378			. 34 🤇
5	27	6728	9048	4925						33 (
5	28	3750	476 2616	.400 0107	8278 520 1974	·542 2027 5791		588 2616 6538		$\begin{vmatrix} 32 \\ 31 \end{vmatrix}$
)	29				1	1	i			30
$\rangle$	30 31	7263	9755 477 3326	5816 9449			566 1568		613 2010	29
7	32	4290			-521 3067			8289	6013	28
ે	33		$\cdot 4780472$	6717		1.544 0862	9254			27
(	$\frac{34}{35}$	4839		°500 0352 3989	·522 0468 4170		567 3098	6134 591 0058		$\begin{vmatrix} 26 \\ 25 \end{vmatrix}$
(	36		479 1197	7627			568 0791			24 (
ζ	37	458 1877	4774	$\cdot 5011266$	•523 1578	5951	L 4639	7910		
5	38	5397	8352	4906					616 0064	
(	39		480 1932	8547	1	1	569 2339	5	1	21 (
S	40	459 2439			524 2698					20 (
-5	41 42	5962	9093 481 2675	5832	·525 0117		570 0045 3899			$ \begin{array}{c} 19 \ 18 \end{array}\rangle$
5	43	460 3011		.503 3121					618 0145	17 5
>	44	6537	9842	6768	7541	548 240	571 1612	5437	4166	
>	45		482 3427							
$\rangle$	46	3591	7014 ·483 0601				9331		619 2211 6236	$\begin{vmatrix} 14 \\ 13 \end{vmatrix}$
$\langle$	$\frac{47}{48}$	462 0649			527 2402				620 0263	
2	49	4179					573 0918			
ì	50	7710	484 1368	8668	1	512	478	9084	8320	10
2	51	$\cdot 4631243$	4959	.506 2322	528 3560	891	8649	597 3030	621 2351	3 >
(	52	4776				551 270				
(	53		485 2145		529 100- 4727				6220417 $4452$	7 6
(	54	·464 1845 5382		507 3290 6948						5 3
(	56		486 2931		530 2178	7890	7999	599 278	623 2527	4 (
(	57	465 2457	6528	4267	5908	553 168	8 576 187	673		
(	58		487 0126						1 624 0607 4650	$\begin{pmatrix} 2 \\ 1 \end{pmatrix}$
(	59 60	9536			531 3364	928	8 9628 1 577 3508			
(	1	650	640	630	620	610	600	590	580	25
(		1000				\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		1000		کہا

$ \begin{bmatrix} 3 & -626 \ 0834 & 6490 \ \\ 4 & 884 \ -651 \ 0631 \ -676 \ 2028 \ \\ 5 & 8995 & 4774 \ \\ 6 & -627 \ 2988 & 8918 \ -677 \ 0599 \ \\ 7 & 7029 \ -652 \ 3064 \ \\ 4752 \ -704 \ -652 \ 3064 \ \\ 4752 \ -705 \ 32484 \ \\ 8 & -622 \ 1098 \ \\ 7211 & 8997 \ \\ 6813 \ -730 \ 1041 \ -757 \ 2090 \ -785 \ 0401 \ \\ 9 & 5155 \ -658 \ 1360 \ -678 \ 3243 \ -704 \ 1103 \ \\ 9 & 9214 \ -5515 \ \\ 11 & -629 \ 3274 \ \\ 21 & -229 \ 3274 \ \\ 22 & 7336 \ -654 \ 3817 \ \\ 23 & -5937 \ \\ 3360 \ 1399 \ 7972 \ -880 \ 248 \ \\ 34 & -655 \ 2193 \ \\ 34 & -704 \ 110$	7840 60 2658 59 2658 59 27478 58 2300 57 67 1124 56 67 1124 56 67 1124 56 67 1124 56 67 1124 56 67 1124 56 67 1125 61 118 50 6044 52 1280 51 2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2658 59 7 7478 58 57 77124 56 57 77124 56 6780 54 6114 52 1280 51 6118 50 0958 49 646 47 5493 46 5493 46 5493 44 5496 42 42 42 6905 42 5496 42
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2658 59 7 7478 58 57 77124 56 57 77124 56 6780 54 6114 52 1280 51 6118 50 0958 49 646 47 5493 46 5493 46 5493 44 5496 42 42 42 6905 42 5496 42
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2300 57 7124 56 1951 55 56 6780 54 1611 53 6444 52 1280 51 6118 50 9958 49 5801 48 0646 47 5493 46 5493 46 5493 46 5493 44 0049 43 44905 42 42 44 44 46 47 48 49 49 49 49 49 49 49 49
	7124 56 ( ) 1951 55 6 ( ) 1951 55 54 ( ) 1611 53 6444 52 ( ) 1280 51 60958 49 5801 48 ( ) 0646 47 60343 45 60343 45 ( ) 0049 43 4905 42 ( )
	1951 55 66780 54 61611 53 6444 52 1280 51 6118 50 958 49 6866 47 6493 46 60343 45 65195 44 6405 42 64 64 64 64 64 64 64 64 64 64 64 64 64
	6780 54 1611 53 6444 52 51 51 6118 50 0958 49 5801 48 75493 46 47 6343 45 6049 43 4905 42 5195 44 64 64 64 64 64 64 64 64 64 64 64 64
$ \left\{ \begin{array}{llllllllllllllllllllllllllllllllllll$	6444 52 1280 51 6118 50 0958 49 5801 48 0646 47 5493 46 6343 45 5195 44 0049 43 4905 42
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1280 51 6118 50 9958 49 5801 48 9646 47 5493 46 9343 45 5195 44 905 42
	6118 50 \ 0958 49 \ 5801 48 \ 0646 47 \ 5493 46 \ 0049 43 \ 4905 42 \ \end{array}
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0958 49 5801 48 6646 47 5493 46 65195 44 6649 43 4905 42
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5801 48 0646 47 5493 46 0343 45 5195 44 0049 43 4905 42
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0646 47 5493 46 0343 45 5195 44 0049 43 4905 42
	5493 46 0343 45 5195 44 0049 43 4905 42
( 16   631 3598 656 0447 681 3016 707 1664 6777 8769 8082	5195 44 0049 43 4905 42
	$0049 \begin{vmatrix} 43 \\ 4905 \end{vmatrix} 42$
( [7   7007] 4009  1210  0046[10±1200[701000[109.4004[010	4905 42 >
18 632 1738 8772 682 1537 708 0395 5730 7959 7524	
19   5810  657 2937   5801   4768   735 0210   762 2557   790 2248	9764 41 5
(21)	4625 40
21   633 3959   658 1271   4333   709 3504   9174   763 1759   791 1703	9488 39 5
22 8035 5441 8601 7878 736 3660 6363 6434 820	4354 38
23   634 2113   9612   684 2371   710 2250   8147   764 0969   792 1167	9222 37 5
\ 24 \ 6193 \cdot 659 \ 3785 \ 7143 \ 6680 \ 737 \ 2686 \ 5577 \ 5902 \cdot 821 \ 25 \ .685 \ 0274 \ 7960 \cdot 685 \ 1416 \ 711 \ 1009 \ 7127 \ 765 \ 0188 \ 793 \ 0640 \	4093 36 8965 35
	3840 34
27 8441 6313 9969 9772 6115 9414 794 0121	8718 33 >
	3597 32
29 6614 4673 8528 8545 5110 8649 9611	8479 31
	3364 30 X
31   4793 662 3040   7093   7320 740 4113   7893   9110   32   8885   7225 688 1379 714 1712   8618 768 2517 796 3862 825	$\begin{array}{c c} 8251 & 29 \\ 3140 & 28 \end{array}$
32 8885 7225 688 1379 714 1712 8618 768 2517 796 3862 825 33 638 2978 663 1413 5666 6106 741 3124 7144 8617	8031 27
34 7073 5601 9955 715 0501 7633 769 1773 797 3374 826	3 2925 26 (
35 639 1169 9792 689 4246 4898 742 2143 6404 8184	7821 25 2719 24
36   5267 664 3984   8538   9297   6655 770 1037 798 2895 827 37   9366   8178 690 2832 716 3698 743 1170   5672 7659	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
	3 2523 22
39   7569   6570 691 1425 717 2505 744 0204   4948 7193	7429 21
00,000,000,000,000	2337 20
\( \frac{40}{41} \big  \big  \frac{600}{5779} \big  \big  \frac{692}{4969} \big  \big  \big  \frac{691}{718} \big	7247 19
42 9886 9171 4328 5729 745 3770 8878 801 1511 830	2160 18
43   642 3994   667 3374   8638   719 0141   8296   773 3526   6288	7075 17 (
	$egin{array}{c c c c c c c c c c c c c c c c c c c $
	2 1834 14
7	6759 13
→ 48   4500   4417 ·695 0181 ·721 2227 ·748 0950   6795 ·804 020€ ·835	3 1 686 12 '
\[ \rightarrow 49 \ 8678 \ 8630 \ 4496 \ 6656 \ 5494 \ 776 1455 \ 4997 \]	6615 11
	4 1547 10
51 6918 7061 696 3131 5509 4575 777 0782 805 4584	6481 9 5 1418 8
	5 1418 8 6357 7
	61298 6
( 55   647 3417   672 3944   698 0422   724 3227   751 2762   9460   807 3787	6242 5
2 56   7546   8169   4749   7668   7314 779 4135   8598 83°	7 1188 4
\$\begin{array}{c c c c c c c c c c c c c c c c c c c	6136 3 8 1087 2
58 5808 6624 699 3409 6540 6423 780 3492 8212 83 59 9941 674 0854 7741 726 0982 753 0981 8173 809 3025	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
59   9941 674 0854   7741 725 0982 753 0981   8175 809 5025   60   649 4076   5085 700 2075   5425   5541 781 2856   7840 83	
\( \begin{array}{c c c c c c c c c c c c c c c c c c c	500 /

50	~~~~~	41°	$\widetilde{42^{\circ}}$	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~ <del>45°</del> ~	$\sim_{46^{\circ}}\sim$	$\sim_{47^{\circ}}$	$\hat{\gamma}$
90		·869 2867		932 5151			1.03 55303	1.07 23687	60)
$\begin{cases} 1 \\ 2 \end{cases}$	5955	7976		933 0591	966 2511	05819	61333	29943	
(3	·840 0915 5878	·870 3087 8200	·901 4580 9854	6034 934 1479	8137 967 3767	11642 17469	67367 73404	36203 42467	
54	841 0844	.871 331€	902 5131	6928	9399	23298	79445	48734	
5 5	5812	8435	·903 0411	935 2380	·968 5035	29131	85489	55006	
$\begin{cases} 6\\7 \end{cases}$	842 0782	872 3556	5693 904 0979	7834	*969 0674	34968 40807	91538 97589	61282 67561	
> 8	5755 843 0730	8680 873 3806	6267	·936 3292 8753	6316 970 1962		1.04 03645	73845	
9	5708	8935	905 1557		7610	52497	09704	80132	
210	844 0688	874 4067	6851	9683	-971 3262	58348	15767	86423	
(11	5670	9201	906 2147		8917	64201	21833	92718	
\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	845 0655 5643	875 4338 9478	7446 907 2748	·939 0625 6101	•972 4575 •973 0236	70058 75918	27904 33977	99018 1.08.05321	
(14				940 1579	5901	81782	40055	11628	
(15	5625		908 3360	7061	-974 1569	87649	46136	17939	
$\begin{cases} 16 \\ 17 \end{cases}$	101.0020	.877 4912 .878 0062		941 2545	7240 •975 2914	93520 99394	52221 58310	24254 30573	
218		5215		942 3523		1.0105272	64402	36896	
19		879 0370		9017	976 4272	11153	70498	43223	
20		5528	9940	943 4513	9956	17038	76598	49554	
$\frac{21}{22}$	, 0002				977 5643	22925	82702	55889	
23			912 0592	5516 945 1021	978 1333 7027	28817 $34712$	88809 94920	62228 68571	
$\langle 24 \rangle$	851 0667		913 1255	6530	979 2724	40610	1.05 01034	74918	
(25	5684	882 1357	6591	:946 2042	8424	46512	07153	81269	35(
$\frac{\langle 26}{27}$				7556	•980 4127	52418	13275 19401	87624	
528				947 3074 8595	9833 •981 5543	58326 64239		93984 1.09.00347	
529					982 1256	70155	31664	06714	
230		7258	916 3312	9646	6973	76074	37801	13085	
31				949 5176	983 2692	81997	43942	19460	
$\begin{cases} 32 \\ 33 \end{cases}$				950 0709 6245	8415 984 4141	87923 93853	50087 56235	25840 32223	28
(34	856 0950		918 4740	951 1784	9871	99786	62388	38610	26(
(38 )36						1.02 05723	68544 74704		
37				952 2871 8420	986 1339 7079		80867		23
)38					987 2821	23555			
)39	618	889 403	921 1590	9526	8567	29500	93206	70609	215
14.0				954 5083	1988 4316				
\\\d\{4\}				955 0644	•989 0069		1.06 05560		
(4:				6208 956 1774	5825 1584		11742 17929		
(4)								1.10 02709	
(43			924 3905	957 2917	•991 3112				
\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\					992 4654				
(4)			2 926 0102	958 4073					
(4	684		5506	959 5241					
55	864 192	6 895 150	927 0914	960 0829	•994 <b>1</b> 993	9520			5 10
5						1.03 0119			
\\ 5				3 ·961 2016 1  7614					
(5									
(5	5 736	5 773	799	8819	997 095	2520	9246	7369	3 5)
(5	- 00. 2.20								
)5 5									
$\zeta_5$				1965 1268			7 1743	9963	0 19
ζ6	0 869 286	7 900 404	0 932 515	1 6888	3 1.000 000			7 1.11.0612	5 00
5	'  49°	480	470	460	450	440	43°	420	13
<b>~</b>	~~~	$\sim \sim$	~~~	~~~	~~~	~~~	~~~	~~~	$\sim$

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$\sim$	$\stackrel{\sim}{148^{\circ}}$	$\sim_{49^{\circ}}$	$\sim_{50^{\circ}}$	$\sim_{\widetilde{51}^\circ}$	$\widetilde{52^{\circ}}$	$\sim_{53}$ $\sim$	$\sim_{54}\sim$	$\sim$
ζ ο						1.3270448	1.37 63819	60 \
ζĭ	12624	10445	24579		1.28 07094	78483	72242	59
( 2	19127	17210	31626	63672		86524	80672	58 ?
7 3	25635	23979	38679	71030	22465	94571	89108	57 >
4	32146	30754	45736	78393		1.33 02624	97551	56 >
) 5	33662	37532	52799	85762		10684	1.38 06001	55 )
> 6	45182	44316	59866	93136		18750	14458	54
5 7	51706	51104		1.24 00518		26822	22922	53 \
5 8	58235	57896	74015	07900		34900	31392	52 \
5 9	64768	64693	81097	15290		42984	39869	51 \
5 10	71305	71495	88184	22688		51075	48353	50 \$
( 11	77846	78301	95276	30086		59172	56844	49
$\begin{cases} 12 \\ 13 \end{cases}$	84391 90941	91927	1·20 02373 09475	37492 44903		67276 75386	65342 73847	48
14	97495	91927	16581		1.29 07421	83502	82358	47 }
15		1.16 05571	23693	59742		91624	90876	45
16	10616	12400	30810	67169		99753	99401	44 <
(17	17183	19284	37932	74602		1.34 07888	1.39 07934	43.
( 18	23754	26073	45058	82040		16029	16473	42 (
( 19	30329	32916	52190	89484	46270	24177	25019	41 (
( 20	36909	39763	59327	9693	54057	32331	33571	40 (
( 21	43493	46615		1.25 04388	61850	40492	42131	39 (
( 22	50081	53472	73615	11848		48658	50698	38 2
23	56674	60334	80767	19313		56832	59272	37 /
24	63271	67200	87924	26784		65011	67852	36 >
25	69872	74071	95085	34260		73198	76440	35
26	76478 83088		1·21 02252 09424	49229	1.30 00904 08733	81390	85034 93636	34 \
$\begin{cases} 27 \\ 28 \end{cases}$	89702	87827 94712	16601	5672		89589 97794	1.40 02245	$\begin{pmatrix} 33 \\ 32 \end{pmatrix}$
29		1.17 01601	23783	64219		1.35 06006	10860	31
30	1.13 02944		30970	7172	1	14224	19483	30
31	09571	08496 15395	38162	7923		22449	28113	29
32	16203	22298	45359	86747		30680	36749	28
33	22839	29207	52562	9426		38918	45393	27
34	29479	36120	59769			47162	54044	26 )
35	36124	43038	66982	0932		55413	62702	25
36	42773	49960	74199	16860		63670	71367	24 5
37	49427	56888	81422	2440		71934	80039	23 (
38	56085	63820	88650	31950		80204	88718 97405	22 (
39	62747	70756	95883		1.31 03140	88481		21 (
40	69414		1.22 03121	4706		96764	1.41 06098	20 (
41	76086	81644	10364	54620		1.36 05054	14799 23506	19 (
$\begin{pmatrix} 42 \\ 43 \end{pmatrix}$	82761 89441	91595 98551	17613 24866	62190 69775		13350 21653	32221	$\begin{vmatrix} 18 \\ 17 \end{vmatrix}$
44		1.18 05512	32125	7735		29963	40943	16
45	1.14 02815	12477	39389	84940		38279	49673	15 4
46	09508	19447	46658	9253		46602	58409	14 (
47	16206			1.27 0013		54931	67153	13 (
48	22908	33402	61211	0773		63267	75904	12 (
249	29615	40387	68496	1534	82474	71610	84662	11 2
2 50	36326	47376	75786	2295	90441	79959	93427	10 /
2 51	43041	54370	83081	3057		88315	1.42 02200	9 )
> 52	49762				11.3206393	96678	10979	8 >
> 53	56486		97687	4583		1.37 05047	19766	7
54	63215		1.23 04997	5347		13423	28561	6 >
55	69949		12313	6111		21806	37362	5 4
\ \ 56 \ 57	76687 83429	89414 96437	19634 26961	6876 7641		30195 38591	46171 54988	3
58		1.19 03465	34292	8407		38591 46994	63811	3
59	96928			9174		55403	72642	1 1
\$ 60	1.15 03684			9941		63819	81480	ōS
57	410	400	390	380	370	360	350	13
$\langle \cdot \rangle$	~~~		<u>ــــــــــــــــــــــــــــــــــــ</u>		~~~.	<u></u>	٠٠٠٠.	کہہٰ
- 0				TATE COT				

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<b>Σ</b>	55°	56°	57°	58°	59°	60°	61°	15
) o			L·53 98650 1	·60 03345	66 42795		1.80 40478	60 >
<b>}</b> 1	90326		L·54 08460	13709	53766	32149	52860	59
2	99178	44231	18280	24082	64748	43803	65256	58
3 4	1·43 08039 16906	53554 62884	28108 37946	34465 44858	75741 86744	55468 67144	77664 90086	57 S
( 5	25781	72223	47792	55260	97758		1.81 02521	55
6	34664	81570	57647		L·67 08782	90533	14969	54
7 7	43554	90925	67510	76094		1.74 02245	27430	53
8 (	52451	1.49 00288	77383	86525	30864	13969	39904	52 )
9	61356	09659	87264	96966	41921	25705	52391	51 )
10	70268	19039		61 07417	52988	37453	64892	50 )
) 11	79187		1.55 07054	17878	64067	49213	77405	49 )
12	88114	37822	16963	28349	75156	60984	89932	48 5
13	97049 1.44 05991	47225 56637	26880 36806	38829 49320	86256 97367	72768 84564	1·82 02473 15026	47 46
$\begin{cases} 14 \\ 15 \end{cases}$	14940	66058	46741		1.68 08489	96371	27593	45
7 16	23897	75486	56685	70330	19621	1.75 08191	40173	44
7 17	32862	84923	66639	80850	30765	20023	52767	43 )
18	41834	94367	76601	91380	41919	31866	65374	42 )
) 19	50814	1.5003821	86572	L·62 01920	53085	43722	77994	41 5
20	59801	13282	96552	12469	64261	55590	90628	40 \
21	68796		1.56 06542	23029	75449	67470	1.83 03275	39 \
22	77798	32229	16540	33599 44178	86647	79362 91267	15936 28610	38 5
$\binom{23}{24}$	86808 95825	41716 51210	26548 36564		97856 1•69 09077	1.76 03183	41297	37 3
$\binom{27}{25}$	1.45 04850	60713	46590	65368	20308	15112	53999	35
26	13883	70224	56625	75977	31550	27053	66713	34
27	22923	79743	66669	86597	42804	39007	79442	88 )
28	31971	89271	76722	97227	54069	50972	92184	32 \
29	41027	98807	86784	<b>Ŀ63</b> 07867	65344	62950	1.84 04940	31 \
30		1.51 08352	96856	18517	76631	74940	17709	30 5
31	59161		1.57 06936	29177	87929	86943	30492	29 5
32	68240 77326	27466 37036	17026 $27126$	39847 50528	99238 1·70 10559	98958 1.77 10985	43289 56099	28 5
34	86420		37234	61218	21890	23024	68923	26
( 35	95522		47352	71919	33233	35076	81761	25
36	1.46 04632		57479	82630	44587	47141	94613	24 )
2 37	13749		67615	93351	55953	59218	1.85 07479	23
38	22874			1.64 04082	67329	71307	20358	22 5
39	32007	1	87915	14824	78717	83409	33252	21 \
240		1.52 04261	98079	25576	90116	95524		20 5
$\begin{pmatrix} 41\\42 \end{pmatrix}$	50296 59452		1.58 08253 18436	47111	1·71 01527 12949	1.78 07651 19790		19 5
43	68616			57893	24382	31943		17
244	77788		38830	68687	35827	44107		16)
45	86967		49041	79490	47283	56285		15 )
₹ 46	9615		59261	90304	58751	68475		
247	1.47 05350			1.65 01128	70230			
48	1455			11963 22808	81720 93222			
\ 49	2376	1			1	1	1	1 )
> 50		3 1.53 01023		33663 44529	1.72 04736			
\ 51 52	4221 5144			55405				
( 53				66292				
2 54				77189		6645	1 28336	6 6
2 55	7919	7 49727	51672	88097	62477	7875	41455	5 5
> 5€			61987	99016	74060			
2 57				1 66 0994				
2 58				20884 31834				
60								
~ ? %	340	330	320	310	300	290	280	1 /)
1	, 01	1 00	5000		1 00	1	1	۱ ـ ۱

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5%	$\widetilde{62^{\circ}}$	63° 1	$64^{\circ}$	$65^{\circ}$	660	670	680	$\widehat{\prime}$
) o		1.96 26105		2.14 45069	2.24 60368		2.47 50869	60 >
) i	20470	40227	18185	61366	77962	77590	71612	59 >
2	33690	54364	33349	77683	95580	96683		58 >
3	46924	68518	48531	94021	2.25 13221	2.36 15801	2.48 13190	57
<b>\ 4</b>	60172	82688		2 15 10378	30885 48572	34946 54118	34023 54887	56 S
5 6	73436	96874 $1.97 11077$	78950 94187	26757 43156	48572 66283	73316	75781	54
> 7	1.89 00006		2.06 09442	59575	84016	92540	96706	53
8	13313	39531	24716	76015	2.26 01773	2.37 11791	2.49 17660	52
) 9	26635	53782	40008	92476	19554	31068	38645	51 >
10	39971	68050	55318	2.16 08958	37357	50372	59661	50 )
) 11	53322	82334	70646		55184	69703	80707	49 >
) 12	66688	96635	85994	41983	73035	89060	2.50 01784	48 >
13		1.98 10952			90909	2.38 08444	22891	47 46
5 14	93464 1.90 06874	25286 39636	16743 32146		2·27 08807 26729	27855 47293	44029 65198	45
$\begin{cases} 15 \\ 16 \end{cases}$	20299	54003		2.17 08283	44674	66758	86398	44
2 17	33738	68387	63007	24911	62643	86250	2.51 07629	$\widetilde{43}$
18	47193		78465	41559	80636		28890	42 >
) 19	60663	97204	93942	58229	98653	25316	50183	41 )
20	74147	1.99 11637	2.08 09438	74920	2.28 16693		71507	40 )
21	87647	26087	24953		34758		92863	39 )
22	1.91 01162			2.18 08364	52846			38
23	14691	55038 69539	56039 71610		70959 89096		35667 57117	36
$\begin{cases} 24 \\ 25 \end{cases}$	28236 41795						78598	35 }
26	55370		2.09 02809			62906	2.53 00111	34 >
27		2.00 13142	18437	92349	4365	82672	21655	33 >
28	82568			2· <b>19</b> 09210				32 >
29	96186	1	1	1	1	l .		$ 31\rangle$
30	1.92 09821							30 >
31	23479							$\begin{vmatrix} 29 \\ 28 \end{vmatrix}$
$\begin{cases} 32 \\ 33 \end{cases}$	37138	86158 912:01 00806						27
34	64516			2.20 10831				26 (
( 35	7822			27843				25 (
( 36	9195							$\begin{vmatrix} 24 \\ 23 \end{vmatrix}$
37	1.93 0569							23
38			1 9161 3 <b>2·11</b> 0747					21 (
39		1			1			20
2 40		0 2·02 0386: 5  1865:		8 <b>2·21 1</b> 3234 6 30379				19 (
$\begin{cases} 41 \\ 42 \end{cases}$								18
( 43							3 70735	17 (
( 44	1.94 0233							16
45			$4 2\cdot 12 0303$					15 (
46		$\begin{array}{cccccccccccccccccccccccccccccccccccc$		0 2 22 1643 6 3370				14 7
47								12
49								
50	ł					- 1		1 /
(5)				08 2 23 0304				
( 5		8251	7 2.13 1545					8 (
(5)	3 2770	04 9751	9 315	59 3784				
(5		13 2.04 1254		14 5528				
( 5								
) 5 5				$\begin{array}{c c} 85 & 9021 \\ 01.2 \cdot 24.0772 \end{array}$				# (
	8 979		00 2.14125					
	9 1.96 120						55 28258	
ζē	0 261	05 2.05 030	38 450	69 603				
(	/ 270	26°	250	24°	230	220	210	11
L_	~~~	~~~	·	~~~	^~~	~~~	$\sim\sim$	$\sim\sim$

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ζ′.	690	70°	71°	, .	20	, .	30	740	750	1)
\ 0 1	2.60 50891 73558	2·74 74774 99661	2·90 42109 69576			3.27		3·48 74144 3·49 12470	3·73 20508 63980	60 }
$\begin{pmatrix} \frac{1}{2} \\ \frac{1}{2} \end{pmatrix}$		2.7524588			37869		76715	50874	3.74 07546	58
$\tilde{3}$	2.61 18995		2.91 24649	ĺ	68468	3.28		89356	51207	57 (
5 4	41766	74561	52256		99122		45164	3.5027916	94963	56 (
5	64571	99608		3.09	29831 60596	0.00	79487	66555	3.75 38815	55 (
$\begin{cases} 6\\7 \end{cases}$	87411 2·62 10286	2·76 24695 49822	2·9 <b>2</b> 07610 35358		60596 91416	3.58	13876 48330	3·51 05273   44070	82763 3.76 26807	54 }
8	33196	74990		3.10	22291		82851	82946	70947	52
9		2.77 00199	90995	10 10		3.30	17438	3.52 21902	3.77 15185	51
10	79121	25448	2.93 18885		84210		52091	60938	59519	50
) 11	2.63 02136	50738		3.11	15254		86811	3.53 00054	3.78 03951	49 (
) 12	25186	76069		1	46353	3.31		39251	48481	48 \
13			2.94 02840		$77509 \\ 08722$		56452	78528 3·54 17886	93109 3·79 37835	47 (
15	71392 94549	26853 52307	59050				$91373 \\ 26362$	57325	82661	$\begin{pmatrix} 46 \\ 45 \end{pmatrix}$
16	2.64 17741	77802			71317	0 01	61419	96846		44
17	40969		2.95 15453	3.13			96543	3.55 36449	72609	43)
18	64232	28917	43727			3.33	31736	76133	3.81 17733	42
2 19	87531	54537	72050		65639		66997	3.56 15900	62957	41 \
20	2.65 10867		2.96 00422		97194	3.34		55749 95681		40 >
$\left\langle \begin{array}{c} 21 \\ 22 \end{array} \right $	54238 57645	2·80 05901 31646			28807 $60478$		37724 73191	3.57 35696	53707 99233	39 8
( 23	81089	57433			92207	3.35		75794		37 }
( 24	2.66 04569	83263	2.97 14399	3.15	23994		44333	3.58 15975	90591	36 2
( 25		2.81 09134			55840		80008	56241	3.84 36424	35 )
$\begin{cases} 26 \\ 27 \end{cases}$	51638	35048	71683 2·98 00400			3.36	15753	96590 3·59 37024	82358 3:85 28396	34 )
28	75227 98853	87003		2.10	51728		51568 87453	77543	74537	$\begin{vmatrix} 33 \\ 32 \end{vmatrix}$
5 29	2.67 22516		57983		83808	3.37		3.60 18146		31 (
30	46215	39129	86850	3.17	15948		59434	58835	67131	30 (
31	69951		2.99 15766		48147		95531	99609	3.87 13584	29 (
32	93725	91426					31699	3.61 40469	60142	28 (
33	2·68 17535 41383	2·83 17639	3.00 02820		12724 $45102$		67938 $04249$	81415 3·62 22447	3.88 06805 53574	$\frac{27}{26}$
35	65267	70196			77540		40631	63566		25
36	89190	96539	61109	3.19	10039		77085	3.6304771		24 5
37		2.8422926				3.40	13612	46064		23 \
38	37147		3.01 19603		75217		50210	87444		22 \
39	61181	75831	1	3.20	07897		86882	3.64 28911	1	21 \
\ 40 41	2·70 09364	2.85 02349	78301 3.02 07728	1	40638 $73440$	3.41	$23626 \\ 60443$	70467 $3.6512111$	3·91 36420 83937	20 S
42	33513	55517			06304		97333	53844		18
43	57699	82168					34297	95665		17 >
44		2.8608863			72215		71334	3.66 37575		16 >
$\begin{cases} 45 \\ 46 \end{cases}$	2.71 06186		3.03 25954					79575		15 >
47	30487 54826	62386 89215			38373 71546		45631 82891	3.67 21665 63845		$\begin{vmatrix} 14 \\ 13 \end{vmatrix}$
\$ 48			3:04 15178					3.68 06115		12 (
49	2.72 03620	43007			38078		57635	48475		ii (
50	28076	69970	74915		71438		95120	90927	3 96 16518	10 1
551	52569	96979	3.05 04866	3.24				3 69 33469		9 (
52	77102	2.88 24033			38346		70315	76104		8 (
53	2·73 01674 26284				$71895 \\ 05508$		$08026 \\ 45813$	3·70 18830 61648		7 7
55			3.06 25203		39184		83676	3.71 04558		6
) 56	75623	32704					21616	47561		45
57	2.7400352	59986			06728		59632	90658		3 5
58	25120		3.07 16020		40596		97726	3.72 33847		-25
60	49927 74774	2·90 14688 42109			$74529 \\ 08526$		35896 $74144$	77131 3·73 20508		$\left \begin{array}{c}1\\0\end{array}\right>$
7	200	190	180		70		60	150	140	13
1~	0	10000	1 20					1 -0		: _ S

5	760	770	$\sim_{78^{\circ}}\sim_{1}$	$\sim_{\widetilde{79^\circ}}$	8000	$\sim_{\widetilde{81}^{\circ}}\sim_{\widetilde{1}}$	$\sim_{82}\sim_{1}$	$\sim$
0	4·01 07809					6.3 137515		60 }
) 1	57570	72316	4.7113686	525557	809446	256601	304190	59 }
$\rangle$ 2	4.02 07446	4.34 30018	81256	605813	906394	376126	455308	58 }
$\begin{cases} 3\\4 \end{cases}$	57440 $4.0307550$		4.7249012 $4.7316954$	767051	5.7003663 101256	496092 616502	607056 759437,	56
( 5	57779	4.36 04003	85083	848035	199173	737359	912456	55 (
(6	4.0408125		4.74 53401	929264	297416		7.2066116	54 (
$\begin{cases} 7\\8 \end{cases}$	58590 4.05 09174	4·37 20731 79317	4·75 21907 90603	5·2 010738 092459	395988	980422 6·4 102633	220422 375378	53 (
5 9	59877		4.76 59490	174428	594122	225301	530987	51
10	4.06 10700	96940	4.77 28568	256647	693688	348428	687255	50
) 11	61643	4.39 55977	97837	339116	793588	472017	844184	49 )
) 12	4.07 12707	4.40 15164	4.78 67300	421836			7.3 001780	48
$\begin{cases} 13 \\ 14 \end{cases}$	63892 4.08 15199		4·79 36957 4·80 06808	504809	994400 5·8 095315	720591 845581	160047 318989	47
15	66627	93641	76854	671517	196572		478610	45
(16	4.09 18178	4.42 53439	4.81 47096	755255		6.5 096981	638916	44 (
217	69852	4.43 13392	4.82 17536	839251	400117	223396	799909	43 (
$\begin{cases} 18 \\ 19 \end{cases}$	4·10 21649 73569	73500 4·44 33762	88174 4·83 59010	923505 5·3 008018			961595 7·4 123978	$\begin{pmatrix} 42 \\ 41 \end{pmatrix}$
20	1.11 25614	94181	4.84 30045	092793		1	287064	40 5
5 21	77784	4.45 54756	4.85 01282	177830				39
5 22	4.12 30079	4.46 15489	72719	263131	915084	862739		38 >
\$ 23	82499	76379	4.86 44359	348696	5.9 019138	992080		37 5
$\begin{cases} 24 \\ 25 \end{cases}$	4.13 35046	4·47 37428 98636	4·87 16201 88248	434527 520626		6.6 121919		36 \
$\frac{25}{26}$	87719 4·14 40519	4.48 60004	4.88 60499	606998				34
27	93446	4.49 21532	4 89 32956	693636				33 }
28	4.15 46501	83221	4.9005620	780538				32 2
29	99635	4.50 45072	78491	867718	651045	778677	787179	31 >
30	4.16 52993	4.51 07085	4.91 51570	955175				30 2
$\begin{cases} 31 \\ 32 \end{cases}$	4·17 06440 60011	69261 4·52 31601	4·92 24859 98358				7·6 128657 300533	$\begin{vmatrix} 29 \\ 28 \end{vmatrix}$
⟨ 33	4.18 13713	94105	4.9372068	21918	8 6.0 079676	313341	473174	27 \
34	67546		4.94 45990					
35 36	4·19 21510 75606		4·95 20125 94474				820769 995735	
37	4.20 29835		4.96 69037	57512			7.7 171486	
38	84196		4.97 43817					
39	4.21 38690	72615	4.98 18813	75478	8 733979	6.8131227	525366	21
40	93318		94027					
241	4.22 48080		4.99 69459					
$\begin{cases} 42 \\ 43 \end{cases}$	4·23 02977 58009	64141 4·59 28325	5.00 45111 5.01 20984					
44	4.24 13177	92680						
45	68482	4.60 57207	5.02 73395					
2 46 47	4.25 23923					$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		
48	79501 4·26 35218						2 7.9 158151	
49								
50	4.27 47066	82457	5.06 58353	76378	6 97027	9 68233	530224	10
51					2 6 2 08510			
552								
53 54							$     \begin{array}{c cccc}       1 & 8 \cdot 0 & 09483 & 0 \\       28479 & 0 & 0 & 0 \\       \hline       28479 & 0 & 0 & 0 & 0   \end{array} $	
) 55								
> 56	85974	1 78595	5.11 2785	5 32947	4 66551	55790	5 667394	4 4
57								
58						$\frac{1}{6.7 \cdot 1} \frac{85457}{00382}$	3 8·1 053599 6 24807	
( 60				0 71281			7 44346	1 0
₹ /	130	120	110	10°	90	80	70	1
4	~~~	~~~	·~~	~~~	·~~	Hosted by	देळळ	'حجح
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( 0	١,	3·1 443464	840				28.636253	57.289962	60 2
( 1	. [	639786	410613	468474	360696	187930	877089	58.261174	59
(2	: 1	837041	679068	507154	421230	295922	29.122006	59.265872	58 (
3		8.2 035239	949022	546093	482273	405133	371106	60.305820	57
$\begin{pmatrix} 4 \\ 5 \end{pmatrix}$		254384 434485	9·6 220486   493475	585294 624761	543833 605916	$515584 \\ 627296$	624499 882299	61·382905 62·499154	56 ) 55 )
( 6		635547	768000	664495	668529	740291	30.144619	63.656741	54
5 7	1	837579	9.7 044075	704500	731679	854591	411580	64.858008	53 (
( 8		8.3 040586	321713	744779	795372	970219	683307	66 105473	52 (
( 8		244577	600927	785333	859616	20.087199	959928	67.401854	51 (
5 10		449558	\$81732	826167	924417	205553	31.241577	68.750087	50 \ 49 \
$\binom{11}{12}$		862519	9·8 164140 448166	867282 908682	989784 15·055723	325308 446486	528392 820516	70·153346 71·615070	48
1		8.4 070515	733823	950370	122242	569115	32.118099	73.138991	47
14	1	279531	9.9 021125	992349	189349	693220	421295	74.729165	46
) 1		489573		12.034622	257052	818828	730265	76.390009	45
		700651 912772	600724 893050	077192 120062	325358 394276	945966 21.074664	33·045173 366194	78·126342 79·943430	44 \ 43 \
(13		8.5 125943		163236	463814	204949	693509	81.847041	42
(1		340172		206716	533981	336851	34.027303	83.843507	41 2
( 2	0	555468	078031	250505	604784	470401	367771	85.939791	40 (
( 2		771838		294609	676233	605630	715115	88.143572	39 (
$\binom{2}{2}$		989290		339028	748337	742569		90·463336 92·908487	$\begin{vmatrix} 38 \\ 37 \end{vmatrix}$
$\begin{cases} \frac{2}{2} \end{cases}$		8·6 207833 427475		383768 428831	821105 894545	881251 22 021710	800553	95.489475	36
5 2		648223		474221	968667	163980		98.217943	1 = 5 /
5 2		870088	260249	519942	16.043482	308097	562659	101.10690	34 (
5 2		8.7 093077		565997	118998	454096		104.17094	$\begin{vmatrix} 33 \\ 32 \end{vmatrix}$
$\begin{cases} 2\\2 \end{cases}$		317198 542461		612390 659125	195225 272174	602015 751892		107·42648 110·89205	31
3		768874		706205	349855	903766	1	114.58865	30
3		996446		753634				118.54018	29
( 3	2	8 8 225186	449112	801417	507456	213666	39.056771	122.77396	28 )
( 3		455103		849557	587396			127·32134 132·21851	$\begin{vmatrix} 27 \\ 26 \end{vmatrix}$
	4	686206 91850		898058 946924				137.50745	25 (
	6	8.9 152009						143.23712	24 (
	37	38672						149.46502	23 (
	8	622668			998957			156.25908	22 (
	9	85984		1	17.083724		1	163.70019	21 \
	0	9.0 09826						171.88540	$\begin{vmatrix} 20 & 19 \\ 19 & 19 \end{vmatrix}$
	$\frac{1}{2}$	33793 57886						180.93220 190.98419	18
	3	82107						202.21875	17 5
	14	9.1 06456	848288	403867	520516	6 264361	45.226141	214.85762	16 5
	15	30934						229.18166	15 5
	L6 L7	55543 80283						245·55198 264·44080	14 (
	18	9.2 05156						286.47773	12
	19	30162						312.52137	11 )
( {	50	55303	5 059433	726738	18.07497	431600		343.77371	10 }
	51	80580						381.97099	9 }
	52	9.3 05993						429.71757	8 }
	$\frac{53}{54}$	31545 57235						572.95721	163
	55	83066				3 48985	882109	687.54887	5 (
	56	9.4 09038	4 27888	6 06545				859.43630	4 <
	57	35153						1145·9153 1718·8732	3 3
	58 59	61411 87814						3437.7467	1 1)
	60	9.5 14364		2 30066				Infinite.	0 >
>	/	60	50	40	30	20	10	00	175
1	$\sim$	$\dot{\sim}$	·~~	$\sim$	·	·~~	بمحند	,~~~	~~,
				:	NAT. COT	AN.	Hosted by	ioogle	2
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## 116 COMPARISON OF FRENCH AND ENGLISH BAROMETERS.

200	$\sim \sim \sim$	$\sim$	$\sim\sim$	$\sim \sim$	$\sim\sim$	$\sim$	$\sim\sim$	$\sim$	$\sim\sim$	$\sim\sim$	$\sim\sim$
Milli-	English	Milli-	English	Milli-	English	Milli-	English	Milli-	English	Milli-	English
metres.	inches.	metres-	inches.	metres.	inches.	metres.	inches.	metres.	inches.	metres.	inches
501	19·725	551	21·693	601	23·662	651	25·630	701	27·599	751	29·567 \
502	·764	552	·733	602	·701	652	·670	702	·638	752	
503	·803	553	·772	603	·741	653	·709	703	·677	753	
504	·843	554	·811	604	·780	654	·748	704	·717	754	
505	·882	555	·851	605	·819	655	·788	705	·756	755	
506	·921	556	·890	606	·859	656	·827	706	·795	756	
507	19·961	557	·930	607	·898	657	·867	707	·835	757	
508	20·000	558	21·969	608	·937	658	·906	708	·874	758	
509	·040	559	22·009	609	23·977	659	·945	709	·914	759	
510	·079	560	·048	610	24·016	660	25·985	710	·953	760	
511 512 513 514 515 516 517 518 519 520	·118 ·158 ·197 ·236 ·276 ·315 ·354 ·394 ·433 ·473	561 562 563 564 565 566 567 568 569 570	·087 ·126 ·166 ·205 ·244 ·284 ·323 ·363 ·402 ·441	611 612 613 614 615 616 617 618 619 620	.056 .095 .134 .174 .213 .252 .292 .331 .371	661 662 663 664 665 666 667 668 669 670	26,024 ·063 ·103 ·142 ·181 ·221 ·260 ·300 ·339 ·378	711 712 713 714 715 716 717 718 719 720	27·992 28·032 ·071 ·110 ·150 ·189 ·229 ·268 ·307 ·347	761 762 763 764 765 766 767 768 769 770	29·961
521	*512	571	·481	621	·449	671	·418	721	*386	771	*355 \ .394 \ .433 \ .473 \ .5512 \ .551 \ .630 \ .670 \ .709 \
522	*551	572	·520	622	·489	672	·457	722	*425	772	
523	*591	573	·559	623	·528	673	·496	723	*465	773	
524	*630	574	·599	624	·567	674	·536	724	*504	774	
525	*670	575	·638	625	·607	675	·575	725	*543	775	
526	*709	576	·678	626	·646	676	·615	726	*583	776	
527	*748	577	·717	627	·685	677	·654	727	*622	777	
528	*788	578	·756	628	·725	678	·693	728	*662	778	
529	*827	579	·796	629	·764	679	·738	729	*701	779	
530	*867	580	·835	630	·804	680	·772	730	*740	780	
531	906	581	*875	631	.843	681	·811	731	.780	781	748
532	945	582	*914	632	.882	682	·851	732	.819	782	788
533	20985	583	*953	633	.922	683	·890	733	.858	783	827
534	21·024	584	22·993	634	.961	684	·930	734	.898	784	866
535	•063	585	28·032	635	25.000	685	26·969	735	.937	785	906
536	•103	586	*071	636	.040	686	27·008	736	28.977	786	945
537	•142	587	*111	637	.079	687	·048	737	29.016	787	30-984
538	•181	588	*150	638	.118	688	·087	738	.055	788	31-024
539	•221	589	*189	639	.158	689	·126	739	.095	789	063
540	•266	590	*229	640	.197	690	·166	740	.134	790	103
541 542 543 544 545 546 547 548 549 550	•300 •339 •378 •417 •457 •496 •536 •575 •614 •654	591 592 593 594 595 596 597 598 599 600	•268 •308 •347 •386 •426 •465 •504 •544 •583 •622	641 642 643 644 645 646 647 648 649 650	·237 ·276 ·315 ·355 ·394 ·433 ·473 ·512 ·552 ·591	691 692 693 694 695 696 697 698 699 700	·205 ·245 ·284 ·323 ·363 ·402 ·441 ·481 ·520 ·559	741 742 743 744 745 746 747 748 749 750	·173 ·213 ·252 ·292 ·331 ·370 ·410 ·449 ·488 ·528	PROP' 0:1 :2 :3 :4 :5 :6 :7 :8 :9	L PARTS. \\   0.0039 \\   0.0039 \\   0.0079 \\   0.0118 \\   0.0157 \\   0.0157 \\   0.0236 \\   0.0276 \\   0.0315 \\   0.0354 \\
1 Metre = $39.3707$ English inches = $443.296$ Paris lines.											

<sup>1</sup> Metre = 39·3707 English inches = 443·296 Paris lines.

<sup>1</sup> English foot = 0.304794 metre = 135.114 Paris lines.

∑о. м.	Chords.	D. M.	Chords	D. M.	Chords.	D. M.	Chords.	∞~ D, М.	$\left\langle \begin{array}{c} \sim \sim \\ \text{Chords.} \end{array} \right\rangle$
5	*0015	9	·1569	18	·3129	27	·4669	36	*6180
10	*0029	10	·1598	10	·3157	10	·4697	10	
20	*0058	20	·1627	20	·3186	20	·4725	20	
30	*0087	30	·1656	30	·3215	30	·4754	30	
40	*0116	40	·1685	40	·3244	40	·4782	40	
50	*0145	50	·1714	50	·3272	50	·4810	50	
1 10 20 30 40 50	*0175 *0204 *0233 *0262 *0291 *0320	10 20 30 40 50	·1743 ·1772 ·1801 ·1830 ·1859 ·1888	19 10 20 30 40 50	·3301 ·3330 ·3358 ·3387 ·3416 ·3444	28 10 20 30 40 50	·4838 ·4867 ·4895 ·4923 ·4951 ·4979	37 10 20 30 40 50	*6346 *6374 *6401 *6429 *6456 *6484
2 10 20 30 40 50	·0349	11	·1917	20	•3473	29	*5008	38	·6511
	·0378	10	·1946	10	•3502	10	*5036	10	·6539
	·0407	20	·1975	20	•3530	20	*5064	20	·6566
	·0436	30	·2004	30	•3559	30	*5092	30	·6594
	·0465	40	·2033	40	•3587	40	*5120	40	·6621
	·0494	50	·2062	50	•3616	50	*5148	50	·6649
3 10 20 30 40 50	·0523	12	·2091	21	·3645	30	•5176	39	·6676 (
	·0553	10	·2119	10	·3673	10	•5204	10	·6703 (
	·0582	20	·2148	20	·3702	20	•5233	20	·6731 (
	·0611	30	·2177	30	·3730	30	•5261	30	·6758 (
	·0640	40	·2206	40	·3759	40	•5289	40	·6786 (
	·0669	50	·2235	50	·3788	50	•5317	50	·6813 (
4	*0698	13	·2264	22	3816	31	•5345	40	-6840
10	*0727	10	·2293	10	3845	10	•5373	10	-6866
20	*0756	20	·2322	20	3873	20	•5401	20	-6895
30	*0785	30	·2351	30	3902	30	•5429	30	-6922
40	*0814	40	·2380	40	3930	40	•5457	40	-6950
50	*0843	50	·2409	50	3959	50	•5485	50	-6977
5 10 20 30 40 50	*0872	14	·2437	23	·3987	32	•5513	41	·7004
	*0901	10	·2466	10	·4016	10	•5541	10	·7031
	*0931	20	·2495	20	·4044	20	•5569	20	·7059
	*0960	30	·2524	30	·4073	30	•5597	30	·7086
	*0989	40	·2553	40	·4101	40	•5625	40	·7113
	*1018	50	·2582	50	·4130	50	•5652	50	·7140
6 10 20 30 40 50	·1047	15	·2611	24	·4158	33	.5680	42	·7167
	·1076	10	·2639	10	·4187	10	.5708	10	·7194
	·1105	20	·2668	20	·4215	20	.5736	20	·7222
	·1134	30	·2697	30	·4244	30	.5764	30	·7249
	·1163	40	·2726	40	·4272	40	.5792	40	·7276
	·1192	50	·2755	50	·4300	50	.5820	50	·7303
7 10 20 30 40 50	·1221	16	·2783	25	·4329	34	*5847	43	·7330
	·1250	10	·2812	10	·4357	10	*5875	10	·7357
	·1279	20	·2841	20	·4386	20	*5903	20	·7384
	·1308	30	·2870	30	·4414	30	*5931	30	·7411
	·1337	40	·2899	40	·4442	40	*5959	40	·7438
	·1366	50	·2927	50	·4471	50	*5986	50	·7465
8 10 20 30 40 50	·1395	17	·2956	26	·4499	35	·6014	44	·7492
	·1424	10	·2985	10	·4527	10	·6042	10	·7519
	·1453	20	·3014	20	·4557	20	·6070	20	·7546
	·1482	30	·3042	30	·4584	30	·6097	30	·7573
	·1511	40	·3071	40	·4612	40	·6125	40	·7600
	·1540	50	·3100	50	·4641	50	·6153	50	·7627

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